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Intrinsic Remediation Engineering Evaluation/Cost Analysis for UST Site 870



Hill Air Force Base Ogden, Utah

Prepared For

Air Force Center for Environmental Excellence Technology Transfer Division Brooks Air Force Base San Antonio, Texas

and

Hill Air Force Base Ogden, Utah

June 1995

PARSONS ENGINEERING SCIENCE, INC.

1700 Broadway, Suite 900 • Denver, Colorado 80290 • (303) 831-8100 • Fax: (303) 831-8208

May 22, 1995

Mr. Jerry Hansen AFCEE/EST 8001 Arnold Drive Brooks AFB, TX 78235-5357

Subject:

Response to Comments on the "Intrinsic Remediation Engineering

Evaluation/Cost Analysis for UST Site 870" Hill AFB, Utah

Dear Mr. Hansen:

Parsons Engineering Science, Inc. (Parsons ES, formerly Engineering-Science, Inc.) is pleased to submit this letter in response to comments from Mr. Andrew F. Gemperline of Hill AFB and from Montgomery Watson (comments submitted through Mr. Gemperline).

We found these comments both constructive and informative and look forward to further comments regarding the intrinsic remediation demonstration program. If you have any comments, or if we can be of further assistance, please do not hesitate to call Todd Wiedemeier or Todd Herrington at (303) 831-8100.

Respectfully,

Todd H. Wiedemeier Project Manager

R. Todd Herrington

Project Environmental Engineer

Attachment

cc:

Lt. Col. Ross N. Miller, AFCEE Mr. Douglas Downey, Parsons ES

File 722450.07 Letters

022/722450/101.WW6



EXECUTIVE SUMMARY

This report presents the results of an engineering evaluation/cost analysis (EE/CA) performed by Parsons Engineering Science, Inc. (Parsons ES) [formerly known as Engineering-Science, Inc. (ES)] at Hill Air Force Base, Uta evaluate the use of intrinsic remediation (natural attenuation) with long-term monitoring as a remedial option for dissolved-phase benzene, toluene, ethylbenzene, and xylene (BTEX) contamination in the shallow saturated zone near underground storage tank (UST) Site 870. Soil and ground water contamination is known to occur at the site, with contamination being present in the dissolved and gaseous phases, and as light nonaqueous phase liquid (LNAPL). This study focused on the impact of dissolved-phase BTEX on the shallow ground water system at the site. Site history and the results of soil and ground water investigations conducted previously are also summarized in this report.

An important component of this study was to assess the potential for BTEX dissolved in ground water to migrate from UST Site 870 to potential receptors. The Bioplume II model was used to estimate the rate and direction of dissolved-phase BTFY movement through the shallow saturated zone under the influence of advection, dispersion, and biodegradation. Input parameters used for the Bioplume II model were obtained from asting site characterization data, supplemented with data collected by Parsons ES in conjunction with personnel from the United States Environmental Protection Agency Robert S. Kerr Environmental Research Laboratory. Chemical analysis of a single LNAPL sample suggests that LNAPL contamination at the site is weathered JP-4 jet fuel. Extensive site-specific data were used as model input. Model input parameters that were not measured at the site were estimated using reasonable literature values for hydrogeologic conditions similar to those found at the site.

The results of this study suggest that dissolved-phase BTEX contamination present in ground water at UST Site 870 poses no significant risk to human health or the environment in its present, or predicted future, concentration and distribution. It is therefore recommended that intrinsic remediation with long-term monitoring be implemented for dissolved-phase BTEX contamination found in ground water at this site. To reduce sources of continuing contamination, it is also recommended that mobile LNAPL recovery operations and bioventing activities currently underway at the site be continued.

To verify Bioplume II model predictions, it is recommended that eight long-term monitoring (LTM) wells, three point-of-compliance (POC) monitoring wells, and a POC sampling location at

I. Response to comments submitted by Mr. Andrew F. Gemperline, Site 870 project manager:

1. Figure 1.2 Site Map Suggest the base boundary and major interstate highway be identified on this figure. This document is intended as part of Hill AFB's corrective action plan and will be subject to public review and comment. Identification of major public roads and structures will aid in local citizen's review.

Response: Agree, these changes have been made to Figure 1.2.

2. P 1-3 Section 1.2 The fifth sentence references the location of former UST 870, however, Figure 1.2, which was referred to in the previous sentence does not identify where UST 870 was. Please include location of former UST, Building 870, Hill Field Elementary, and other predominant surface features that would aid the unfamiliar reader in understanding the site.

Response: Agree, these changes have been made to Figure 1.2.

3. P1-6 Section 1.2.1. Delete in fourth sentence the reference to Patriot Hills as consisting of industrial and office facilities associated with mission support services. It is a military residential community.

Response: Agree, the sentence now reads: "The Patriot Hills housing area consists of military residential housing."

4. P1-6 Section 1.2.1 Second paragraph Replace the wording, "to optimize the usage and number of storage tanks," with "upgrade the underground storage tank,".

Response: Agree, the sentence now reads: "UST 870.0 was excavated and removed in May 1991 and upgraded with a new double-walled steel UST equipped with leak-detection equipment. The new UST serves the same purpose as UST 870.0"

5. **P2-2 Section 2.1** Reference Figure 1.2 for location of the EPA wells identified in this section. Reference to Figure 1.2 in section 2.2.1 can then be deleted.

Response: We agree that Figure 1.2 should be referenced in Section 2.1. However, Section 2.2.1 references Geoprobe[®], storm sewer, and monitoring well locations where groundwater samples were collected, and reference to Figure 1.2 should not be deleted. Therefore, the second sentence in the second paragraph of Section 2.1 now reads: "Phase one occurred during the week of 16 August 1993, and consisted of drilling, soil sampling, and monitoring well installation at EPA-82-A, EPA-82-B, EPA-82-C, EPA-82-D, EPA-82-E, EPA-82-F, EPA-82-H, and EPA-82-I (Figure 1.2)."

6. P2-3 Section 2.1.2.2 More details as to location of Hill AFB decontamination pad and their collection tanks is required in this section. I believe the location would have been on the north end of the Industrial Waste Treatment Facility (IWTP) on base. Please clarify and describe. Furthermore, on P2-7, the final paragraph of this section probably meant the well completion materials were "not" stored near or in areas which could be affected by these substances.

Response: The first sentence in the second paragraph now reads 'During drilling operations, the drill rig, augers, and any downhole drilling and/or sampling equipment were decontaminated at the northern end of the industrial waste treatment plant (IWTP) at Hill AFB." If you can provide more information on the number and size of the IWTP holding tanks, Parsons ES will incorporate this information into Section 2.1.2.2."

The final paragraph of Section 2.1.2.2 now reads: "Well completion materials were not stored near or in areas which could be affected by these substances."

7. **P2-10 Section 2.1.2.5** Last sentence should reference the Hill AFB industrial wastewater treatment plant (IWTP). Furthermore, did all the wells produce the 10 well casing volumes and have stable numbers for the parameters stated in this section? If not please indicate those that didn't and give explanation.

Response: The last sentence of Section 2.1.2.5 now reads: "All well development waters were collected in 55-gallon drums and transported to the Hill AFB IWTP for treatment and disposal."

As stated in the document, ten casing volumes were purged from each well, and all parameters listed in Section 2.1.2.5 stabilized.

8. Section 2 General Comment Geoprobe is often referred to throughout this section. Please provide detailed description as to what the Geoprobe and its sampling apparatus is. Include diagrams where appropriate.

Response: Agree, a new Figure 2.1 showing the Geoprobe apparatus has been included. In addition, the following text has been added to Section 2.2.3.1: "The Geoprobe® system is a hydraulically powered percussion/probing machine used to advance sampling tools through unconsolidated soils. This system provides for the rapid collection of ground water (and soil and soil gas if necessary) samples at shallow depths while minimizing the generation of investigation-derived waste materials. Figure 2.1 is a diagram of the Geoprobe® system. The following sections describe the Geoprobe® ground water sample collection methods and decontamination methods for the Geoprobe® system."

9. **P2-9 Section 2.1.2.4.2** Please direct reader to location where Monitoring Well Installation Record form information can be found.

Response: Field copies of the monitoring well installation records have been included in Appendix A and referenced as appropriate in Section 2.1.2.4.2. The first sentence in Section 2.1.2.4.2 now reads: "Upon completion of drilling, a monitoring well casing was installed. Well construction details were noted on a Monitoring Well Installation Record form. This information became part of the permanent field record for the site, and copies of the forms are included in Appendix A."

10. P2-13 Section 2.2.2.1 Please direct reader to location where the ground water sampling form information can be found.

Response: No deviations from the protocol listed in Section 2.2.2.1 were necessary.

Therefore, the last sentence in this section has been removed.

11. **P2-16 Section 2.2.3.2.3** Reference IWTP as stated in comment #7 above.

Response: Agree, the reference now reads: "All purge water was placed in 55-gallon drums and transported to the Hill AFB IWTP for disposal and treatment."

12. **P2-17 Section 2.2.4.1 & 2.2.4.2** Please be more detailed as to how DO was measured (e.g. Flask was continuously filled by peristaltic pump well water while DO meter was submerged.)

Response: Agree, Section 2.2.4.1 now reads: "DO measurements were taken using an Orion model 840 DO meter. Groundwater was continuously extracted and collected in an erlenmeyer flask using a peristaltic pump. The probe of the DO meter was submerged in the flask to monitor DO concentrations. DO concentrations were recorded after DO readings stabilized, and these readings represent the lowest DO concentration observed."

Section 2.2.4.2 now reads: "Redox potential measurements were taken in a similar manner as DO measurements using an Orion model 290A redox potential meter. Groundwater was continuously extracted with a peristaltic pump and collected in an erlenmeyer flask. The redox probe was submerged in the flask to take continuous redox measurements. Redox potential measurements were recorded after the readings stabilized, and these readings represent the lowest redox potential observed."

13. **P2-17 Section 2.2.5.1** Please provide the details of what chemical preservatives were used, their amounts, which analytical methods required them, etc. The ability to evaluate the data quality would require this knowledge.

Response: Additional detail on preservation methods has been added, and the section now reads: 'The USEPA Mobile Laboratory added any necessary chemical preservatives to sample containers prior to sampling. Soil samples collected for VOC analysis were stored in 40 milliliter (mL) volatile organic analysis (VOA) vials and preserved with 5 mL of acidified water (pH < 2) and 5 mL of methylene chloride. Soil samples collected for TOC measurements were stored at 4 degrees Celsius (°C) in coolers. Ground water samples collected for VOC analysis were stored in 40 mL VOA vials with lead-lined septa and preserved with 4 grams of trisodium phosphate. Ground water samples for all oxidized inorganic compounds, with the exception of nitrate, were stored in 200 mL high-density polyethylene (HDPE) sample containers and stored at 4°C or below. Ground water samples collected for nitrate analysis were stored in 200 mL HDPE sample containers and acidified (pH < 2) with sulfuric acid. All analysis for reduced inorganic species (e.g., ferrous iron, nitrite, and methane) were performed immediately in the field."

14. **P3-1 Section 3.1.2** The stormwater collection pond is designated Pond 5 not Pond 3. Please change in this section and on Figure 3.1.

Response: The referenced storm water collection pond should have read 'Pond 5" instead of 'Pond 3". The reference to the pond now reads: 'There is a stormwater collection pond (Pond 5) located to the southwest of the Patriot Hills Housing Area (Figure 3.1)." The same change was made on Figure 3.1.

15. Appendix A Monitoring Well completion diagrams for wells other than EPA-92A, 82B, and 82J were not included in this appendix. Please provide.

Response: Parsons ES records show that completion diagrams for monitoring wells EPA-82-A through EPA-82-J were included in the EE/CA report. Missing well completion diagrams were probably the result of accidental omission during copying. Monitoring well EPA-82-G does not exist and monitoring well EPA-82-K was a temporary Geoprobe® ground water sampling point. Hence, neither EPA designated well has a construction diagram.

16. Figure 3.5 Section 3.3.3.1 references the gradient between EPA-82-I and CPT-27 as shown in Figure 3.5. It is difficult for the reader to find these points when looking at Figure 3.5. Please clean up Figure 3.5 by placing monitoring point location annotation in visible areas.

Response: Agree that certain well labels are obscured. Monitoring point locations have been clarified in Figure 3.5 revisions.

Give explanation for the two orders of magnitude difference in 17. **P3-8 Section 3.3.3.2** hydraulic conductivity between the ES slug test findings and the JMM (1991) findings.

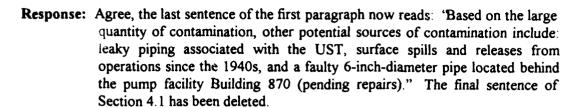
Response: As illustrated in available boring logs from both Parsons ES and JMM, the heterogeneous site stratigraphy is composed of numerous soil types. including moderately sorted, silty fine- to medium-grained sand, medium- to course grained sands, cohesive clayey silts to silty clays, silty clay, and clayey sand. Slug tests were performed by JMM at MW-1, whose screened interval is located in silty sands with a large interval (~4 ft) of clayey sand. The EPA monitoring wells where Parsons ES performed slug tests are screened in predominately fine- to medium grained sands. Based on well screen placement, slug tests performed by Parsons ES would give higher hydraulic conductivity values because they were performed at well location screened in more conductive soils.

> The above comments have been included in Section 3.3.3.2 as an additional paragraph that reads: "The average hydraulic conductivity estimated by Parsons ES for the shallow saturated zone is one to two orders of magnitude higher than hydraulic conductivities estimated by JMM (1993b). illustrated in available boring logs from Parsons ES and JMM, the heterogeneous site stratigraphy is composed of numerous soil types including moderately sorted, silty fine- to medium-grained sand, medium- to course grained sands, cohesive clayey silts to silty clays, silty clay, and clayey sand. Slug tests performed by JMM at MW-1 were influenced by silty sands with a large interval (~4 ft) of clayey sand over the screened interval of the well. The locations selected by ES for slug testing (EPA installed wells) were characterized by predominately fine- to medium-grained sands over the well screen intervals; thus, higher values of hydraulic conductivity were derived because slug tests were conducted in more transmissive soils."

18. P3-11 Section 3.3.3.5 More specific data about the utility corridor on the north side of Sixth Street should be given to assure the reader that it is an unlikely flow path. Include depth to ground water and anticipated or verified depth of utilities to substantiate the improbability of this corridor as a preferential flow path.

> Response: Parsons ES will gladly incorporate any utility corridor data (e.g., survey data) into Section 3.3.3.5 (illustrating the low potential of the utility corridor as a preferential flow route for groundwater) if Hill AFB will provide the necessary information.

19. P4-1 Section 4.1 Indicate that there were many sources of contamination identified at Site 870 including, leaky piping associated with the UST, surface spills and releases from operations since the 1940s, and a faulty 6"diameter pipe located behind the pump facility Building 870 which has been taken out of use until repairs are made. Delete the last sentence, "All underground pipelines have been replaced with aboveground pipelines to remove this possible source of contamination."



20. **P4-9 Table 4.2** Add note to the bottom of table including what "d" associated with SS870A-03 d means. I believe it is a duplicate of a sample analysis.

Response: Agree, this change has been made to Table 4.2. Please confirm for Parsons ES that "d" does indicate a duplicate sample analysis.

21. **P4-12 Section 4.2.3 & Table 4.3** The sample location designations are confusing to me. Need to clarify where these samples were taken within the boring, e.g. Additionally, no discussion as to the appropriateness of using one sampling point over a 10 acre site, consisting of varying geology, to determine the TOC value for the site is given. Montgomery Watson may have additional TOC or OC information to help substantiate the overall site conditions. Please address.

Response: Sample depth designations have been clarified in Table 4.3. An additional paragrarh justifying Parsons ES use of soil TOC data reads: 'Soil TOC samples were collected just below the phreatic surface for accurate estimates of TOC in the shallow saturated zone. EPA-82-E was selected as a TOC sampling location because it was located outside of mobile or residual LNAPL contaminated soils (which would compromise TOC readings) and directly downgradient from potential plume migration. As a result, the soil TOC at EPA-82-E is indicative of the potential sorptive potential in the shallow aquifer directly downgradient of anticipated plume migration. The TOC estimate compares favorably with literature values defining TOC contents in relatively clean, sandy soils (0.01 percent TOC)." If MW personnel can supply additional TOC data, they will be taken into consideration.

22. **P4-20 Section 4.3.1** Top line references the period between August 1993 and July 1994. It would be less confusing to state between August 1992 and July 1994 to account for the actual comparison time frame. Additionally, some discussion of the comparability of results of samples taken from CPT and TP locations in the field in 1992, with those taken from monitoring wells August 1993 and July 1994, should be given. I do not believe the comparison of Figure 4.4 with Figure 4.5 is appropriate because of the differing sampling and analysis methods used in obtaining the BTEX results used. We can discuss further, however, the presentation of data with questionable comparability is not wise when presenting an innovative approach to cleanup.

Response: We agree that some confusion exists concerning the description of analytical data that were combined to produce BTEX isopleth maps in Figures 4.4 and 4.5. Additional clarification on the generation of these figures has been added to Section 4.3.1.

We disagree that comparison of different sampling and analysis methods used in obtaining BTEX results is invalid. Great care was taken by EPA chemists to protect the integrity of ground water samples by proper sampling technique (minimizing the formation of headspace gases or turbulence that might cause premature volatilization of BTEX compounds) and sample preservation. The same assumption of appropriate sampling technique was extended to JMM's sampling effort for well locations in 1992.

As long as appropriate QA/QC procedures (e.g., sample preservation, instrument calibration, duplicates, matrix spike analyses) are followed from the time the samples are collected through the time they are analyzed, the use of different analytical methods should not produce incompatible results. Therefore, the comparison of data collected in 1992 (EPA methods SW8020 and SW8015M) with data collected in 1993 and 1994 (RSKOP-124) is appropriate.

In addressing concerns about the compilation of different time periods of BTEX data to construct 1993 and 1994 BTEX plume maps, this is a valid technique because it conservatively estimates the total, potential areal extent and concentrations of the hydrocarbon plume, especially when data sets are incomplete based on the number of sampling points at a certain time period. In realization that upgradient data points were missing from 1992/1993 data sets (and it was known that contamination was present in the source area), monitoring wells MW-01, MW-02, and MW-04 through MW-09 were supplemented with 1992/1993 data for a conservative BTEX plume shape. Regardless of the 1992/1993 (with supplemented 1994) data compilation, BTEX in ground water did not migrate a significant distance downgradient, or expand laterally, as indicated by BTEX concentrations in samples collected from Jowngradient and peripheral wells.

These previous comments were addressed in Section 4.3.1 by adding or amending the text as follows (in bold): "To evaluate trends in BTEX loss over the site, data sets from different sampling periods were combined to form BTEX isopleth maps for 1993 and 1994 (described in preceding paragraphs). Although generally not a concern, the various ground water analytical methods used to sample ground water from different site characterization studies (1992 to 1994) were judged for their quantitative comparability. Method RSKOP-124 was used by Parsons ES to quantitate aqueous BTEX concentrations during August 1993 and 1994 sampling events. RSKOP-124 is a dual-column, gas

chromatography/mass spectrometry (GC/MS) technique that has resolution capabilities that are superior to EPA SW-846 Methods 8020/602, 8015M, and 8240 (used for volatile and semi-volatile organic analysis by JMM in 1992). All analytical techniques used for VOC analysis in the different site characterization studies from 1992 to 1994 had identical, achievable detection limits of 1 µg/L and adequate compound resolution capabilities. Hence, comparison of different ground water data sets is not compromised by underestimation or overestimation of a particular analytical technique. Groundwater extraction and preparation techniques used by JMM in 1992 are not available; however, potential differences in sampling technique were predicted to be minor because ground water sampling techniques are fairly standardized."

'Figure 4.4 is an isopleth map that shows the distribution of total BTEX dissolved in ground water through August 1993. Because this figure was used for Bioplume II model input (to be conservative), the highest total BTEX concentrations observed in ground water between August 1992 and August 1993 were used to prepare this figure. This figure also includes data collected from monitoring wells in the source area north of Sixth Street in December 1993/January 1994 (MW-01, MW-02, and MW-04 through MW-09). These wells cover a very small area relative to the areal extent of the plume, and in some cases these data represent the only data available for this area. As a result, Figure 4.4 represents the most justifiably conservative representation of the 1993 BTEX plume based on all available data. BTEX contamination is migrating to the southwest in the direction of ground water flow. During the period through August 1993, the BTEX plume was approximately 1,650 feet long and 750 feet wide at the widest point."

Figure 4.5 is an isopleth map that shows the distribution of total BTEX dissolved in ground water in July 1994. Like Figure 4.4, this figure also includes data collected from monitoring wells in the source area in December 1993/January 1994 (MW-01 through MW-09) to illustrate the most justifiably conservative BTEX plume for 1994. Comparison of Figures 4.4 and 4.5 suggests that a substantial reduction in the areal extent and concentration of the BTEX plume occurred between August 1993 and July 1994. With the exception of total BTEX concentrations in some of the monitoring wells located in the area containing mobile LNAPL (wells MW-05, MW-06, EPA-82-D), dissolved-phase total BTEX concentrations were seen to decline over this period. The increased concentrations in these wells could be the result of a fresh spill in the source area. Figure 4.4 shows that through August 1993, the majority of the dissolved-phase..."

23. **P4-20 Section 4.3.1** Provide some discussion as to the comparability of EPA-82-I analytical results in 11/93 to those of 7/94.

Response: Groundwater BTEX levels measured at EPA-82-I in November 1993 were quantitated with a head space analysis, while July 1994 BTEX levels were not. Agree that an analysis discrepancy existed between these two sampling events, and the November 1993 data has been omitted from use in Figure 4.4. Otherwise, Figure 4.4 remains unchanged. Furthermore, references to EPA-82-I data during this time period have been omitted from the text in Section 4.3.1.

24. Figure 4.4 It appears the southeastern portion of this isopleth is a fabrication without data to support. I feel it unwise to present Figure 4.4 as shown with contour lines for concentrations of 1,000 through 4,000 µg/L between monitoring points such as CPT-36 and MW-10. This portion of Figure 4.4 is a large portion to have decreased, as shown in Figure 4.5 and is not founded on available comparable data. Where isopleth contours are in question due to lack of data, please use a broken line to present the uncertainty of the condition.

Response: We feel that isopleth lines of any sort have an inherent error associated with them because they are interpretations of predicted contaminant concentrations based on observed trends and gradients. Isopleth lines unbounded at an edge by a data point have been dashed in Figures 4.4 and 4.5, and in all other figures in the Hill AFB EE/CA.

25. Figure 4.6 & Figure 4.7 My guess is that Figure 4.6 presents a wider DO plume than the data used to generate it represents. Neither Figure 4.6 or 4.7 have much DO data to substantiate the contours on the southeast portion of the plume. Remove all symbols associated with Geoprobe sampling, soil boring or monitoring well locations not used in measuring the DO in preparation of these figures to enable a less cluttered look at the data used to prepare these figures. Where no data exist to support the isocontours over a large area, we need to use a broken line and explain the uncertainty of our contour placement. Otherwise, the reader is left believing we sampled extensively and our isopleth is quite accurate, when in reality the isopleth is at best an individual interpretation of the data. Each reader may have a wholly different interpretation of the isopleth configuration if examining the DO points used to produce the figure alone.

Response: The isopleths on the southeast portion of the plume were drawn to honor the data points collected at CPT-23, EPA-82-H, and EPA-82-B. Hence, continuity was maintained between the source area and these wells by using inferred isopleth intervals. As stated in response 24, all isopleths are somewhat subjective interpretations of site data. We feel that the locations of the isopleth lines we used are good representations of the data; however, dashed isopleth lines have been included to illustrate the potential variance of these lines in this area. Points containing no data have been removed from Figures 4.6 and 4.7.

26. Figure 4.8 & 4.9 I would suggest, as in comment #25, that those points not sampled for the parameter, in this case Nitrate and Nitrite, be removed from each figure to allow the reader to evaluate the interpretation of the isopleth map for him/herself.

Response: Agree, well and CPT locations not sampled have been omitted from Figures 4.8 and 4.9.

27. General Comment: Figures 4.10 through 4.17 Refer to comment #25. Remove all unnecessary symbols and sampling points not sampled to gain data for preparation of these figures.

Response: Agree, well and CPT locations not sampled have been omitted from Figures 4.10 through 4.17.

28. **P4-33 Section 4.3.24** Provide an explanation as to why there did not appear to be any clear trend between BTEX and sulfate concentrations in August 1993. Why would the data be so erratic or non-comparable?

Response: Considering the numerous interactions between different consortia of bacteria, it is quite possible that the redox reactions for sulfate reduction were not mediated in all locations because the subsurface microorganisms were inhibited in some way. A definitive trend showing site-wide sulfate reduction in the vicinity of greatest hydrocarbon contamination was not evident (Figure 4.12). Depletion of other available electron acceptors likely caused sulfate reduction to become more predominant in 1994.

Pursuant to the above response, the following text was amended in Section 4.3.2.4 (in bold): "There does not appear to be any clear trend between BTEX and sulfate concentrations downgradient from the source (compare Figure 4.12 to Figure 4.5), near the leading edge of BTEX contamination in August 1993. However, localized sulfate reductions are seen in the source area. Figure 4.13 is an isopleth map showing the distribution of sulfate in ground water in July 1994. This figure includes data collected from monitoring wells in the source area north of Sixth Street in December 1993/January 1994. These wells cover a small area and these data represent the only data available for this area. Comparison of

Figures 4.5 and 4.13 shows graphically that by July 1994, areas with elevated total BTEX concentrations had depleted sulfate concentrations. This is a strong indication that the rate of anaerobic biodegradation of the BTEX compounds through sulfanogenesis increased from 1993 to 1994. It is possible that the redox reactions required for sulfate reduction to proceed in the ground water environment in 1993 were not microbially mediated, and that the depletion of other available electron acceptors by 1994 likely increased the importance of sulfate reducing processes."

29. **P5-2 Section 5.2 Bottom of Final Paragraph** The text states that the isopleth maps for DO and nitrate compounds were superimposed and combined to form a "total" electron acceptor isopleth map. Please provide a figure to show what this would look like. Also, see Montgomery Watson comment #3.

Response: Agree, a superimposed isopleth map for oxygen and nitrate has been included in Section 5. The solute transport model was originally set up to use only dissolved oxygen as an electron acceptor. This model predicted a plume size and shape that extended nearly twice as far as the observed plume in 1994. BTEX biodegradation predictions were grossly underestimated by assuming aerobic biodegradation only. Based on these results, it was clear that dissolved oxygen was not the only electron acceptor being utilized for BTEX biodegradation at the site, and in order to calibrate the solute transport model, it was necessary to include another degradation mechanism. Denitrification processes are the most thermodynamically favorable after aerobic respiration. Upon incorporating nitrate into the solute transport model, the predicted plume in 1994 was a better match to the observed data, and Parsons ES was able to calibrate the model.

30. **P5-6 Section 5.4.3** The text states the highest total-dissolved BTEX concentrations obtained from laboratory analytical data for the period through August 1993 was used for model development. Be more specific as to how the Appendix D concentration values were arrived at. My first assumption was that the highest BTEX concentration within a grid would be used in the model, however, some other method of determining the BTEX value for each grid square was used. Please explain in the text.

Response:

Agree, additional explanation for generation of the modeled total BTEX plume has been added to Section 5.4.3. Ground water analytical data often were collected in multiple sampling events from 1992 to 1993. conservative total BTEX isopleth map for 1993 was generated by picking the highest total BTEX concentrations at well locations sampled in 1992 to 1993. This conservative isopleth map was then used in model development by superimposing the model grid over it, and extracting representative total BTEX concentrations for the model based on the isopleth contours that intersected a given model cell. Total BTEX concentrations used in the model, and shown in Appendix D, are an estimated average concentration of all isopleth lines in a model cell. The highest concentrations at the site, per se, were not necessarily used for each model cell because a single point or single isopleth line was not considered representative of total BTEX concentrations over the entire 85' by 110' model cell. This method produced a calibrated model plume in 1993 that closely matched observed data in 1993 (Figure 5.2 vs. Figure 4.4). In fact, the calibrated total BTEX plume is slightly higher in both concentration and extent.

Section 5.4.3 now has the following addition: "The BTEX data from Figure 4.4 were used in model development by superimposing the model grid over the isopleth contours. The total BTEX concentrations used in the model, and shown in Appendix D, are estimated average concentrations of all the isopleth lines intersecting the boundaries within each model cell. The highest concentration isopleth lines were not used for allocating BTEX concentrations to model cells because a single isopleth concentration was not representative of the average total BTEX concentrations over the entire 85foot by 110-foot model cell. Figure 5.2 shows the distribution of the BTEX plume as calculated by the Bioplume II model for T=0 for all models. Comparison of Figures 4.4 and 5.2..."

31. P5-8 Top paragraph The units used for hydraulic conductivity in this section are in ft/s. Please make the presentation of conductivity values consistent between this section which discusses the model input parameters and the previous sections 3.3.3.2 and Table 3.1. Also, explain whether the Montgomery Watson slug test data was used to develop the range identified in this section. If not please explain. See comment #17.

Response: Agree, hydraulic conductivity values have been changed to consistent units Montgomery Watson slug test data were throughout the document. evaluated before generating a calibrated water table, but it was decided that the higher values of hydraulic conductivity measured by ES (Table 3.1) were more representative of the aquifer matrix through which the contaminant is traveling (described in response #17). Higher hydraulic conductivities also were conservative because plume migration distance increases in proportion to increased hydraulic conductivity.

Section 5.4.4 now has the following addition: 'Based on slug tests performed at the site, hydraulic conductivity varies from 1.08x10⁻⁴ ft/s to 6.08x10⁻⁴ ft/s. This is within the accepted range for sandy materials (Freeze and Cherry, 1979). Slug test results used for modeling do not reflect slug test data collected by JMM (1993) at MW-1. MW-1 was screened in a soil interval characterized by silty sands with a large interval (~4 ft) of clayey sand. Therefore, slug test data from MW-1 were not considered representative of the fine- to medium-grained sandy soils located around the screened monitoring wells used for Parsons ES slug tests in 1993. The sensitivity of the model to this parameter was evaluated during the sensitivity analysis described in Section 5.6."

32. P5-9 Section 5.4.5 First Paragraph The assumption at the bottom of this paragraph appears correct, that the oxygen was utilized first by aerobic bacteria and then anaerobic bacteria consumed nitrate as the next available electron acceptor. This assumption does not appear to have been followed when combining the DO and nitrate concentrations because the only place the nitrate would be effective as an electron acceptor is where the DO is equal to zero. See MW comment #3.

Response:

We feel that combining oxygen and nitrate concentrations throughout the model grid was appropriate. Theoretically, nitrate is not used for BTEX biodegradation until all modeled oxygen concentrations are depleted to low concentrations. However, significant nitrate reductions occurred in areas with significant oxygen reductions. These trends support the likelihood that denitrification will consistently occur following depletion of oxygen through aerobic biodegradation in all areas of BTEX contamination. Furthermore, both oxygen and nitrate react instantaneously with BTEX relative to the advective groundwater velocity in the aquifer (Borden and Bedient, 1986; J.T. Wilson, personal communication, 1994). Model simulations would be more accurate if instantaneous BTEX biodegradation mechanisms in the presence of nitrate (via denitrification) and other anaerobic electron acceptors (e.g., ferrous iron, sulfate and carbon dioxide) are incorporated into a ground The utilization of instantaneous aerobic and anaerobic water model. reactions in modeling will be expanded by Bioplume III [anticipated release to be in late 1995 (Rifai, 1995)], which will incorporate the instantaneous aerobic and anaerobic reactions using DO, nitrate, ferrous iron, sulfate, and carbon dioxide.

The following text was added after the first paragraph of Section 5.4.5: "The Bioplume II model was calibrated with DO as the only electron acceptor. The result of using DO as the only electron acceptor was a modeled BTEX plume that extended nearly twice as far (and past the Hill AFB boundary) downgradient than the plume observed in 1994. Based on these results, it was clear that DO is not the only electron acceptor being utilized for BTEX

biodegradation. Successful calibration of the Bioplume II model required the use of nitrate, which is the most thermodynamically favorable electron acceptor following oxygen. Furthermore, decreases in nitrate concentrations from anaerobic biodegradation processes were observed in areas with reduced DO concentrations (compare Figures 4.6 and 4.7 with Figures 4.8 and 4.9, respectively). This strongly suggests both denitrification and aerobic oxidation are important biodegradation mechanisms at the site. Although some localized areas on the fringe of the BTEX plume overestimated the actual rate of denitrification because of background DO concentrations, both aerobic oxygenation and denitrification of BTEX contamination were widely observed in the same areas. Therefore, simulating nitrate concentrations with DO concentrations in the model was not an overgeneralization of site electron acceptor potential (as might initially be presumed), but instead was an improved representation of site conditions. Related modeling initiatives to improve simulations of BTEX biodegradation in ground water systems are being accomplished by incorporating nitrate, and other potential anaerobic electron acceptors (e.g., ferric iron, sulfate, and carbon dioxide) into the model code, specifically within the code of the soon-to-be released Bioplume III ground water model (Rifai, 1995)."

'The loss of DO and nitrate in the Bioplume II model was conceptualized with aerobic bacteria using DO, and then with anaerobic bacteria using nitrate as the next available electron acceptor. This assumption is justified based on the observation that aerobic oxidation and denitrification are important biodegradation mechanisms at the site. Once utilized, DO and nitrate will react instantaneously with BTEX relative to the advective groundwater velocity in the aquifer (Borden and Bedient, 1986; Wilson, 1994)."

Furthermore, the second to last sentence in the fifth paragraph also has been omitted.

Because of the high degree of model sensitivity to the reaeration 33 P5-11 Section 5.4.7 coefficient, a better understanding of why the .003 day⁻¹ was used should be given. See MW comment #5.

Response: The reaeration coefficient of 0.003 day⁻¹ was originally estimated, based on other documented Bioplume modeling efforts (for example, Rifai et al., 1988). Use of the reaeration coefficient is justified at this site because of the shallow water table and the relatively high DO concentrations observed in site ground water. An anaerobic decay coefficient was not included in the model as a conservative assumption.

First-order biodegradation rate constant estimates for Hill AFB range from approximately 0.010 to 0.032 day (Wiedemeier et al., 1995). These estimates are an order of magnitude larger than the reaeration coefficient used in the Hill AFB model and suggest that the total of aerobic and anaerobic biodegradation of compounds is occurring at magnitudes much greater than accounted for. However, biodegradation rate estimates based on field data were unavailable at the time of modeling. biodegradation rates are simulated in the Bioplume II model through either reaeration or anaerobic decay coefficients.

Pursuant to the above response, the following text was amended to Section 5.4.7 as follows (in bold): "The reaeration coefficient is a first-order decay rate constant used by Bioplume II to simulate the replenishment of oxygen into the ground water by soil gas diffusion and rainwater infiltration. Recent data on first-order biodegradation rate coefficients in groundwater at Hill AFB suggest that biodegradation rates ranged from 0.010 to 0.032 day over the center and periphery of the groundwater contaminant plume (Wiedemeier et al., 1994). To be conservative, a first-order biodegradation rate coefficient of 0.003 day was used in this model. This rate coefficient was increased and decreased by one order of magnitude during the sensitivity analyses described in Section 5.6.

34. P5-14 &15 Section 5.5.2 Comparison of BTEX plume data derived up to August 1993 with that of July 1994 is very uncertain. Uncertainly arises from two primary factors: first, the sampling and analysis techniques are different between the two events, and second, the location of sampling, especially on the periphery of the plume was not consistent. These two factors make for a questionable calibration method described in this section.

Response: We disagree that differences between sampling techniques create a large uncertainty between data taken at two different times (as described in the response to comment #22). Although some wells sampled in 1993 were not re-sampled in 1994, the available data for 1994 are sufficient for describing the BTEX plume shape. Perhaps the greatest confusion arises on the representation of ground water BTEX contamination in 1994. monitoring wells at the front of the plume (EPA-82-F, -E, -N, -K, -O, and -H) had nondetectable BTEX concentrations (<1 ppb). Monitoring wells MW-11 and EPA-82-B on the sides of the plume also had nondetectable BTEX concentrations. Considering these peripheral wells, and the 21 other monitoring wells showing ground water BTEX contamination, we feel that an accurate representation of the available data is made by Figure 4.5 (and Figure 4.4), and that the ground water model calibration is accurate. Additional data are always preferable, however such data were not available during the generation of these figures.

Dashed isopleth lines in Figures 4.4 and 4.5 (as previously discussed in comment #24) have been included to show areas of uncertainty; however, the figures shown are the best representation of the available ground water BTEX data, and they are not unduly compromised by either different analytical methods or data interpretation. If a preferred method of data representation can be suggested by the reviewer, Parsons ES would consider using it.

A single sentence referring back to Section 4.3.1 was added, because this issue was justified in that section per the response to comment #22. The sentence has been added after the first sentence of the Section 5.5.2 and reads: "The extent of dissolved-phase BTEX contamination in 1993 and 1994 is described in Section 4.3.1."

35. **P5-27 Section 5.7.3** The reference to Figure 5.13 in the text should indicate that the results are for T=3 years. Then the later discussion of the plume disappearance at T=4 years would be more easily understood. I was a little mixed up expecting the T=4 years model results to be shown in Figure 5.13.

Response: Agree, the following text has been amended to the paragraph in Section 5.7.3 (in bold): "...Figures 5.13 and 5.14 show the results of this model for 1 and 3 years after the implementation of a 15-percent annual source removal technology. The initial 1 year prediction of plume migration suggests that the plume would extend as far as Cambridge Street at concentrations of 1 µg/L. By year 3 (Figure 5.14), the BTEX plume had undergone significant attenuation, including a complete reduction of BTEX contamination in the source area. By year 4, the plume had entirely disappeared. This plume disappearance at year 4 was caused by the reduction of the injection loading rates of modeled BTEX to 55 percent of the original loading rate, which was within the biodegradation capacity of the upgradient, influent electron acceptors and aquifer reaeration.

36. **P5-21 Section 5.7.1** Please show how the initial 3900 gm of dissolved-phase BTEX contamination was derived at T=0.

Response: This estimate was made by using the Bioplume II model output for "Hill-A" which describes the mass of dissolved-phase contamination for each time step.

The following text has been added after the second sentence in Section 5.7.1: "This estimate was calculated by Bioplume II, which summed all dissolved BTEX contamination over the Hill AFB model domain at time zero."

37. P6-1 Section 6.1 Last sentence contains a double negative, 'ho unacceptable'. Please reword.

Response: Agree, the sentence now reads: "Rather, this report focuses on the potential use of intrinsic remediation and source reduction technologies to reduce BTEX concentrations within the shallow ground water to levels that pose an acceptable risk to human health or the environment."

38. P 6-6 Second Paragraph Last Line Change the word "grade" to "degrade".

Response: Agree, the sentence now reads: "The DO introduced by biosparging can also be utilized effectively to aerobically biodegrade the dissolved contaminant mass."

39. P6-8 Section 6.2.3.2 At the bottom of the second complete paragraph the report states that other studies conducted at this site have addressed the potential impact of soil gas on residential areas and have determined that these pathways are incomplete. This statement is not true, the vapor exposure assessment below the residential area confirmed a completed pathway for soil gas emanating from the ground water contamination to within 4 feet of the surface. No pathway has been completed into the homes. State only in the report that other studies have addressed the potential impact of soil gas.

Response: Agree, the bottom of the fourth paragraph now reads: 'Other studies have addressed the potential of soil gas and have determined that pathways to residential structures are incomplete."

40. **P6-9 Section 6.2.3.3** Write out the full wording of Point of Compliance in the first sentence. The designation of the pond referenced should be Pond 5 not Pond 3. See previous comment #14.

Response: Agree, the first paragraph now reads: "The stormwater drain located along Cambridge Street has been identified as the point of compliance (POC) for ground water remedial activities because this appears to be the most likely point of exposure for migrating contamination to impact human or ecological receptors. Migration to and discharge of contaminated shallow ground water into the stormwater system could complete an exposure pathway to human or ecological receptors via dermal contact or possible ingestion. The stormwater drain outfall into Pond 5 is an accessible and well-defined location for monitoring and for demonstrating compliance with protective ground water quality standards, such as federal MCLs."

41. **P6-9 Section 6.2.3.3 Second paragraph** The goal statement indicating that the remediation goal includes restricting long-term ground water use is incorrect. Restricting ground water use is a means for preventing exposure but in itself is not a goal of Hill AFB. Please reword.

Response: Agree, the remediation goal paragraph has been amended as follows (in bold): "This remedial strategy would be consistent with remediation requirements set forth by the State of Utah. The State recognizes that compliance with

promulgated, single-point remediation goals is not necessary if site-related contamination does not pose a threat to human health or the environment (i.e., the exposure pathway is incomplete). Thus, the magnitude of required remediation in areas that can and will be placed under institutional control is different from the remediation that is required in areas that may be available for unrestricted use. This means that viable remedial alternatives, which includes long-term restrictions on shallow ground water use, must be able to achieve concentrations that minimize plume migration and expansion and potential human risk associated with ground water contact. The remediation goal for shallow ground water impacting the Cambridge Street stormwater drain is attainment of federal MCLs for each of the BTEX compounds, as listed in Table 6.1. Although it is unlikely that stormwater would be ingested by humans, this level of long-term protection is appropriate for a residential area."

Furthermore, the fourth paragraph of the second paragraph in Section 6.2.3.3 has been omitted.

4. P6-10 Top Sentence This sentence is not necessarily accurate. The soil gas emanating from the contaminated shallow ground water below the residential housing area does have a completed pathway to the surface. However, no human health risk is associated with this completed pathway based upon results of the vapor exposure assessment (VEA). See comment #39.

Response: Agree, changes to the top paragraph on P6-10 now reads (in bold): "In summary, available data indicate that no potential exposure pathway involving shallow ground water is complete under current conditions, with the exception of soil gas emanating from the ground water to within 4 feet of the surface. The exposure route for soil gas was identified in a vapor exposure assessment performed in other site characterization studies (Gemperline, 1995). Although an exposure pathway to the surface is completed from BTEX contamination volatilizing from ground water, human risk was calculated to be inconsequential. Other than soil gas, no potential exposure pathway involving shallow ground water will be complete under future land use assumptions provided use of ground water as a potable or industrial source of water is prohibited by institutional controls within and downgradient of the source area to the Cambridge Street stormwater drain. Thus, institutional controls are likely to be a necessary component of any ground water remediation strategy for this site. The required duration of these institutional controls may vary depending on the effectiveness of any remedial technology at reducing contaminant mass and concentrations in the ground water. If federal MCLs are exceeded in the Cambridge Street stormwater discharge, remediation of stormwater will be required to prevent pathway completion."

43. **P6-10 Section 6.2.4** Include the word "of" in the third sentence.

Response: Agree, the sentence now reads: 'Screening was conducted systematically by considering the objectives of the AFCEE intrinsic remediation demonstration, the physiochemical properties of BTEX compounds, and other site-specific characteristics such as..."

44. **P6-15 Section 6.2.4** The acronym most commonly used for the industrial waste water treatment plant is (IWTP). Please change the IWWTP to IWTP for consistency with Hill's use of the acronym. See also P6-13 Table 6.2.

Response: Agree, this change has been made.

45. **P6-14 Table 6.2** Please change reference to bioventing system currently operating in source area to read "Pilot test system currently operating in source area."

Response: Agree, this change has been made.

46. **P6-15 Section 6.3.1** Please show how the stated 5% annual reduction in source BTEX using the current LNAPL removal system was derived. Show calculations as to how much LNAPL is theorized to be present, how much BTEX is present, how much is removed each year by the LNAPL removal operations. Also, explain whether a 5% removal rate per year can realistically be maintained for more than a few years or whether the rate would most likely decrease over time.

Response: The following two paragraphs have been added after the second paragraph of Section 6.3.1: "A 5-percent annual LNAPL recovery/reduction was selected as a reasonable removal rate of BTEX concentrations emanating from mobile LNAPL at the site. A 5-percent annual BTEX source recovery/reduction could accomplish this. The most important physical processes contributing to BTEX source weathering are volatilization and dissolution. The dissolution of BTEX compounds from LNAPL is accomplished through interfacial dissolution at the fuel/water interface and dissolution into precipitation that is percolating downward."

"The 5-percent annual BTEX loss was selected for comparison purposes only, and is not intended to reflect an actual rate of BTEX source reduction. On the basis of previous fuel-spill investigations in similar soils at Wurtsmith AFB, BTEX constituents in mobile LNAPL decreased at rates exceeding 70 percent per year through natural weathering (Parsons ES, 1995). Approximately 1,500 gallons of JP-4 released into a shallow, sandy aquifer at Wurtsmith AFB in October 1988 had weathered to low residual-phase concentrations (<150 µg/L) without measurable free-product by June 1991. BTEX compounds in LNAPL are being similarly weathered at UST 870, as seen by a decrease in BTEX concentrations in LNAPL over time (Table 4.1). The LNAPL sample taken from MW-10 exhibited a 70-percent loss of BTEX constituents relative to fresh LNAPL (JP-4). Hence, the partitioning strength of BTEX compounds in LNAPL contamination is diminishing not only from engineered removal (bioslurpers), but also from natural weathering. Regardless of the value used to estimate annual BTEX source reductions, the calibrated model predicts that groundwater will not migrate past the base boundary, with the front of the plume stabilizing near Cambridge Street (assuming current conditions are not compromised with further fuel spills). The BTEX plume is expected to disappear from overwhelming natural attenuation mechanisms once BTEX source concentrations are reduced to approximately 50 percent of their current concentration."

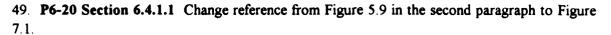
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47. P6-16 Top paragraph Remove the word "of" from the second to last sentence.

Response: Agree, the sentence now reads: 'Based on model predictions, the BTEX plume will approach the Cambridge Street storm drain in approximately 1 to 4 years at concentrations exceeding 1 μg/L."

48. P6-17 Sections 6.3.2 Bottom paragraph states that during high-flow conditions in the stormwater drain from heavy precipitation events that a portion of the stormwater would pass over the proposed weir and discharge directly into the pond. Please clarify what is meant by a "portion" of the discharge. What happens to the other portion? Does the portion over the low flow weir get treated by the sparge unit?

Response: Agree, this paragraph has been rewritten as follows: "A low-flow weir would be constructed at the stormwater discharge point to convey stormwater through the sparge tank at rates the system is capable of handling. In the event that stormwater runoff exceeds the capacity of the weir (and the sparge tank system), the excess stormwater will be discharged directly to collection ponds without treatment. Although excess water would not be treated, the anticipated risk of BTEX contamination would be very low due to dilution of the BTEX compounds."



Response: Agree, this reference in the second paragraph now reads: 'However, the model predicted a potential exceedance of the federal MCL for benzene at the POC wells (Figure 7.1) and..."

50. **P6-22 Section 6.4.1.1** The top paragraph states that source removal will continue for 8 years. Did the Bioplume model assume we could remove 5 percent of the source continuously for 8 years? If so, is this a good estimate? Please quantitatively present this in the document. See comment # 46.

Response: In response to comment #46, the following sentence has been added after the first sentence of the last paragraph of Section 6.4.1.1: "The 8-year time frame is a reasonable source removal goal based on predictions of successful source removal, both engineered and natural, that will approach, or exceed, 5 percent annually (Section 6.3.1)."

51. P6-23 Section 6.4.2 The discussion of Alternative 2 in this section leads me to believe the storm water treatment system is to be constructed and operated from the outset of the corrective action process. Whereas, section 6.3.2 which describes Alternative 2 gave me the impression that only if monitoring of the storm water drain outfall indicated the BTEX MCLs were exceeded would the treatment system be put in place. Please clarify the intentions of this alternative and assure consistency between these two sections. Also, correct formatting error on page 6-24.

Response: Agree, the following text has been amended in Section 6.4.2.1 (in bold): "The effectiveness of Alternative 1 is enhanced under Alternative 2 by ensuring that if stormwater becomes contaminated, an air stripping unit will be installed to treat ground water to levels below federal drinking water MCLs before it is discharged to the stormwater pond. As stated in Section 6.3.2, the use of a stormwater air stripper would be contingent on BTEX concentrations exceeding MCLs at the stormwater discharge point. Air stripping technologies, including sparging tanks, are proven and reliable systems for reducing BTEX compound concentrations in water by more than 95 percent. The use of a low-flow diversion weir to treat only more concentrated BTEX-contaminated stormwater will reduce the size and complexity of the air stripping system. This alternative also complies with the program goals because intrinsic remediation remains the predominant decontamination method at the site."

The formatting error on page 6-24 has been corrected.

52. **P6-26 Section 6.4.3.1** Last sentence of the second paragraph states, 'based on flux testing at other fuel contaminated sites, vapor migration is not anticipated." Flux chamber sampling at this site has confirmed a pathway for BTEX compounds to the surface exists. Please remove the statement from this report.

Response: Agree, this sentence has been removed.

53. General Comment: Alternative 3 Same concern as in comment #46, please substantiate what 15% removal quantitatively would mean at this site. Also, due to the results of previous total fluids removal techniques and bioslurping study, coupled with the fact that bioventing within the residential area is not an option based upon site flux testing data, I don't believe a 15% removal rate of the BTEX plume continuously over 4 years is a realistic assumption. Must support the assumption better to use it.

Response: Agree, the following paragraph has been included after the first paragraph of Section 6.4.3.1 and reads as follows: 'Conceptually, this 15-percent annual reduction in a BTEX source from mobile LNAPL will be obtained from both natural weathering and increased engineered removal. Natural weathering rates of BTEX compounds in mobile LNAPL under similar conditions can be substantial (Section 6.3.1). Similar weathering losses of JP-4 contamination are occurring at Site UST 870. The assumed 15-percent annual reduction of BTEX constituents in mobile LNAPL does not necessarily represent actual weathering rates, but show potential LNAPL reduction rates as a result of increased LNAPL removal along with natural weathering. More intensive source removal could help achieve protectiveness approximately 4 years sooner than that under Alternative 1. The model predicts that with more intensive source removal, the BTEX plume will be less concentrated approaching the Cambridge Street stormwater drain, and this exposure pathway may not be completed."

54. P7-2 Top sentence Change Pond 3 to Pond 5.

Response: Agree, the reference now reads: "The second network of ground water monitoring points will consist of three POC wells and a POC sampling point at the Pond 5 outfall of the stormwater drain located along Cambridge Street."

55. P7-2 Section 7.2.1 CPT-40 is recommended as a LTM monitoring point. There is concern from past experience that data collected from a CPT placed monitoring point is not comparable with a standard monitoring well installed by other methods. Additionally, no explanation as to why this point needs to be monitored is given and I am not sure whether the this point exists any longer or whether it is capable of being sampled. Please address these issues before recommending use to this point.

Response: Agree, the following text has been added (in bold): 'Eight ground water monitoring wells placed upgradient, within, and immediately downgradient of

the existing BTEX contaminant plume will be used to monitor the effectiveness of intrinsic remediation in reducing total contaminant mass and minimizing contaminant migration. Figure 7.1 shows the proposed locations of these wells. One new and four existing monitoring wells (MW-04, MW-05, EPA-82-D and MW-10) will be used as LTM wells to monitor natural attenuation within the anaerobic treatment zone and BTEX concentrations in the source area. In the event that the MW-04 screen is too shallow to permit collection of accurate ground water data, monitoring well EPA-82-I, MW-01, or MW-14 should be considered as a substitute LTM location. One new LTM well should be placed within the aerobic treatment zone to monitor natural attenuation within this zone. One new LTM well should be placed downgradient of the BTEX plume. Sampling and analysis of the downgradient LTM well (and the POC wells) will be useful in monitoring changes in ground water chemistry through time and will facilitate early detection of plume migration. Because the velocity of the dissolvedphase BTEX plume is retarded relative to the advective ground water velocity and the velocities of the electron acceptors are not, depleted DO, nitrate, and sulfate concentrations, and elevated ferrous iron and methane concentrations will advance in front of the BTEX plume. Thus, changes in the concentrations of the electron acceptors can be used to provide early warning of BTEX plume encroachment on the LTM and POC wells."

"An existing CPT monitoring point (CPT-40) should be used as an upgradient LTM well. CPT-40 was selected as an upgradient LTM point because it has historically been free of ground water contamination and is suited for monitoring background levels of ground water electron acceptors, pH, and oxidation/reduction potential. The different well diameter of CPT-40 compared to the other proposed LTM wells is not a sampling issue because background levels of ground water parameters are presumed to be uniform throughout the shallow aquifer. In the case that CPT-40 is destroyed or inaccessible, a new LTM well (described in Section 7) well be installed instead."

56. P7-2 Section 7.2 Last statement infers that any detection of BTEX in the POC wells will trigger further evaluation of remedial options. I thought any detection of BTEX compound concentrations above the MCLs would be the trigger for evaluation of other options. Please clarify.

Response: Agree, the last sentence in Section 7.2 now reads: 'Should BTEX compounds be detected in POC wells above MCLs, other remedial options will be evaluated."

57. P7-3 Figure 7.1 Eliminate extraneous symbols and sampling points from this figure that do not deal with the monitoring plan being proposed. Change Pond 3 to Pond 5 and include a boundary line for Hill AFB property. Inclusion of street names and the elementary school would be helpful as well.

Response: These changes have been incorporated into Figure 7.1

58. P7-5 Section 7.3.2 The statement, 'If the data collected at any time during the monitoring period indicate the need for additional remedial activities at the site..." is too broad and undefined. Either eliminate this statement or indicate what data and concentration levels would indicate the need for additional remedial activity.

Response: Agree, the last sentence of Section 7.3.2 now reads: "If the data collected at any time during the monitoring period indicate the need for additional remedial activities at the site (i.e., if concentrations of BTEX exceed MCLs at POC locations) sampling frequency should be adjusted accordingly."

59. General Comment: Change references to Pond 3 and all figures designating Pond 3 to read Pond 5 throughout the document. See comment #s 57, 40 and 14.

Response: Agree, these changes have been applied globally throughout the document.

60. General Comment: In Section 8 and other locations within the document, recommendations are made as to the final preferred actions. It is probably wise to reference the Air Force as making those recommendations rather than the contractor, as the ultimate responsibility for the report and site is the Air Force.

Response: Agree, all recommendations will be referred to as Air Force recommendations.

61. P7-2 Section 7.2.1 Suggest we not recommend MW-04 as an LTM well. Installation problems caused the well to be screened very shallow below the water table. If seasonal fluctuations in the ground water drop the water table, this well may not be a useful data collection point. I'd recommend EPA-82-I, MW-01 or MW-14.

Response: Water level fluctuations may be a concern in sampling LTM wells; however, EPA-82-I is screened under a shallower interval than MW-04 because it has a shorter screen length. In addition, all the monitoring wells appear to be screened in approximately the same relative interval, suggesting that water table drops may occur in all local wells to the same degree. Based on positioning of MW-4, we recommended the same well for an LTM location.

In response to the above comment, the following text has been added into the first paragraph of Section 7.2.1: "In the event that MW-04 screen is too shallow to permit an accurate ground water sampling, monitoring well EPA-82-I, MW-01, or MW-14 should be considered as a substitute LTM location."

II. Response to comments submitted by Montgomery Watson(MW):

1. The model does not seem to be conservative overall because the continuing source term and the biodegradation assumptions are not conservative. If the source term is underestimated and the degradation rate is overestimated, the model could predict a much more favorable situation than may exist.

Response: We disagree that the model is not conservative because of the biodegradation assumptions used. The suggestion of lowering the degradation coefficient to a lower value, or even eliminating it, is unjustified considering site data. Section 4 illustrates in detail that numerous electron acceptors such as oxygen, nitrate, sulfate, ferric iron, and carbon dioxide are being utilized to varying degrees at Site UST 870 for the microbial destruction of fuel contaminants. Background DO levels of a least 5 mg/L were reduced to below 1 mg/L in the center of the BTEX plume. Reduction of DO alone provides sufficient evidence that biodegradation is occurring and the use of a biodegradation coefficient is warranted. Without a biodegradation coefficient, the plume would travel practically unrestrained toward downgradient receptors (and extending past the base boundary).

The reaeration coefficient was obtained as described in the response to Air Force comment 33. Hence, it is highly likely considering the amount of biodegradation occurring at the site and the number of electron acceptors used, that the reaeration coefficient has been underestimated. Conservatism of biodegradation assumptions was further assumed by using only DO and nitrate as electron acceptors in the model. Because it is likely that biodegradation of site contaminants is underestimated, it is also likely that more biodegradation is occurring than suggested by the model, making it conservative overall.

2. In your assumptions, the presence of measurable free-phase LNAPL is defined as the source area. Residual LNAPL could also act as a source. A larger source area should be used for a more conservative model.

Response: Residual LNAPL contamination was not included as a potential source in the model because little residual-phase soil contamination exists outside of areas estimated to contain mobile LNAPL. This is illustrated when comparing Figures 4.1 and 4.2 in the model. Residual BTEX concentrations downgradient from the LNAPL are below 50 mg/kg and would not be a substantial source of contamination through partitioning from soil to infiltrating waters. As a safety factor, the calibrated model used higher concentrations of dissolved BTEX in the source than have been observed to

further establish a conservative bias to the model. This elevated dissolved BTEX parameter helps to offset the effects of any potential residual-phase contamination that was not accounted for by starting model assumptions.

3. Are the degradation assumptions really as conservative as you suggest? Doesn't denitrification take place only in anaerobic areas, therefore, it should not take place simultaneously with aerobic degradation. By adding the nitrate and oxygen together around the periphery of the plume you may overestimate degradation if the two processes do not occur simultaneously. A more conservative model scenario without nitrate should be added for comparison. Aerobic biodegradation is the only process we are sure is happening on the edges of the plume.

Response: Model simulations using DO as the only electron acceptor were run during initial model calibrations. Results of these simulations predicted plume shapes and concentrations greatly in excess of observed conditions. It became evident during the model calibration that additional biodegradation mechanisms, such as denitrification, are occurring at the site. Inclusion of the effects of denitrification into the ground water model created a better match between observed data and modeled results.

Denitrification was modeled by transforming nitrate concentrations into oxygen equivalent concentrations, as described in Section 5 of the EE/CA. The underlying assumption made was that biodegradation potential was great enough that available oxygen and nitrate concentrations both would be utilized. This assumption is supported by comparisons of Figures 4.6 and 4.7 to Figures 4.8 and 4.9, which qualitatively depict nitrate reductions occurring in the same area of DO reductions. Localized overestimation of biodegradation by including nitrate as an electron acceptor may occur; however, overall, geochemical evidence suggests that denitrification is a predominant process occurring at the site. In modeling, BTEX loss theoretically occurs first through aerobic oxidation. When the oxygen is depleted, nitrate remains to degrade more BTEX through denitrification. This is the biodegradation sequence mimicked in the ground water model.

4. The report should note that the overall assimilative capacity is a best case estimate. The reactions are very specific to geochemical conditions and are not guaranteed to happen. The assimilative capacity calculations were done using the highest observed electron acceptor or metabolic byproduct concentrations. Therefore, it is likely to be an overestimate. For example, degradation by iron reduction is calculated based upon the highest ferrous iron concentrations observed (50.5 mg/L). From Figures 4.10 and 4.11, typical ferrous iron concentrations in the source area are 5-10 mg/L. The assimilative capacity due to denitrification was calculated using a background nitrate concentration of 17 mg/L. This value is very high and doesn't appear to be representative of the background nitrate levels shown on Figures 4.8 and 4.9. A value which represents the average background value should be used.

Response: Assimilative capacity is an estimate of the biodegradation potential of ground water. Hence, this estimate must be based on background concentrations of individual electron acceptors. In the case of ferrous iron, ferrous iron is a reduced species of iron generated after ferric iron is used in iron reduction processes. As stated in section 4.3.2.3, the highest concentration of ferrous iron is indicative of the potential for iron reduction because it is formed only under reducing environments (ferrous iron is typically non-existent in aerobic environments). The highest levels of ferrous iron will occur in locations of greatest anaerobic activity, such as in the center of the plume. Therefore, we feel that the ferrous iron content of 50.5 mg/L at MW-02 is representative of the iron-reducing capacity of ground water at the site. Assimilative capacity is not connotative of average degradation potential. Biodegradation capacity through methanogenesis is predicted through the same means.

In terms of the other electron acceptors, such as nitrate, background concentrations outside of the influence of BTEX biodegradation must be used to show uninfluenced, background electron acceptor concentrations. Otherwise, the assimilative capacity of the ground water cannot accurately be gauged. For these reasons, we feel that substituting average values for maximum background values would not accurately describe the overall ability of ground water to biodegrade compounds through aerobic and anaerobic mechanisms.

5. The document doesn't describe where the reaeration coefficient comes from. It seems high, considering the site is covered with a tight clay layer that is sufficient to keep the contaminant vapors from reaching the residents. A lower or zero reaeration value may be more appropriate and conservative. In any case, the source or rationale for the reaeration value used should be stated in the report.

Response: Please see the response to MW comment #1.

INTRINSIC REMEDIATION

ENGINEERING EVALUATION/COST ANALYSIS

for

UST SITE 870

HILL AIR FORCE BASE

OGDEN, UTAH

June 1995

Prepared for:

AIR FORCE CENTER FOR ENVIRONMENTAL EXCELLENCE BROOKS AIR FORCE BASE SAN ANTONIO, TEXAS

AND

HILL AIR FORCE BASE OGDEN, UTAH

Prepared by:

Engineering-Science, Inc. 1700 Broadway, Suite 900 Denver, Colorado 80290 the mouth of the stormwater drain that runs along Cambridge Street be used to monitor the long-term migration and degradation of the dissolved-phase BTEX plume. Regular sampling and analysis of water from these sampling locations will allow the effectiveness of intrinsic remediation to be monitored and should allow sufficient time to implement hydraulic controls to contain the plume if BTEX is detected at the POC sampling locations. The LTM wells and POC sampling locations should be sampled on a semiannual basis for at least 13 years. If the data collected during this period supports the anticipated effectiveness of intrinsic remediation, the sampling frequency can be reduced to once every year, or eliminated. Ground water samples should be analyzed for the parameters described in Section 7 of this report. If BTEX concentrations in water from the POC sampling locations are found to exceed promulgated maximum contaminant levels, additional corrective actions should be taken to remediate ground water at the site, as described in this report.

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SECTION 1

INTRODUCTION

This report was prepared by Parsons Engineering Science, Inc. (Parsons ES) [formerly known as Engineering Science, Inc. (ES)] and presents the results of an engineering evaluation/cost analysis (EE/CA) conducted to evaluate the use of intrinsic remediation (natural attenuation) with long-term monitoring (LTM) for remediation of fuel-hydrocarbon contamination dissolved in ground water at underground storage tank (UST) Site 870, Hill Air Force Base (AFB), Utah. Previous investigations determined that JP-4 jet fuel had been released into the soil and shallow ground water at the site. The main emphasis of the work described herein was to evaluate the potential for intrinsic degradation mechanisms to reduce dissolved-phase benzene, toluene, ethylbenzene, and xylene (BTEX) concentrations in ground water to levels that are protective of human health and the environment.

1.1 SCOPE AND OBJECTIVES

Parsons ES, in conjunction with researchers from the United States Environmental Protection Agency (USEPA) Robert S. Kerr Environmental Research Laboratory (RSKERL), was retained by the United States Air Force Center for Environmental Excellence (AFCEE) to conduct site characterization and ground water modeling in support of intrinsic remediation with LTM at UST Site 870.

The scope of work for this project included the following tasks:

- Reviewing existing hydrogeologic and soil and ground water quality data for the site;
- Conducting supplemental site characterization activities to determine the nature and extent of soil and ground water contamination and to collect geochemical data to demonstrate the occurrence of intrinsic remediation;
- Developing a conceptual hydrogeologic model of the shallow saturated zone, including the distribution of contaminants and probable contaminant pathways;
- Determining if intrinsic processes of contaminant destruction are occurring in ground water at the site;

- Performing contaminant fate and transport modeling based on site hydrogeologic conditions using the Bioplume II model;
- Evaluating a range of model input parameters to determine the sensitivity of the model to these parameters and to consider several contaminant fate and transport scenarios;
- Determining if naturally-occurring processes are sufficient to minimize BTEX plume expansion so that ground water quality standards can be met at a downgradient point of compliance (POC);
- Conduct a preliminary exposure assessment for receptors potentially exposed to fuel hydrocarbon contamination in ground water;
- Developing remedial action objectives (RAOs) and reviewing available remedial technologies;
- Using the results of modeling to recommend the most appropriate remedial option based on specific effectiveness, implementability, and cost criteria; and
- Providing a LTM plan that includes LTM and POC well locations and a sampling and analysis plan (SAP).

Site characterization methods used to evaluate intrinsic remediation included Geoprobe® sampling of ground water near existing cone penetrometer testing locations, soil borehole drilling, soil sample collection and analysis, monitoring well installation, and sampling and analysis of ground water from newly installed and existing monitoring wells.

Site-specific data were used to develop a fate and transport model for the site using Bioplume II and to conduct a preliminary exposure assessment. The Bioplume II model was used to simulate the movement and degradation of BTEX in the shallow saturated zone under the influence of advection, dispersion, sorption, and biodegradation. As part of the EE/CA, this modeling effort had three primary objectives: 1) to predict the future extent and concentration of a dissolved-phase contaminant plume by modeling the combined effects of advection, dispersion, sorption, and biodegradation; 2) to assess the possible risk to potential downgradient receptors by conducting a preliminary exposure assessment; and 3) to provide technical support for the intrinsic remediation with LTM remedial option at regulatory negotiations, as appropriate.

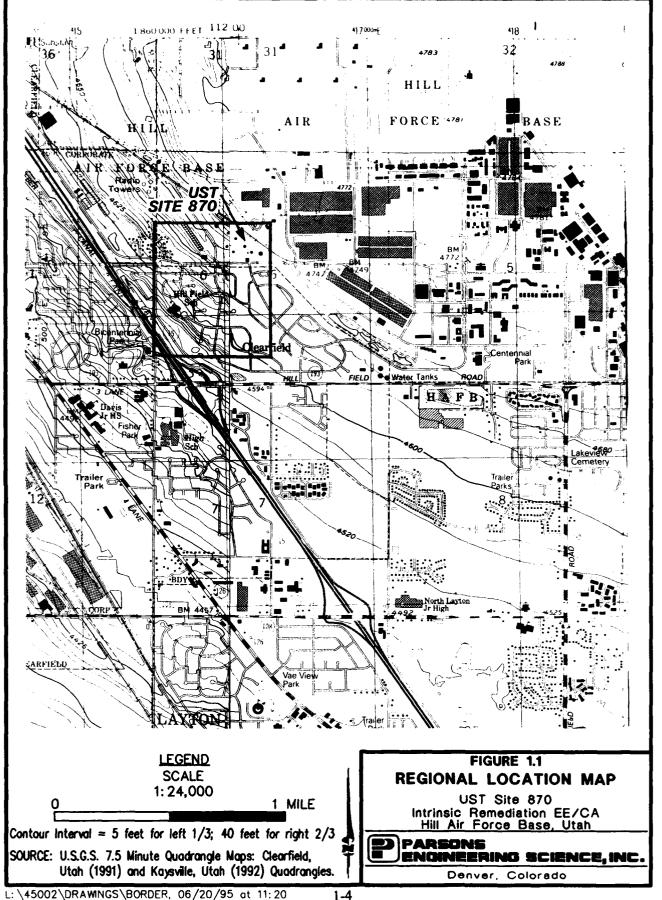
Several remedial options were evaluated as part of this EE/CA, including light nonaqueous-phase liquid (LNAPL) removal; soil vapor extraction; bioventing, hydraulic containment; and intrinsic remediation with LTM. Hydrogeologic and ground water chemical data necessary to evaluate the various remedial options were collected under this program; however, field work was designed to collect the data required by the Bioplume II model and

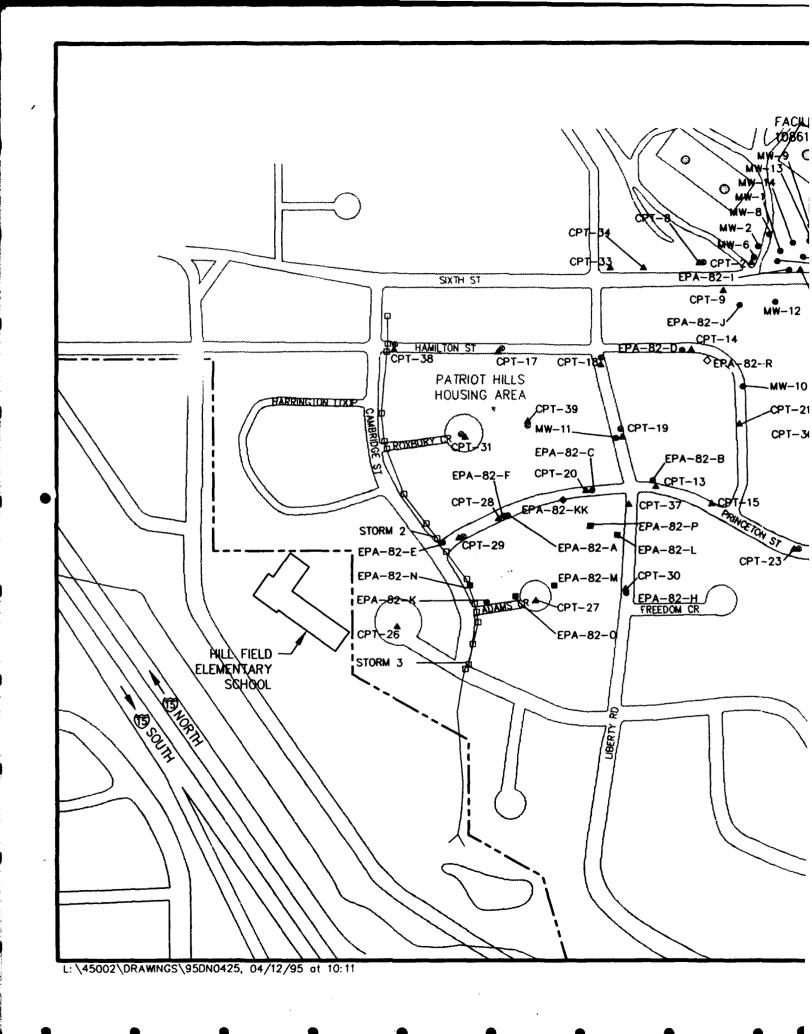
to support the intrinsic remediation with LTM remedial option for restoration of fuel-hydrocarbon-contaminated ground water.

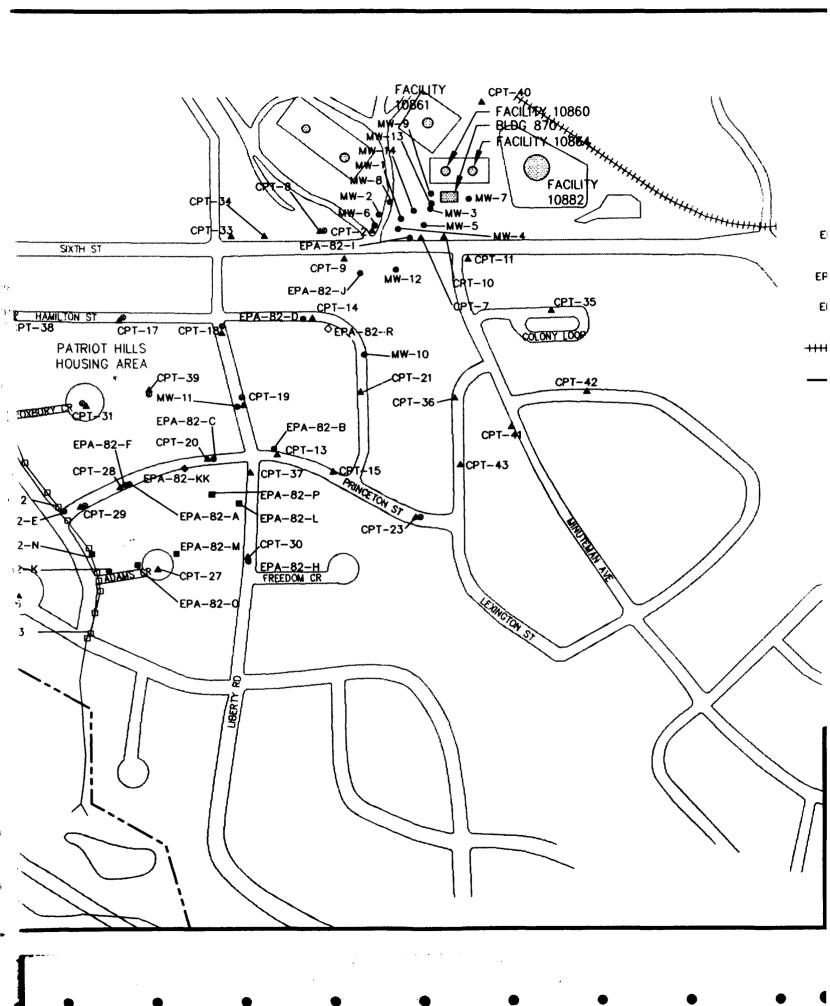
This report contains nine sections, including this introduction, and five appendices. Section 2 summarizes site characterization activities. Section 3 summarizes the physical characteristics of the study area. Section 4 describes the nature and extent of soil and ground water contamination and the geochemistry of soil and ground water at the site. Section 5 describes the Bioplume II model, the site conceptual model, lists model assumptions and input parameters, and describes sensitivity analyses, model output, and the results of the Bioplume II simulations. Section 6 presents a comparative analysis of remedial alternatives. Section 7 presents the LTM plan for the site. Section 8 presents the conclusions of this investigation and provides recommendations for further work at the site. Section 9 lists the references used to develop this document. Appendix A contains boring logs, monitoring well completion diagrams, and slug test results. Appendix B contains ground water elevation data and information on the seasonal variation in ground water flow at the site. Appendix C presents soil and ground water analytical results. Appendix E contains gridded model input parameters and water table calibration results. Appendix E contains Bioplume II model output on a diskette in ASCII format.

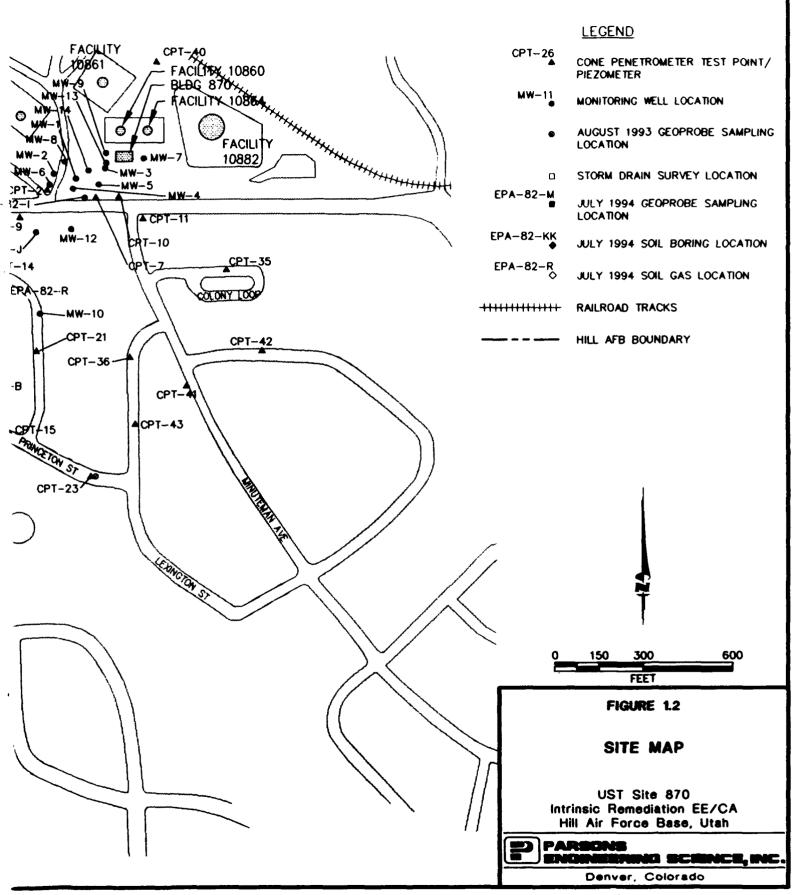
1.2 FACILITY BACKGROUND

Hill AFB is located at 41°07'N latitude, 111°58'W longitude on a bench of the Wasatch Mountains on the edge of the Great Salt Lake Basin. UST Site 870 is located in the southwestern corner of Hill AFB, Utah. Figure 1.1 is a regional location map showing the location of UST Site 870 relative to Hill AFB and the surrounding area. Figure 1.2 is a detailed site map showing UST Site 870 and the immediately adjacent area. UST Site 870 encompasses the area immediately downgradient from and adjacent to the former location of UST 870.0. This site is referred to as Site EGSS by the Utah Division of Environmental Response and Remediation (DERR), and as Site Code ST61 under the Air Force Installation Restoration Program (IRP). For the purposes of the work described herein, UST Site 870 refers to the area shown in Figure 1.2. This area includes the base fuel tank farm which consists of nine aboveground storage tanks (ASTs) used to store JP-4 and diesel fuel. A portion of the Patriot Hills base housing area located southwest of the AST farm, is also included with the site.









1.2.1 Operational History

UST Site 870 is located at one of the base fuel tank farms. This tank farm is bounded on the south by Sixth Street and the Patriot Hills housing area (Figure 1.2). Building 870 at the tank farm serves as the command and logistical support center for the dispensing of JP-4 to the flightlines. Several ASTs are located directly north of Building 870. The Patriot Hills housing area consists of military residential housing. Warehouses, offices, and other large structures are located east and west of the tank farm. Hill Field elementary school is located immediately southwest of the housing area near the base's southwestern property boundary.

UST 870.0 was a 1,000-gallon tank used to store condensate and off-specification JP-4 generated by activities at an adjacent filter stand. UST 870.0 was excavated and removed in May 1991 and upgraded with a new double-walled steel UST that was equipped with leak-detection equipment. The new UST serves the same purpose as UST 870.0.

Soil and ground water contamination was observed during removal of UST 870.0. Several site investigations were conducted by Montgomery-Watson, Inc. (MWI) [formerly James M. Montgomery Consulting Engineers, Inc. (JMM)] in response to this contamination. The results of these investigations are presented in several reports, including:

- Site Characterization Report (JMM, 1991)
- Free Product Letter Report (JMM, 1992a)
- Pumping Tests and Product Thickness Test Letter Report (JMM, 1992b)
- Remedial Options Letter Report (JMM, 1993a)
- Investigation Summary Report (JMM, 1993b)

The site-specific data presented in Sections 3, 4, and 5 are based on a review of these documents and on data collected by Parsons ES and researchers from the RSKERL under this program. A synopsis of site characterization activities conducted prior to implementation of the field work described in this report is provided in the 1993 Investigation Summary Report prepared by JMM (1993b).

1.2.2 Current Remedial Activities

Current remedial activities at UST Site 870 include active and passive light non-aqueous phase liquid (LNAPL) recovery. Active mobile-phase LNAPL recovery is being accomplished

using a QED® specific-gravity skimmer pump installed in a monitoring well and has been conducted since June 1992. Passive LNAPL recovery is also being performed in selected wells by using Soak Ease® absorbent pads enclosed in a stainless steel perforated bailer. To date, about 700 gallons of LNAPL has been recovered using these systems. Water and LNAPL levels are measured monthly to provide information about LNAPL thickness and ground water level fluctuations.

SECTION 2

SITE CHARACTERIZATION ACTIVITIES

To meet the requirements of the intrinsic remediation demonstration, several investigative techniques, including soil and ground water sampling and aquifer testing, were utilized. Soil sampling was accomplished during this investigation using modified hollow-stem auger (HSA) drilling in conjunction with continuous solid-barrel sampling. Previous investigations conducted at the site utilized standard HSA drilling and soil sampling as well as cone penetrometer testing (CPT). Geoprobe[®] sampling apparatus and newly installed and previously existing monitoring wells were used to collect ground water samples during this investigation. Previous investigations utilized monitoring wells installed in HSA boreholes and monitoring points installed in CPT holes to sample ground water. Aquifer tests conducted at the site included pumping and slug testing.

This section presents the methods used by Parsons ES and researchers from the RSKERL to collect site-specific data at Hill AFB, Utah. Site characterization data obtained under this program were collected in four phases. Phase one consisted of collecting shallow ground water samples using a Geoprobe[®]. Phase two consisted of continuous soil boring and sampling, ground water monitoring well installation and sampling, and aquifer testing. Phase three consisted of collecting ground water samples from existing monitoring wells. Phase four consisted of continuous soil boring and sampling, ground water monitoring well installation and sampling, and ground water sampling using a Geoprobe[®]. In addition to the work conducted under this program, MWI collected soil and ground water data on numerous occasions (JMM, 1993b; MWI, MWI, 1994a; MWI, 1994b). Data collected under this program and data collected by MWI were integrated to develop the conceptual site model and to aid interpretation of the physical setting (Section 3) and contaminant distribution (Section 4).

The physical and chemical hydrogeologic data listed below were collected during the field work phase of the EE/CA:

- Depth from measurement datum to the water table or potentiometric surface in monitoring wells and monitoring points;
- Depth from measurement datum to the base of the shallow saturated zone;
- Location of potential ground water recharge and discharge areas;
- Hydraulic conductivity as determined from slug test data;
- Detailed stratigraphic analysis of subsurface media;
- Estimation of extent and thickness of mobile-phase LNAPL;
- Dissolved oxygen, nitrate, ferrous iron, sulfate, methane, chloride, ammonia, and total organic carbon (TOC) concentrations in ground water;
- Temperature, specific conductance, reduction/oxidation (redox) potential, total alkalinity, and pH of ground water;
- BTEX, trimethylbenzene, and total petroleum hydrocarbon (TPH) concentrations in ground water;
- BTEX, trimethylbenzene, and TPH concentrations in soil;
- TOC concentrations in select soil samples; and
- Chemical analysis of free product to determine the mass fraction of BTEX;

The following sections describe the procedures followed when collecting site-specific data. The applied drilling, soil sampling, lithologic logging, and monitoring well development procedures are described in Section 2.1. Ground water sampling procedures are described in Section 2.2. Aquifer testing procedures are described in Section 2.3.

2.1 DRILLING, SOIL SAMPLING, AND MONITORING WELL INSTALLATION

Drilling, soil sampling, and monitoring well installation were accomplished in two phases under this program. Phase one occurred during the week of 16 August 1993, and consisted of drilling, soil sampling, and monitoring well installation at EPA-82-A, EPA-82-B, EPA-82-C, EPA-82-D, EPA-82-E, EPA-82-F, EPA-82-H, and EPA-82-I (Figure 1.2). Phase two occurred during the week of 4 July 1994, and consisted of drilling and soil sampling at EPA-82-J and EPA-82-K, and monitoring well installation at EPA-82-J. Drilling, soil sampling, and monitoring well installation were accomplished using the procedures described in the following sections.

2.1.1 Well Locations and Completion Intervals

Nine new ground water monitoring wells were installed to help characterize the shallow ground water flow system UST Site 870. These wells are identified as EPA-82-A, EPA-82-B, EPA-82-C, EPA-82-D, EPA-82-E, EPA-82-F, EPA-82-H, EPA-82-I, and EPA-82-J. The new monitoring wells were installed in the locations shown on Figure 1.2. The well locations were selected to provide the hydrogeologic data necessary for successful implementation of the Bioplume II model and to support intrinsic remediation. Table 2.1 presents well completion details.

2.1.2 Well Drilling and Installation Procedures

This section describes the procedures used for drilling and installation of new monitoring wells. All new monitoring wells were installed in accordance with general procedures outlined in Section 8.5 of A Compendium of Superfund Field Methods (USEPA, 1987).

2.1.2.1 Pre-Drilling Activities

All necessary digging, drilling, and ground water monitoring well installation permits were obtained prior to mobilizing to the field. In addition, all utility lines were located and proposed drilling locations were cleared prior to any drilling activities.

Water used in drilling, equipment cleaning, or grouting were obtained from an onsite potable water supply. Water use approval was verified by contacting the appropriate facility personnel.

2.1.2.2 Equipment Decontamination Procedures

Prior to arriving at the site, and between each drilling location, the drill rig, augers, drilling rods, bits, casing, samplers, tools, and other downhole equipment were decontaminated using a high-pressure, steam/hot water wash. Only potable water was used for decontamination.

During drilling operations, the drill rig, augers, and any downhole drilling and/or sampling equipment were decontaminated at the north end of the industrial waste treatment plant (IWTP) at Hill AFB. Water from the decontamination operations was allowed to collect in

TABLE 2.1 WELL COMPLETION INFORMATION UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

EASTING** NORTHING**** (f.mst) 27.00 27.	(fms) (fms) PREVIOUSLY EXIST		-				
EASTING** NORTHING***	(ft msl) (ft msl) PREVIOUSLY EXIST	DEPTH DIAMETER	ER LENGTH	70.	BASE	3 0	BASE
2475.32 3841.98 4683.5 2533.09 382.19 4690.6 2446.70 3798.05 4682.19 2446.70 3798.05 4682.19 2253.47 3813.49 4682.2 2253.47 3813.49 4682.2 2252.21 3900.79 4693.6 2529.21 3930.05 4692.0 2529.21 3930.05 4652.0 1923.08 3213.91 4676.8 2167.57 3503.4 4676.8 2167.57 3503.4 4676.8 2167.57 3503.4 4606.3 1546.22 2945.10 4606.3 1548.19 2943.57 4606.1 1548.19 2943.57 4606.1 2520.42 3771.26 4683.0 2523.42 3771.26 4683.0 NA NA NA NA NA NA NA	PREVIOUSLY EXIST	(ft btoc) (inches)	s) (feet)	(fl bloc)	(ft btoc)	(foot)	(fext)
2475.32 3841.98 4683.91 2389.21 3846.24 4684.39 2533.09 3882.19 4690.67 2446.70 3798.05 4682.13 2536.47 3813.49 4682.13 2621.27 3900.79 4693.80 2449.70 3893.96 4682.09 2529.21 3930.05 4692.09 2529.21 3930.05 4692.09 2354.84 3397.60 4662.67 1923.08 3213.91 4637.37 2457.72 3650.34 4676.87 2167.57 3507.69 4625.11 1546.62 2945.10 4606.13 11345.36 2245.10 4600.13 1548.19 2943.57 4606.19 1550.42 3771.26 4683.08 2520.42 3771.26 4683.08 2520.42 3771.26 4683.08 2520.42 3771.26 4683.08 2530.42 3771.26 4683.08 2548.14 3861.96 NA NA NA NA NA NA NA	i -	NG MONITORING	WELLS				
2389.21 3846.24 4684.39 2533.09 3882.19 4690.67 2446.70 3798.05 4682.13 2536.47 3813.49 4682.13 2536.47 3813.49 4682.13 2521.27 3900.79 4693.80 2529.21 3930.05 4692.09 2354.84 3397.60 4662.67 1923.08 3213.91 4676.87 2457.72 3560.34 4676.87 2167.57 3507.69 4600.13 1345.36 2945.10 4606.19 1546.62 2945.10 4606.19 1546.42 2545.10 4606.19 1546.42 3771.26 4683.08 2520.42 3771.26 4683.08 25398.75 3645.85 4600.13 2550.42 3771.26 4683.08 2573.50 3896.74 4689.21 2548.14 3861.96 NA	_	28.20 4.00	10.00	18.00	28.00	4665.91	4655.91
2533.09 3882.19 4690.67 2446.70 3798.05 4682.13 2536.47 3813.49 4682.13 2536.47 3813.49 4692.03 2621.27 3900.79 4693.80 2449.70 3893.96 4693.80 2529.21 3930.05 4692.09 2529.21 3930.05 4692.09 2539.84 3397.60 4662.67 1923.08 3213.91 4637.37 2457.72 3503.4 4633.28 1840.49 3035.78 4655.39 1345.36 2245.10 4606.35 1545.19 2243.57 4606.19 1564.51 2719.71 4610.81 2520.42 3771.26 4683.08 2398.75 3645.85 4675.82 2573.50 3896.74 4689.21 2548.14 3861.96 NA NA NA NA NA NA		27.90 4.00	10.00	15.00	25.00	4669.39	4659.39
2446.70 3798.05 4682.13 2536.47 3813.49 4686.76 2389.06 3794.35 4679.03 2621.27 3900.79 4693.80 2449.70 3893.96 4682.09 2529.21 3930.05 4692.09 2529.21 3930.05 4692.09 2529.21 3930.05 4662.67 1923.08 3397.60 4662.67 1923.08 3397.60 4606.35 1546.62 2945.10 4606.35 1546.62 2945.10 4606.35 1546.49 3035.78 4625.17 1546.49 3035.78 4606.19 1547.72 3507.69 4655.39 1547.72 3507.69 4655.39 1548.19 2943.57 4606.19 1564.51 2719.71 4610.81 2520.42 3771.26 4683.08 2573.50 3896.74 4689.21 2548.14 3861.96 NA NA NA NA NA NA NA NA		37.24 6.00	20.00	15.00	35.00	4675.67	4655.67
2536.47 3813.49 4686.76 2389.06 3794.35 4679.03 2621.27 3900.79 4693.80 2449.70 3893.96 4682.09 2354.84 3397.60 4662.67 1923.08 3213.91 4637.37 2457.72 3503.4 4638.32 1546.62 2945.10 4606.35 1546.62 2945.10 4606.35 1546.49 3035.78 4606.19 1543.19 2943.57 4606.19 1550.42 3771.26 4683.08 2550.42 3771.26 4683.08 2550.42 3771.26 4683.08 2573.50 3896.74 4689.21 2548.14 3861.96 4689.21 NA NA NA NA NA	_	24.68 6.00	10.00	14.00	24.00	4668.13	4658.13
2389.06 3794.35 4679.03 2621.27 3900.79 4693.80 2449.70 3893.96 4689.02 2529.21 3930.05 4692.09 2354.84 3397.60 4662.67 1923.08 3213.91 4637.37 2457.72 3650.34 4676.87 2062.23 3063.44 4633.28 1840.49 3035.78 4606.19 1543.19 2243.57 4606.19 1564.51 2719.71 4610.81 2520.42 3771.26 4683.08 2398.75 3645.86 4675.82 2573.50 3896.74 4689.21 2548.14 3861.96 NA		27.39 4.00	10.00	17.50	27.50	4669.26	4659.26
2621.27 3900.79 4693.80 2449.70 3893.95 4688.02 2529.21 3930.05 4692.09 2354.84 3397.60 4662.67 1923.08 3213.91 4637.37 2457.72 3650.34 4637.37 2062.23 3063.44 4633.28 1840.49 3035.78 4606.35 1543.19 2243.57 4606.19 1564.51 2719.71 4610.81 2520.42 3771.26 4683.08 2559.87 366.98 4655.39 1543.19 2943.57 4606.19 1564.51 3771.26 4689.21 2558.14 3861.96 4689.21 NA NA NA NA NA NA	_	29.34 4.00	10.00	20.00	30.00	4659.03	4649.03
2493.70 3893.96 4688.02 2529.21 3930.05 4692.09 2354.84 3397.60 4662.67 1923.08 3213.91 4676.87 2457.72 3650.34 4676.87 2062.23 3063.44 4676.83 2062.23 3063.44 4633.28 1840.49 3035.78 4606.13 1543.19 2943.57 4606.19 1543.19 2943.57 4606.19 1543.19 2943.57 4606.19 1543.19 2943.57 4606.19 2520.42 3771.26 4683.08 2550.42 3771.26 4689.21 2548.14 3861.96 4688.21 NA		40.20 4.00	10.00	28.00	38.00	4665.80	4655.80
2529.21 3930.05 4692.09 2354.84 3397.60 4662.67 1923.08 3213.91 4637.37 2457.72 3650.34 4676.87 1546.62 2945.10 4606.35 2062.23 3063.44 4633.28 1840.49 3035.78 4625.17 2167.57 3507.69 4655.39 1345.36 2845.36 4600.13 1543.19 2943.57 4606.19 1564.51 2719.71 4610.81 2520.42 3771.26 4689.21 2548.14 3861.96 4689.21 2548.14 3861.96 NA	_	29.72 2.00	10.00	20.00	30.00	4668.02	4658.02
2354.84 3397.60 4662.67 1923.08 3213.91 4637.37 2457.72 3650.34 4676.87 2062.23 3063.44 4636.35 2062.23 3063.44 4633.28 1840.49 3035.78 4625.17 2167.57 3507.69 4655.39 1345.36 2845.36 4605.13 1543.19 2943.57 460.13 1550.42 3771.26 4683.08 2520.42 3771.26 4683.08 2573.50 3896.74 4689.21 2548.14 3861.96 NA NA NA NA NA NA NA NA NA	_	36.65 2.00	20.00	15.00	35.00	4677.09	4657.09
1923.08 3213.91 4637.37 2457.72 3650.34 4676.87 1546.62 2945.10 4606.35 2062.23 3063.44 4633.28 1840.49 3035.78 4625.17 2167.57 3507.69 4655.39 1345.36 2845.36 4600.13 1543.19 2943.57 4606.19 1964.51 2719.71 4610.81 2520.42 3771.26 4683.08 2398.75 3645.85 4675.82 2573.50 3896.74 4689.21 2548.14 3861.96 NA NA NA NA NA NA NA		44.94	20.50	25.00	45.50	4637.67	4617.17
1546.62 2945.10 4606.35 2062.23 3063.44 4633.28 2062.23 3063.44 4633.28 2167.57 3507.69 4625.39 1345.36 2845.36 4605.39 1543.19 2943.57 4606.19 1964.51 2719.71 4610.81 2520.42 3771.26 4683.08 2398.75 3645.85 4675.82 2573.50 3896.74 4689.21 2548.14 3861.96 NA	_	45.32 6.00	20.50	25.00	45.50	4612.37	4591.87
1546.62 2945.10 4606.35 2062.23 3063.44 4633.28 1840.49 3035.78 4625.17 2167.57 3507.69 4655.39 1345.36 2845.36 4600.13 1543.19 2943.57 4606.19 1964.51 2719.71 4610.81 2520.42 3771.26 4683.08 2350.42 3771.26 4683.08 2573.50 3896.74 4689.21 2548.14 3861.96 NA NA NA NA NA NA NA	\dashv	44.80 6.00	20.50	24.50	45.00	4652.37	4631.87
1546.62 2945.10 4606.35 4606.01 2002.23 3003.44 4633.28 4632.99 1840.49 3035.78 4625.17 4624.92 2167.57 3507.69 4655.39 4655.13 1345.36 2845.36 4600.13 4599.74 1543.19 2943.57 4606.19 4605.89 1 1964.51 2719.71 4610.81 4610.57 2520.42 3771.26 4683.08 4682.80 2398.75 3645.85 4675.82 4676.17 2573.50 3896.74 4689.21 4689.56 2548.14 3861.96 4689.21 4688.55 NA NA N	NEWLY INSTALLE	D MONITORING W	ELS				
1840.49 3053.78 4633.28 4632.99 1840.49 3035.78 4625.17 4624.92 2167.57 3507.69 4655.39 4655.13 1345.36 2845.36 4600.13 4559.74 1543.19 2943.57 4600.13 4509.74 1564.51 2719.71 4610.81 4610.57 2520.42 3771.26 4683.08 4682.80 2573.50 3866.74 4689.21 4689.56 NA NA NA NA NA NA NA NA NA NA NA NA		30.40 2.00	5.00	25.00	30.00	4581.35	4576.35
1840.49 3035.78 4625.17 4624.92 2167.57 3507.69 4655.39 4655.13 1345.36 2845.36 4600.13 4599.74 1543.19 2943.57 4606.19 4605.89 1964.51 2719.71 4610.81 4610.57 2520.42 3771.26 4683.08 4682.80 2398.75 3645.85 4675.82 4676.17 2573.50 3896.74 4689.21 4689.56 2548.14 3861.96 4686.21 4686.53 NA NA N	_	30.45 2.00	10.00	20.05	30.05	4613.23	4603.23
2167.57 3507.69 4655.39 4655.13 1345.36 2845.36 4600.13 4599.74 1543.19 2943.57 4606.19 4605.89 1964.51 2719.71 4610.81 4610.58 2520.42 3771.26 4683.08 4682.80 2398.75 3645.85 4675.82 4676.17 2573.50 3896.74 4689.21 4689.56 2548.14 3861.96 4686.21 4686.53 NA NA N	_	24.75 2.00	2:00	19.35	24.35	4605.82	4600.82
1345.36 2845.36 4600.13 4599.74 1543.19 2943.57 4606.19 4605.89 1964.51 2719.71 4610.81 4610.57 2520.42 3771.26 4683.08 4682.80 25398.75 3645.85 4675.82 4676.17 2573.50 3896.74 4689.21 4689.56 2548.14 3861.96 4686.21 4686.53 NA N			00.01	19.41	29.41	4635.98	4625.98
1543.19 2943.57 4606.19 4605.89 1964.51 2719.71 4610.81 4610.57 2520.42 3771.26 4683.08 4682.80 23398.75 3645.85 4675.82 4675.12 4680.55 2573.50 3896.74 4689.21 4680.55 2548.14 3861.96 4686.21 4686.53 NA			2:00	3.92	8.92	4596.21	4591.21
1 1964.51 2719.71 4610.81 4610.57 2520.42 3771.26 4683.08 4682.80 2398.75 3645.85 4675.82 4676.17 2573.50 3896.74 4689.21 4689.56 2548.14 3861.96 4686.21 4686.53 NA		9.30 2.00	2:00	3.90	8.90	4602.29	4597.29
2520.42 3771.26 4683.08 4682.80 2398.75 3645.85 4675.82 4676.17 2573.50 3896.74 4689.21 4689.56 2548.14 3861.96 4686.21 4686.53 NA NA N			15.00	9.10	24.10	4601.71	4586.71
2.1 2398.75 3645.85 4675.82 4676.17 2573.50 3896.74 4689.21 4689.26 4686.53 4686.51 4686.53 NA			2:00	17.85	22.85	4665.23	4660.23
3 2573.50 3896.74 4689.21 4689.56 4 2548.14 3861.96 4686.21 4686.53 NA NA N	_		10.00	22.30	32.30	4653.52	4643.52
1 2548.14 3861.96 4686.21 4686.53 4686.53 A 46			10.00	10.00	35.00	4679.21	4654.21
NA N	\dashv	35.00 7.25	10.00	10.00	35.00	4676.21	4651.21
NA N	PIEZ	OMETERS					
NA N		27.00 0.50	5:00	22.00	27.00	Ϋ́	¥
NA NA NA NA		26.00 0.50	2:00	21.00	26.00	¥	٧Z
		27.60 0.50	2:00	22.60	27.60	ž	¥ Z
NA NA NA NA	AN AN		2:00	19.00	24.00	ž	▼
CPT-7 2547.88 3772.45 4684.21 4684.37 23.85		23.85 0.50	5.00	18.85	23.85	4665.36	4

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TABLE 2.1 (Continued)

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WELL COMFLETION INFORMATION UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

			DATUM.	GROUND	TOTAL	INNER WELL	SCREEN	DEPTH TO SCREEN	SCREEN	SCREEN E	SCREEN FLEVATION
WELL			ELEVATION	ELEVATION	DEPTH	DIAMETER	LENGTH	TOP	BASE	TOP	BASE
NUMBER	EASTING.	EASTING ** NORTHING ***	(fi msl)	(ft msl)	(ft btoc)	(inches)	(feet)	(fl btoc)	(ft btoc)	(feet)	(feet)
				PIEZOMET	PIEZOMETERS (Continued)	inued)					
CPT-10	2602.28	3772.04	4686.54	4686.80	25.50	0.50	2:00	20.50	25.50	4666.04	4661.04
CPT-11	Y Y	NA	Y Y	Ϋ́	30.25	0.50	2:00	25.25	30.25	¥	¥
CPT-12	2354.84	3397.60	4662.67	4662.95	Ϋ́	0.50	2.00	Y Y	ĄZ.	¥	×
CPT-13	2062.91	3060.14	4633.21	4633.43	24.00	0.50	2.00	19.00	24.00	4614.21	4609.21
CPT-14	2182.60	3507.60	4655.88	4656.10	28.28	0.50	2.00	23.28	28.28	4632.60	4627.60
CPT-15	2262.51	2985.53	4638.74	4638.92	35.40	0.50	2.00	30.40	35.40	4608.34	4603.34
CPT-17	1528.38	3493.12	4635.28	4635.51	14.41	0.50	2.00	9.41	14.41	4625.87	4620.87
CPT-18	1885.05	3457.77	4641.46	4641.82	15.09	0.50	\$.00	10.09	15.09	4631.37	4626.37
CPT-19	1948.46		4636.98	4637.31	33.35	0.50	8.00	28.35	33.35	4608.63	4603.63
CPT-20	1848.28	3037.59	4625.48	4625.69	28.20	0.50	2.00	23.20	28.20	4602.28	4597.28
CPT-21	2349.56	3244.25	4655.91	4656.26	34.15	0.50	2.00	29.15	34.15	4626.76	4621.76
CPT-22	Ϋ́	NA	Y.	NA AN	25.35	0.50	2.00	20.35	25.35	Ϋ́	Y'A
CPT-23	2526.12	2835.21	4642.49	4642.69	31.00	0.50	5.00	26.00	31.00	4616.49	4611.49
CPT-25	Ϋ́	NA	¥.	ΝΑ	38.00	0.50	2.00	33.00	38.00	X X	¥ X
CPT-26	1208.02	2573.01	4591.94	4592.20	12.30	0.50	2.00	7.30	12.30	4584.64	4579.64
CPT-27	1662.55	2660.73	4604.04	4604.32	10.00	0.50	2.00	2.00	10.00	4599.04	4594.04
CPT-28	1538.79	2939.72	4605.62	4605.96	7.77	0.50	8.00	2.77	7.77	4602.85	4597.85
CPT-29	1400.23	2863.23	4600.67	4600.89	7.00	0.50	2.00	2.00	7.00	4598.67	4593.67
CPT-30	1963.38	2711.28	4610.22	4610.48	15.35	0.50	2.00	10.35	15.35	4599.87	4594.87
CPT-31	1418.19	3205.92	4610.88	4611.15	10.35	0.50	2.00	5.35	10.35	4605.53	4600.53
CPT-33	Ϋ́	Y.	Υ Y	N.	¥	0.50	2.00	Υ V	٧Z	Ϋ́	¥ X
CPT-34	Ϋ́	Y Y	Y Y	A'A	21.90	0.50	2.00	16.90	21.90	¥	Y X
CPT-36	2670.91	3231.11	4669.78	4670.01	35.00	0.50	2.00	30.00	35.00	4639.78	4634.78
CPT-37	1970.30	2978.15	4625.35	4625.60	27.50	0.50	2.00	22.50	27.50	4602.85	4597.85
CPT-38	1177.69	3504.76	4615.66	4615.90	14.55	0.50	2.00	9.55	14.55	4606.11	4601.11
CPT-40	2758.65	4145.21	4715.46	4715.05	55.33	0.50	20.00	35.33	55.33	4680.13	4660.13
CPT41	2857.64	3142.16	4675.19	4675.41	40.05	0.50	2.00	35.05	40.05	4640.14	4635.14
CPT-42	3067.32	3238.57	4678.34	4678.49	39.73	0.50	2.00	34.73	39.73	4643.61	4638.61
CPT-43	2683.44	3014.06	4659.74	4660.02	37.60	0.50	2.00	32.60	37.60	4627.14	4622.14
CPT-44	NA	NA	NA A	Ϋ́Α	41.00	0.50	200	36.00	41.00	Y'A	A A

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TABLE 2.1 (Concluded)

UST SITE 870 INTRINSIC REMEDATION EE/CA WELL COMPLETION INFORMATION HILL AFB, UTAH

			DATUM	GROUND	TOTAL	INNER WELL	SCREEN	DEPTH TO SCREEN	SCREEN	SCREENE	SCREEN ELEVATION
WEL.			ELEVATION	ELEVATION	DEPTH	DIAMETER	LENGTH	TOP	BASE	TOP	BASE
NUMBER	EASTING** NORTHING	NORTHING***	(ft.msl)	(ft msl)	(ft btoc)	(inches)	(feet)	(ft btoc)	(ft btoc)	(fæt)	(feet)
				GEOP	GEOPROBE						
EPA-82-K	1458.62	2656.22	4598.38	4598.38	9.6	0.25	::	9.64	9.64	4588.74	4588.74
EPA-82-L1	-8055.75	2834.32	4614.15	4614.15	18.80	0.25	1.50	17.30	18.80	4596.85	4595.35
EPA-82-L2	-8055.75	2834.32	4614.15	4614.15	21.80	0.25	1.50	20.30	21.80	4593.85	4592.35
EPA-82-L3	-8055.75	2834.32	4614.15	4614.15	24.80	0.25	1.50	23.30	24.80	4590.85	4589.35
EPA-82-M	1700.5	2698.09	4605.01	4605.01	12.00	0.25	•	12.00	12.00	4593.01	4593.01
EPA-82-M duplicate	1700.5	2698.09	4605.01	4605.01	12.00	0.25	:::	12.00	12.00	4593.01	4593.01
EPA-82-N	N A	2738.09	4599.81	4599.81	8 :00	0.25	***	8.00	8.00	4591.81	4591.81
EPA-82-0	1594.5	2688.82	4602.30	4602.30	9.80	0.25	::	9.80	9.80	4592.50	4592.50
EPA-82-P	1,776,37	2865.35	4612.65	4612.65	19.00	0.25	****	19.00	19.00	4593.65	4593.65

Datum is top of PVC well casing

For absolute easting coordinates add 1,860,000 to these numbers
*** For absolute northing coordinates add 280,000 to these numbers

**** Sample collected from end of polyethylene tubing

ft btoc = Feet below top of PVC well casing

ft msl = Feet above mean sea level NA = Data not available

the decontamination pad collection tanks. Precautions were taken to minimize any impact to the area surrounding the decontamination pad that might result from the decontamination operations.

All sampling tools were cleaned onsite prior to use and between each sampling event with a clean water/phosphate-free detergent mix and a clean water rinse. All well completion materials were factory sealed. All decontamination activities were conducted in a manner so that the excess water was controlled and not allowed to flow into any open borehole.

Fuel, lubricants, and other similar substances were handled in a manner consistent with accepted safety procedures and standard operating practices. Well completion materials were not stored near or in areas which could be affected by these substances.

2.1.2.3 Drilling and Soil Sampling

Drilling was accomplished by using the HSA method, modified with a hinged door on the lead auger. The use of the hinged door facilitated collection of representative soil samples over the entire range of contamination. The borings were drilled and continuously sampled to the proposed total depth of the monitoring well. A final borehole diameter of at least 8 inches (with the exception of EPA-82-J, which used a 6-inch boring) was used for the installation of wells with a 2-inch inside-diameter (ID) casing.

Continuous soil samples were obtained using a 3-inch-ID solid-barrel continuous sampling device. Samples were collected continuously over the full depth of the soil borehole. The soil samples collected were removed from the continuous sampler in 0.3-foot intervals and placed in clean glass jars for laboratory analysis. In addition, a portion of the soil sample was placed in a clean glass jar for photoionization detector (PID) headspace measurements for volatile organic compounds (VOCs) and lithologic logging. Representative portions of the soil samples collected for the headspace procedure were quickly transferred to clean glass jars, sealed with aluminum foil, and held for 15 minutes at an ambient temperature of 65 degrees Fahrenheit (°F) or greater. Semiquantitative measurements were made by puncturing the aluminum foil seal with the PID probe and reading the concentration of the headspace gases. The PID relates the concentration of total VOCs in the sample to an isobutylene calibration standard. The PID was also used to monitor the worker breathing zone.

The Parsons ES field hydrogeologist observed drilling and well installation activities, maintained a detailed descriptive log of subsurface materials recovered, and photographed representative samples. Final geologic boring logs are presented in Appendix A These logs contain:

- Sample interval (top and bottom depth);
- Presence or absence of contamination based on odor, staining, and/or PID readings;
- Soil description, including color, major textural constituents, minor constituents, relative moisture content, plasticity of fines, cohesiveness, grain size, structure or stratification, relative permeability, and any other significant observations; and
- Lithologic contacts with the depth of lithologic contacts and/or significant textural changes recorded to the nearest 0.1 foot (1 inch).

Soils exhibiting petroleum hydrocarbon contamination based on PID screening were drummed and stored onsite during the drilling operations. Upon completion of the drilling activities, two composite samples from the contaminated soil drums were collected and analyzed by USEPA Methods SW8020 and SW8015 modified. Upon receipt of the soil analytical results, these soils were transferred for disposal to E.T. Technologies, Inc. in Salt Lake City, Utah by Hill AFB personnel. Clean soils were handled by Hill AFB personnel who were responsible for the final disposition of these soils.

2.1.2.4 Monitoring Well Installation

Ground water monitoring wells were installed in nine soil borings under this program. Detailed well installation procedures are described in the following paragraphs. Well completion diagrams are included in Appendix A.

2.1.2.4.1 Well Materials Decontamination

Well completion materials were inspected by the field hydrogeologist and determined to be clean and acceptable prior to use. All well completion materials were factory sealed. Prepackaged sand, bentonite, and Portland[®] cement were used in well construction, and the bags were inspected for possible external contamination before use. Materials that could not be cleaned to the satisfaction of the field hydrogeologist were not used.

2.1.2.4.2 Well Casing

Upon completion of drilling, a monitoring well casing was installed. Well construction details were noted on a Monitoring Well Installation Record form. This information became part of the permanent field record for the site and is included in Appendix A.

Blank well casing was constructed of Schedule 40 polyvinyl chloride (PVC) with an ID of 2 inches. All well casing sections were flush-threaded, and glued joints were not used. The casing at each well was fitted with a threaded bottom plug and a top cap constructed of the same type of material as the well casing. The top cap was vented to maintain ambient atmospheric pressure within the well casing.

The field hydrogeologist verified and recorded the boring depth, the lengths of all casing sections, and the depth to the top of all well completion materials placed in the annulus between the casing and borehole wall. All lengths and depths were measured to the nearest 0.1 foot.

2.1.2.4.3 Well Screen

Well screens were constructed of flush-threaded, Schedule 40 PVC with an ID of 2 inches. The screens were factory slotted with 0.010-inch openings. Each well was screened so that seasonal fluctuations of the water table can be measured. Except where specified, the entire thickness of the sand interval of the shallow aquifer was screened. The position of the screen was selected by the field hydrogeologist after consideration was given to the geometry and hydraulic characteristics of the stratum in which the wells were screened.

2.1.2.4.4 Sand Filter Pack

A graded sand filter was placed around the screened interval from the bottom of the casing to approximately 2 feet above the top of the screen. Number 10-20 Colorado silica sand was used for the sand filter pack.

2.1.2.4.5 Annular Sealant

An annular seal of sodium bentonite pellets was placed above the sand pack. The pellet seal was a minimum of 2 feet thick and was hydrated in place with potable water. In wells EPA-82-A, EPA-82-B, EPA-82-C, EPA-82-D, EPA-82-E, EPA-82-F, EPA-82-H, and EPA-

82-I, the pellet seal was overlaid with a Portland® cement/sodium bentonite grout that extends from the top of the pellet seal to approximately 4.5 feet below ground surface (bgs). The Portland® cement/sodium bentonite grout mix consisted of one 94-pound sack of cement and about 5 pounds of bentonite for each 7 gallons of water used. The bentonite content of the grout did not exceed 8 percent by dry weight. In well EPA-82-J, Baroid® 3/8 bentonite chips were placed in the borehole from the top of the sand pack to approximately 4.8 feet bgs. The grout or bentonite chips were overlaid with concrete that extends to the ground surface.

2.1.2.4.6 Flush-Mount Protective Cover

Each monitoring well was completed with an at-grade protective cover. In areas with pavement, the at-grade covers were cemented in place using concrete blended to the existing pavement. All wells were completed with concrete pads that slope gently away from the protective casing to facilitate runoff during precipitation events.

2.1.2.5 Well Development

Before being sampled, newly installed monitoring wells were developed. Well development removes sediment from inside the well casing and flusies fines, cuttings, and drilling fluids from the sand pack and the portion of the formation adjacent to the well screen.

Well development was accomplished using a peristaltic pump. The pump tubing was regularly lowered to the bottom of the well so that fines were agitated and removed from the well in the development water. Development was continued until a minimum of 10 casing volumes of water were removed from the well and the pH, temperature, specific conductivity, dissolved oxygen (DO) concentration, and redox potential of the ground water had stabilized. All well development waters were collected in 55-gallon drums and transported to the Hill AFB IWTP for treatment and disposal.

2.1.2.6 Water Level Measurements

Water levels at all sampled monitoring wells were measured. Measurements were made using an electric water level probe capable of recording to the nearest 1/8 inch (0.01 foot). In addition, water level measurements were made in select piezometers and previously existing monitoring wells at the site.

2.1.2.7 Well Location and Datum Survey

The location and elevation of the new wells were surveyed by a registered surveyor soon after well completion. The horizontal location were measured relative to established Hill AFB coordinates. Horizontal coordinates were measured to the nearest 1 foot. Vertical location of the ground surface adjacent to the well casing and the measurement datum (top of the PVC well casing) were measured relative to a US Geological Survey (USGS) mean sea level datum. The ground surface elevation was measured to the nearest 0.1 foot, and the measurement datum elevation was measured to the nearest 0.01 foot.

2.2 GROUND WATER SAMPLING

This section describes the procedures used for collecting ground water quality samples. In order to maintain a high degree of quality control during this sampling event, the procedures described in the following sections were followed.

Ground water samples were collected in four phases under this program. Phase one occurred during the week of 2 August 1993, and consisted of collecting ground water samples near existing CPT locations using a Geoprobe[®]. This ground water sampling process is described in Section 2.2.3.1. The second phase of ground water sampling occurred during the week of 16 August 1993, and consisted of collecting ground water samples from monitoring wells and water samples from the stormwater drain. The procedures used to sample ground water monitoring wells are described in Section 2.2.3.2. The third phase of ground water sampling occurred during the week of 8 November 1993, and consisted of sampling ground water monitoring wells. The fourth phase of ground water sampling occurred during the week of 4 July 1994, and consisted of collecting ground water samples from monitoring wells and by using a Geoprobe[®]. In addition to the sampling events conducted under this program, several ground water sampling events have been conducted by MWI at this site.

Activities that occurred during ground water sampling are summarized below:

- Assembly and preparation of equipment and supplies;
- Inspection of the well integrity (for monitoring well sampling), including
 - Protective cover, cap and lock,
 - External surface seal and pad,
 - Datum reference, and

- Internal surface seal;
- · Ground water sampling, including
 - Water level measurements,
 - Visual inspection of water,
 - Well casing or Geoprobe® point evacuation, and
 - Sampling;
- Sample preservation and shipment, including
 - Sample preparation,
 - Onsite measurement of physical parameters, and
 - Sample labeling and packing;
- Completion of sampling records;
- Completion of chain-of-custody records; and
- Sample disposition.

Detailed ground water sampling and sample handling procedures that were used are presented in following sections.

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2.2.1 Ground Water Sampling Locations

Ground water samples were collected from existing and newly installed monitoring wells, from Geoprobe® ground water sampling equipment, and at accessible locations along the storm sewer.

2.2.1.1 Geoprobe® Sampling Locations

Ground water samples were collected using the Geoprobe® sampling apparatus near nine existing CPT locations (CPT-8, CPT-17, CPT-18, CPT-19, CPT-23, CPT-29, CPT-31, CPT-38, and CPT-39) during the week of 2 August 1994. During the week of 4 July 1994, ground water samples were collected using the Geoprobe® sampling apparatus at points EPA-82-K, EPA-82-L, EPA-82-M, EPA-82-N, EPA-82-O, and EPA-82-P. Geoprobe® sampling locations are shown in Figure 1.2.

2.2.1.2 Monitoring Well Sampling Locations

Nine new monitoring wells were installed in the locations shown on Figure 1.2. After completion of well installation and development activities, these wells were sampled using a peristaltic pump with dedicated polyethylene tubing. Previously existing monitoring wells were also sampled under this program.

2.2.1.3 Storm Sewer Sampling Locations

Water samples were collected from accessible locations along the storm sewer system shown on Figure 1.2. These samples are labeled storm-2 and storm-3.

2.2.2 Preparation for Sampling

All equipment used for sampling was assembled and properly cleaned and calibrated (if required) prior to arriving in the field. In addition, all record keeping materials were gathered prior to leaving the office.

2.2.2.1 Equipment Cleaning

All portions of sampling and test equipment that contacted the sample were thorough cleaned before use. This equipment included water level probe and cable, lifting line, test equipment for onsite use, and other equipment that contacted the samples. The following cleaning protocol was used:

- Cleaned with potable water and phosphate-free laboratory detergent;
- Rinsed with potable water;
- Rinsed with distilled or deionized water;
- Rinsed with reagent-grade acetone;
- Air dried prior to use.

2.2.2.2 Equipment Calibration

As required, field analytical equipment were calibrated according to the manufacturer's specifications prior to field use. This applied to equipment used for onsite chemical measurements of DO, redox potential, pH, specific conductivity, and temperature.

2.2.3 Sampling Procedures

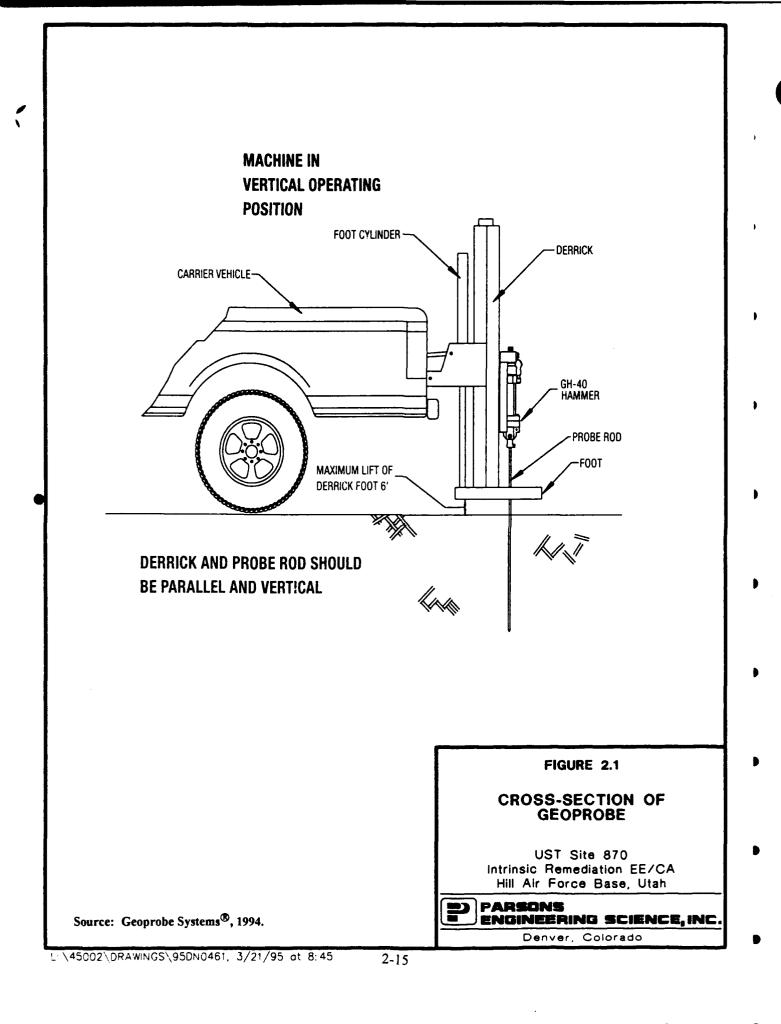
Special care was taken to prevent contamination of the ground water and extracted samples through cross contamination from improperly cleaned equipment. Water level probes and cable used to determine static water levels and well total depths were thoroughly cleaned before and after field use and between uses at different sampling locations according to the procedures presented in Section 2.2.2.1. In addition, a clean pair of new, disposable nitrile gloves was worn each time a different well was sampled.

2.2.3.1 Geoprobe® Ground Water Sampling

The Geoprobe® system is a hydraulically powered percussion/probing machine used to advance sampling tools through unconsolidated soils. This system provides for the rapid collection of ground water (and soil and soil gas if necessary) samples at shallow depths while minimizing the generation of investigation-derived waste materials. Figure 2.1 is a diagram of the Geoprobe® system. The following sections describe the ground water sample collection methods and decontamination methods using the Geoprobe® system.

2.2.3.1.1 Sampling Interval and Method

Based on the anticipated ground water elevation, the sampling depth and interval were estimated prior to driving the Geoprobe® sampling rods into the ground. The Parsons ES field hydrogeologist verified the sampling depth by measuring the length of each Geoprobe® sampling rod prior to insertion into the ground. A disposable drive tip was placed at the tip of the Geoprobe® sampling rods. This tip was threaded on the uphole end to allow attachment of 3/8-inch, high-density polyethylene (HDPE) tubing. After reaching the desired depth, HDPE tubing was threaded through the center of the hollow Geoprobe® sampling rod and secured to the drive point. The tubing was perforated at the downhole end using a 1/16-inch drill bit at 1/4-inch intervals alternately offset at 90 degree angles. The Geoprobe®



sampling rod was then pulled back approximately 1 foot to allow ground water to enter the perforated end of the polyethylene tubing. When the rod was pulled up, the sampling tip remained at the probe termination depth, and the 1-foot perforated interval of the polyethylene tubing was exposed to ground water. Ground water samples were then acquired using a peristaltic pump, as described in Section 2.2.3.1.4

2.2.3.1.2 Preparation of Location

Prior to sampling, the area around the well was cleared of foreign materials, such as brush, rocks, and debris. This prevented sampling equipment from inadvertently contacting foreign materials near the sampling point.

2.2.3.1.3 Water Level and Total Depth Measurements

Prior to removing any water from the Geoprobe® sampling location the static water level was measured. A manometer with hollow HDPE tubing was inserted into the HDPE tubing through which the ground water sample was acquired until positive pressure on the manometer indicated that ground water was reached. The manometer tube was then marked at the level of the ground surface and removed from the ground. Depth to water was determined by placing a tape measure next to the HDPE tubing and measuring the length from the base of the tubing to the ground level mark to the nearest 0.1 foot. Sampling depth was measured to the nearest 0.1 foot by noting the length of each section of Geoprobe®sampling rod placed in the ground.

2.2.3.1.4 Sample Extraction

A peristaltic pump was used to extract ground water samples from the Geoprobe® sampling point. Prior to sample collection, ground water was purged until DO and temperature readings stabilized. The samples were transferred directly to the appropriate sample container. The water was carefully poured down the inner walls of the sample bottle to minimize aeration of the sample.

2.2.3.1.5 Geoprobe® Equipment Decontamination

All geoprobe rids, tips, or other downhole equipment were decontaminated with a highpressure, steam/hot water wash. Enough linear feet of Geoprobe® rods and Geoprobe® tips were available that decontamination procedures were minimized to every fourth or fifth Geoprobe[®] sampling location. Only potable water was used for decontamination. Collection of waters and decontamination of sampling tools is as described in Section 2.1.2.2.

2.2.3.2 Ground Water Monitoring Well Sampling

2.2.3.2.1 Preparation of Location

Prior to starting the sampling procedure, the area around the well was cleared of foreign materials, such as brush, rocks, and debris. These procedures prevented sampling equipment from inadvertently contacting debris around the monitoring well.

2.2.3.2.2 Water Level and Total Depth Measurements

Prior to removing any water from the well the static water level was measured. An electric water level probe was used to measure the depth to ground water below the datum to the nearest 0.01 foot. After measurement of the static water level, the water level probe was lowered to the bottom of the well for measurement of total well depth (recorded to the nearest 0.01 foot). Based on these measurements, the volume of water purged from the wells was calculated.

2.2.3.2.3 Well Bore Purging

Three times the calculated casing volume was removed from each well prior to sampling. All purge water was placed in 55-gallon drums and transported to the Hill AFB IWTP for disposal and treatment. The empty drums were rinsed with hot water and returned to base personnel for reuse. A peristaltic pump with dedicated Teflon®-lined polyethylene tubing was used for well evacuation.

2.2.3.2.4 Sample Extraction

A peristaltic pump with dedicated Teflon[®]-lined polyethylene tubing was used to extract ground water samples from the well. The sample was transferred directly to the appropriate sample container. The water was carefully poured down the inner walls of the sample bottle to minimize aeration of the sample.

2.2.3.3 Storm Sewer Sampling

A peristaltic pump with dedicated Teflon[®]-lined polyethylene tubing was used to extract ground water samples from the storm sewer. The sample was transferred directly to the appropriate sample container. The water was carefully poured down the inner walls of the sample bottle to minimize aeration of the sample.

2.2.4 Onsite Chemical Parameter Measurement

2.2.4.1 Dissolved Oxygen Measurements

DO measurements were taken using an Orion[®] model 840 DO meter. Groundwater was continuously extracted and collected in an erlenmeyer flask using a peristaltic pump. The probe of the DO meter was submerged in the erlenmeyer flask to monitor DO concentrations. DO concentrations were recorded after DO reading, stabilized and these readings represent the lowest DO concentration observed.

2.2.4.2 Reduction/Oxidation Potential Measurements

Redox potential measurements were taken in a similar manner as DO measurements using an Orion® model 290A redox potential meter. Groundwater was continuously extracted with a peristaltic pump and collected in an erlenmeyer flask. The redox probe was submerged in the erlenmeyer flask to take continuous redox measurements. Redox potential measurements were recorded after the readings stabilized and these readings represent the lowest redox potential observed.

2.2.4.3 pH, Temperature, and Specific Conductance

Because the pH, temperature, and specific conductance of the ground water change significantly within a short time following sample acquisition, these parameters were measured in the field. The measurements were made in a clean glass container separate from those intended for laboratory analysis, and the measured values were recorded in the ground water sampling record.

2.2.5 Sample Handling

2.2.5.1 Sample Preservation

The USEPA Mobile Laboratory added any necessary chemical preservatives to sample containers prior to sampling. Soil samples collected for VOC analysis were stored in 40 milliliter (mL) volatile organic analysis (VOA) vials and preserved with 5 mL of acidified water (pH < 2) and 5 mL of methylene chloride. Soil samples collected for TOC measurements were stored at 4 degrees Celsius (°C) in coolers. Ground water samples collected for VOC analysis were stored in 40 mL VOA vials with lead lined septa and preserved with 4 grams of trisodium phosphate. Ground water samples for all oxidized inorganic compounds, with the exception of nitrate, were stored in 200 mL high density polyethylene (HDPE) sample containers and stored at 4°C or below. Ground water samples collected for nitrate analysis were stored in 200 mL HDPE sample containers and acidified (pH < 2) with sulfuric acid. All analysis for reduced inorganic species (e.g. ferrous iron, nitrite, and methane) were performed immediately in the field.

2.2.5.2 Sample Container and Labels

Sample containers and appropriate container lids were provided by the EPA Mobile Laboratory. The sample containers were filled as described in Sections 2.2.3.1.4, 2.2.3.2.4, and 2.2.3.3, and the container lids were tightly closed. Samples to be analyzed for VOCs were collected into containers with zero headspace. The sample label was firmly attached to the container side, and the following information was legibly and indelibly written on the label:

- · Facility name;
- Sample identification;
- Sample type (ground water);
- Sampling date;
- Sampling time;
- · Preservatives added; and,
- Sample collector's initials.

2.2.5.3 Sample Shipment

After the samples were sealed and labeled, they were packaged for immediate transport to the onsite USEPA Mobile Laboratory. The following packaging and labeling procedures were followed:

- Sample was packaged to prevent leakage or vaporization from its container;
- Shipping container was labeled with
 - Sample collector's name, address, and telephone number;
 - Laboratory's name, address, and telephone number;
 - Description of sample;
 - Quantity of sample; and
 - Date of transfer to onsite laboratory.

The packaged samples were delivered to the USEPA Mobile Laboratory. Delivery occurred shortly after sample acquisition.

2.3 AQUIFER TESTING

2.3.1 Slug Testing

Slug tests were conducted to estimate the hydraulic conductivity of the shallow saturated zone at UST Site 870. Slug tests are single-well hydraulic tests used to determine the hydraulic conductivity of an aquifer in the immediate vicinity of the tested well. Slug tests can be used for both confined and unconfined aquifers that have a transmissivity of less than 7,000 square feet per day (ft²/day). Slug testing can be performed using either a rising head or a falling head test. Rising head tests generally give more accurate results and were used at this site. Slug tests were performed in monitoring wells EPA 82-C, EPA 82-F, EPA 82-G, EPA 82-H, and EPA 82-I. Detailed slug testing procedures are presented in the *Draft Technical Protocol for Implementing the Intrinsic Remediation with Long-Term Monitoring Option for Natural Attenuation of Dissolved-Phase Fuel Contamination in Ground Water* (Wiedemeier et al., 1994), hereafter referred to as the Technical Protocol document.

2.3.1 Slug Test Data Analysis

Data obtained during slug testing were analyzed using AQTESOLV software and the method of Bouwer and Rice (1976) and Bouwer (1989) for unconfined conditions. The results of slug testing are presented in Section 3.3.

2.4 SURVEYING

After completion of field work all new monitoring wells, soil boring locations, and those Geoprobe® sampling locations not located immediately adjacent to a CPT test location were surveyed by a State of Utah licensed professional land surveyor. Horizontal location was surveyed to the nearest 0.1 foot. Datum and ground surface elevations for were surveyed to the nearest 0.01 foot.

SECTION 3

PHYSICAL CHARACTERISTICS OF THE STUDY AREA

This section incorporates data collected during investigations as summarized by JMM (1993b) and MWI (1994a and 1994b), and more recent investigations conducted by Parsons ES in conjunction with researchers from the USEPA RSKERL in August 1993 and July 1994, to describe the physical characteristics of UST Site 870. The investigative techniques used by Parsons ES and RSKERL researchers to determine the physical characteristics of UST Site 870 are discussed in Section 2.

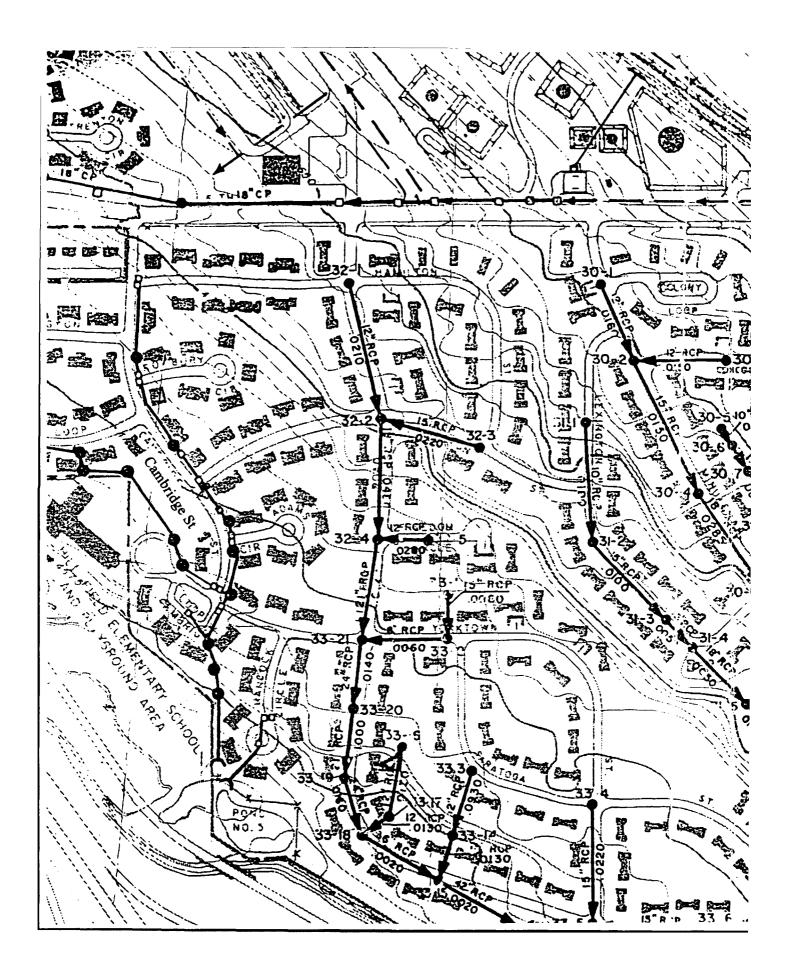
3.1 SURFACE FEATURES

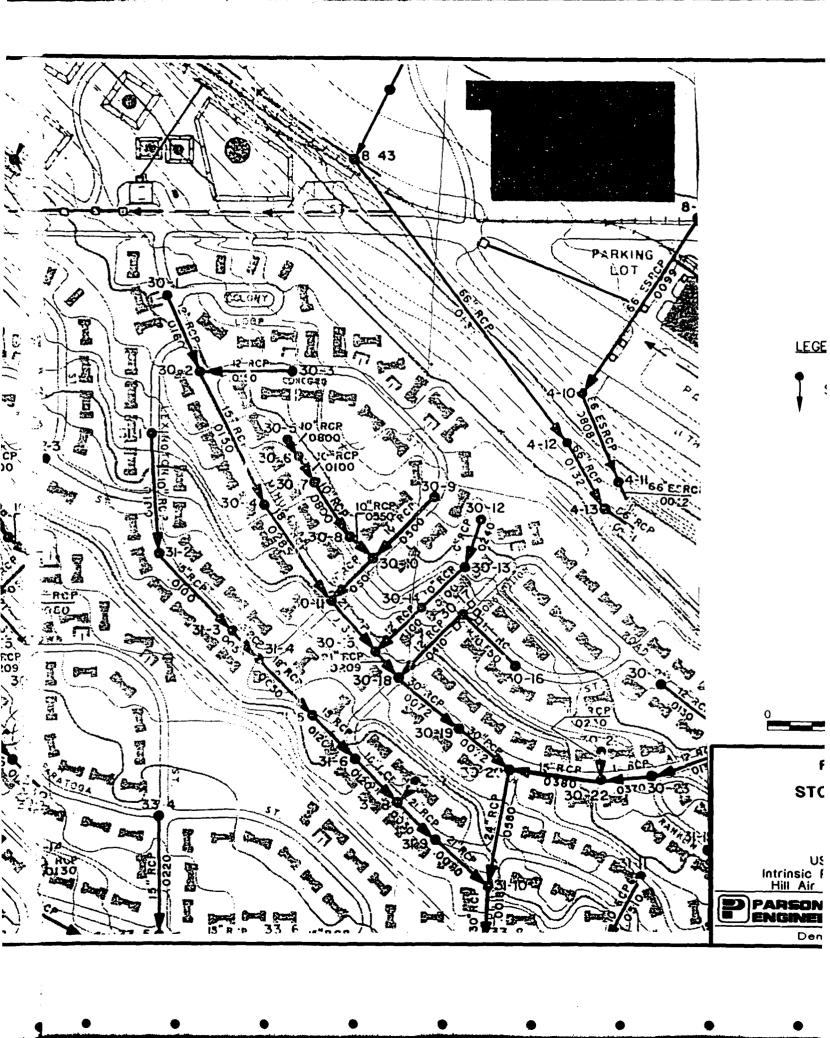
3.1.1 Topography and Surface Water Hydrology

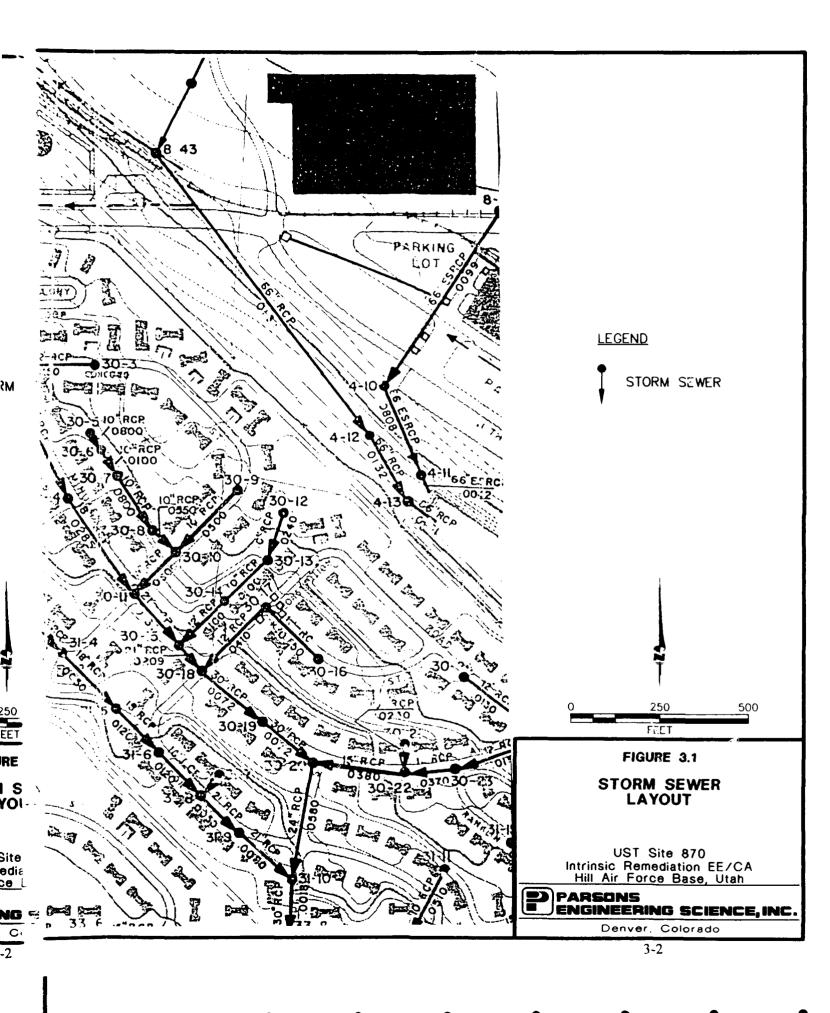
UST Site 870 is located on a plateau-like bench formed by the paleodelta of the ancient Weber River. This delta was formed as the Weber River deposited its sediment load when it entered ancient Lake Bonneville. Surface topography at the site slopes to the southwest (Figure 1.1). There are no naturally occurring surface water bodies in the immediate vicinity of UST Site 870. There are, however, several manmade features at or near the site that influence surface water runoff. These features are discussed in Section 3.1.2.

3.1.2 Manmade Features

Surface cover at UST Site 870 and adjacent areas consists of asphalt paving, grass, residential housing, concrete overlays, etc. Precipitation either infiltrates into the ground surface or is collected in gutters along the numerous roads in the Patriot Hills housing complex and diverted into several stormwater sewers in the Patriot Hills housing area. Figure 3.1 shows the locations of stormwater sewers in the area. One storm sewer, located along Cambridge Street, potentially intercepts ground water flow. There is a stormwater collection pond (Pond 5) located to the southwest of the Patriot Hills Housing Area (Figure 3.1).







3.2 REGIONAL GEOLOGY AND HYDROGEOLOGY

Three aquifers are present in the vicinity of UST Site 870. In order of increasing depth, these aquifers are the shallow aquifer, the Sunset Aquifer, and the Delta Aquifer. Hill AFB is located just west of the Wasatch Front in north-central Utah. Sediment comprising the shallow subsurface in the area consists of unconsolidated clay, silt, sand, and gravel which was eroded from the Wasatch Front and deposited as fluvial-deltaic basin-fill deposits where the ancient Weber River entered Lake Bonneville during Quaternary and Recent times (Feth et al., 1966).

The shallow aquifer in the vicinity of UST Site 870 is the subject of this study and is discussed in detail in the following sections. Insufficient data are available for ground water in the Sunset Aquifer beneath UST Site 870 to allow an assessment of ground water quality. Total dissolved solids (TDS) values for the Delta Aquifer range from 156 to 354 milligrams per liter (mg/L) (JMM, 1993b). These TDS values, and the fact that no regulated contaminants have been detected in ground water of the Delta Aquifer, allow this aquifer to be classified as Class IA (Pristine Ground Water) under Utah Administrative Code (UAC) R448-6-3.

3.3 SITE GEOLOGY AND HYDROGEOLOGY

Characterization of the vadose zone and shallow aquifer system at UST Site 870 has been the objective of several site investigations. MWI (formerly JMM) installed 44 CPT test holes (some of which contain piezometers) and 14 ground water monitoring wells (MW prefix) at UST Site 870. Figure 1.2 shows the locations of these test holes and wells. During the week of 2 August 1993, Parsons ES, in conjunction with researchers from the USEPA RSKERL, collected 17 Geoprobe® ground water samples at 9 locations (shallow and deep testing) next to the CPT locations previously investigated by MWI. During the week of 16 August 1993, Parsons ES, in conjunction with researchers from the RSKERL, drilled eight soil borings in which ground water monitoring wells were installed. These soil boreholes/monitoring wells are designated EPA-82-A. EPA-82-B, EPA-82-C, EPA-82-D, EPA-82-E, EPA-82-F, EPA-82-H, and EPA-82-I (Sample location designation EPA 82-G was used for ground water samples collected from the stormwater drain running parallel to Cambridge Street) During the week of 4 July 1994, Parsons ES, in conjunction with researchers from the RSKERL, crilled two soil borings designated EPA-82-J and EPA-82-KK. A monitoring well, designated EPA-82-J was installed in soil boring EPA-82-J. No monitoring well was installed in soil boring EPA-82-KK. Table 2.1 presents available well and piezometer completion information.

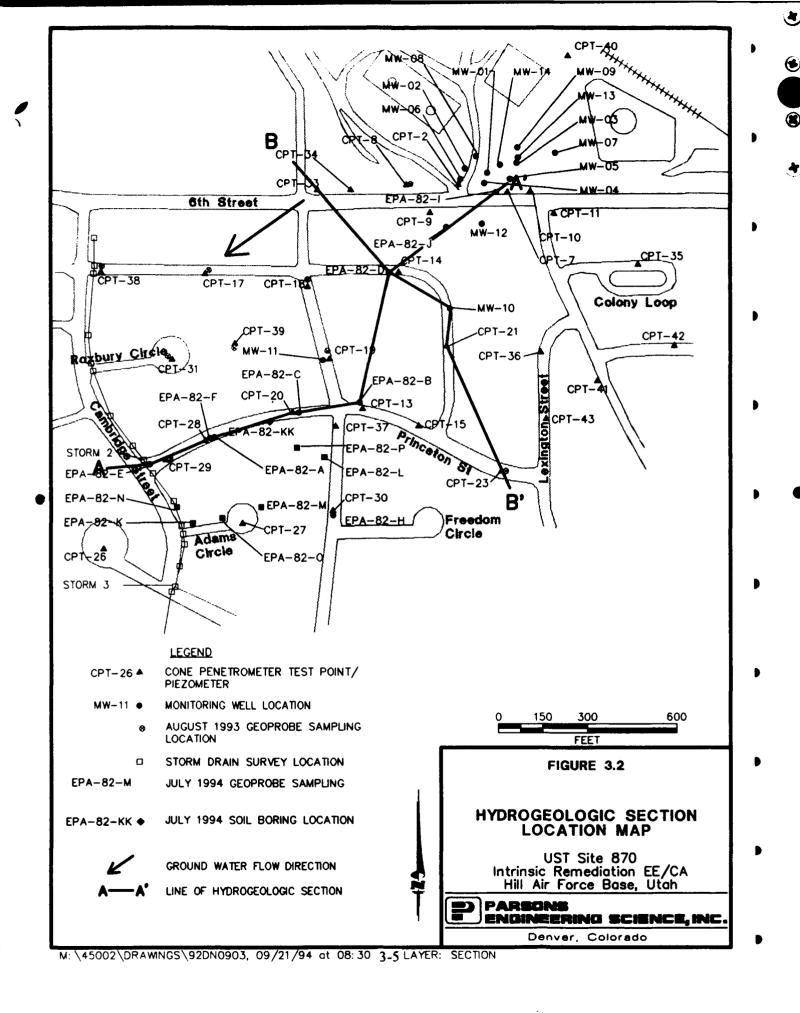
3.3.1 Lithology and Stratigraphic Relationships

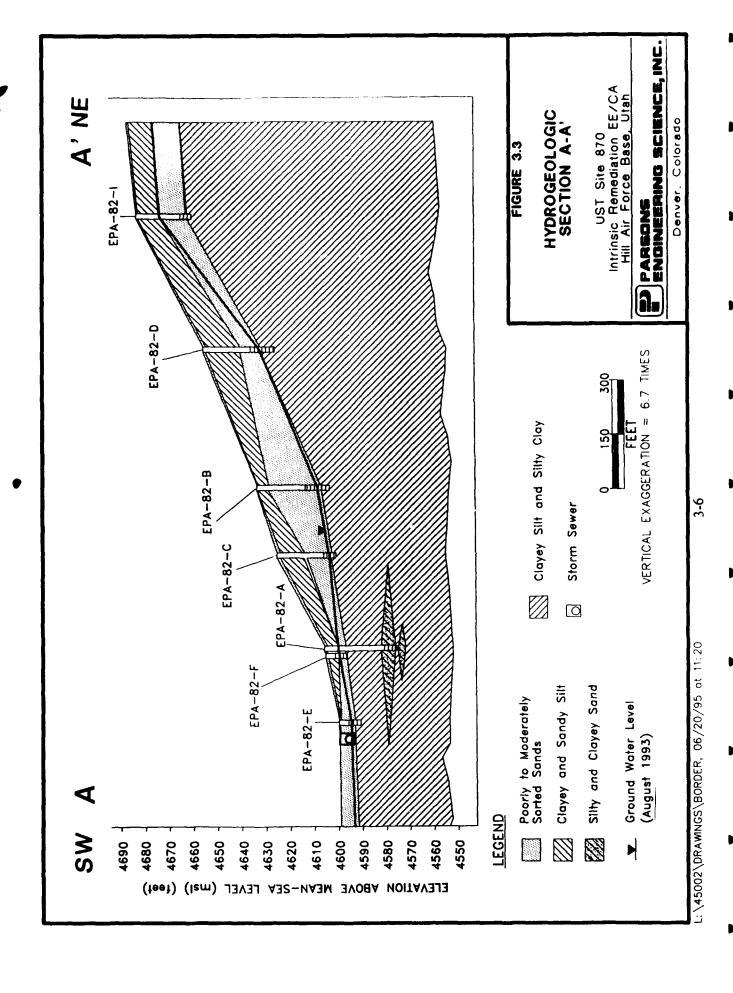
The shallow sediments underlying UST Site 870 and the Patriot Hills housing area are comprised of shallow, light reddish-brown to dark gray, cohesive clayey silts to silty clays. This clayey silt to silty clay interval ranges in thickness from approximately 4 feet to 15 feet and is abruptly underlain by poorly to moderately sorted, yellowish-brown to reddish-brown, silty fine-grained sands that coarsen downward into moderately sorted medium- to coarse-grained sands. These sands range in thickness from approximately 3 to 22 feet and the shallow saturated zone at the site occurs within these sands. Underlying the sands is a sequence of competent, thinly interbedded clay to silty clay and fine- to very-fine-grained clayey sand and silt of unknown thickness. This sequence of interbedded clay and fine-grained sand and silt appears to act as an effective barrier to the vertical migration of water and contaminants.

These stratigraphic relationships are illustrated by hydrogeologic sections A-A' and B-B'. Figure 3.2 shows the locations of these sections. Figure 3.3 presents hydrogeologic section A-A', which is oriented approximately parallel to the direction of ground water flow. Figure 3.4 presents hydrogeologic section B-B', which is oriented approximately perpendicular to the direction of ground water flow.

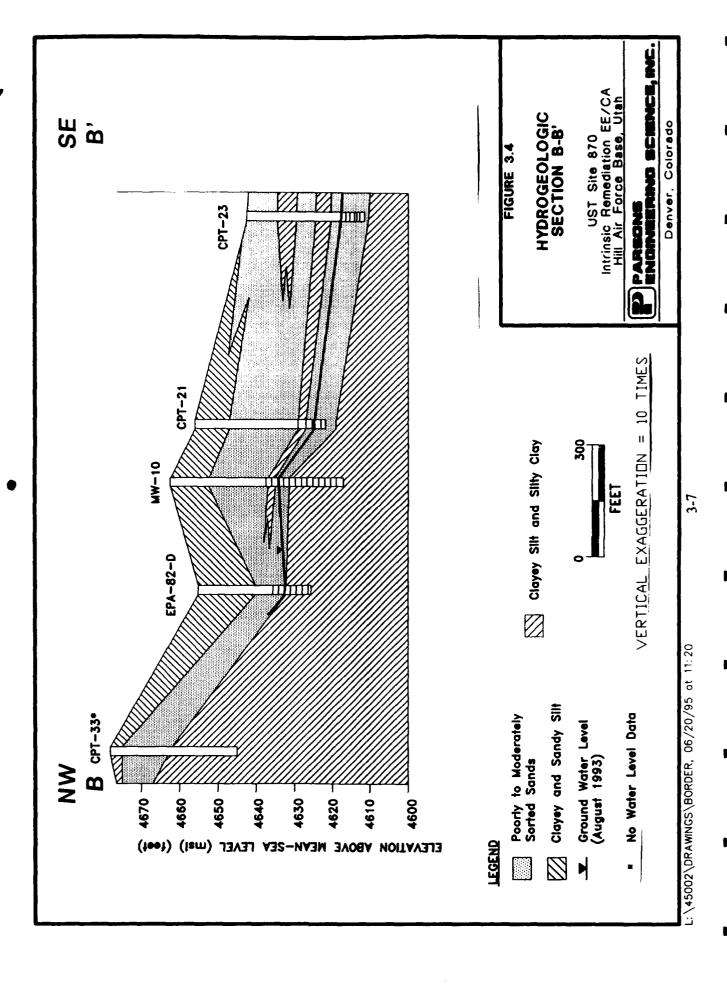
3.3.2 Grain Size Distribution

Grain size analyses were performed by JMM on soil samples from the soil borings completed as monitoring wells MW-5 (sample collected from approximately 31 feet bgs) and MW-6 (sample collected from approximately 31 feet bgs). Both samples are representative of the deep interbedded clay to silty clay and fine- to very-fine-grained clayey sand and silt described earlier. Seventy to 90 percent of the soils from both samples passed through the #200 US Standard Sieve. The #200 sieve size represents the break between fine sand and silt, and therefore these sediments are dominated by silt and clay.





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3.3.3 Ground Water Hydraulics

3.3.3.1 Flow Direction and Gradient

Ground water flow in the vicinity of UST Site 870 is to the southwest, with an average gradient of approximately 0.048 foot per foot (ft/ft) between wells EPA-82-I and CPT-27 (Figure 3.5). Available ground water elevation data are presented in Appendix B. Ground water flow appears to be limited to a relatively thin zone in the medium- to coarse-grained sands located immediately above the lower thinly interbedded clay to silty clay and fine- to very-fine-grained clayey sand and silt horizon (Figures 3.3 and 3.4). Available site data show that there is almost no seasonal variation in ground water flow direction or gradient at the site (Appendix B and MWI, 1994b).

3.3.3.2 Hydraulic Conductivity (K)

Hydraulic conductivity in the medium- to coarse-grained sands of the shallow saturated zone was estimated using rising head slug tests as described in Section 2. Slug tests were performed in monitoring wells EPA-82-A, EPA-82-E, EPA-82-F, EPA-82-H, and EPA-82-I. The results of these slug tests are summarized in Table 3.1. The average hydraulic conductivity for the shallow saturated zone as determined from these tests is 0.0159 foot per minute or 0.0085 centimeter per second (cm/sec). Appendix A contains slug test results. In addition, JMM (1991) performed two slug tests in monitoring well MW-01. The hydraulic conductivity as determined from these tests ranged from 0.00015 to 0.00018 cm/sec.

The average hydraulic conductivity estimated by Parsons ES for the shallow saturated zone is one to two orders of magnitude higher than hydraulic conductivities estimated by JMM (1993b). As illustrated in available borelogs for both Parsons ES and JMM, the heterogeneous site stratigraphy is composed of numerous soil types including moderately sorted, silty fine- to medium-grained sand, medium- to course-grained sands, cohesive clayey silts to silty clays, silty clay, and clayey sand. Slug tests performed by JMM at MW-1 were influenced by silty sands with a large interval (~4 ft) of clayey sand over the screened interval of the well. The locations selected by Parsons ES for slug testing (EPA installed wells) were characterized by predominately fine- to medium-grained sands over the well screen intervals; thus, higher values of hy audic conductivity were derived because slug tests were conducted in more transmissive soils.

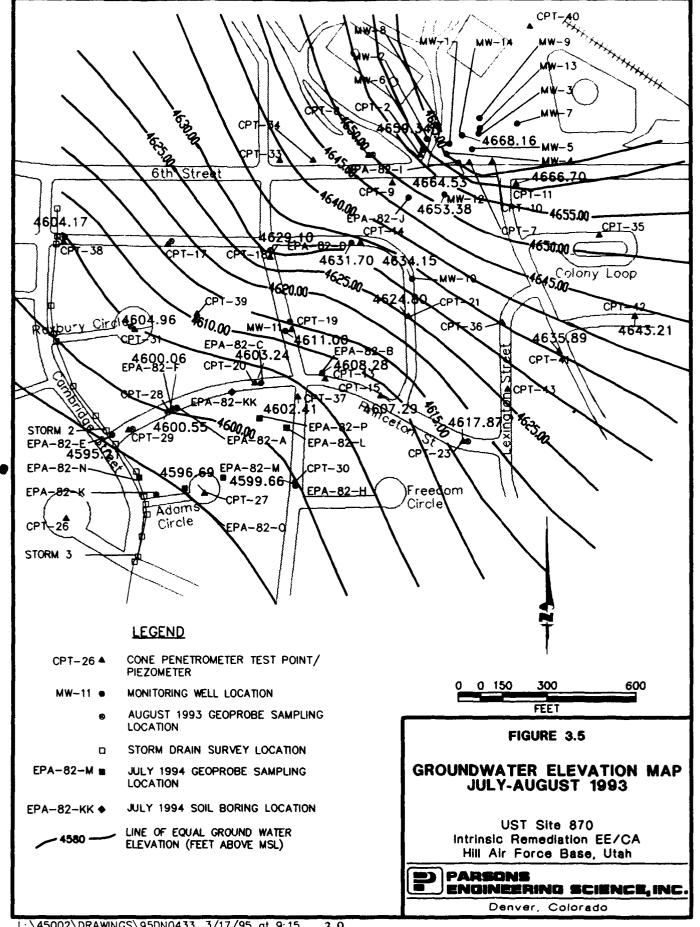


TABLE 3.1

SLUG TEST RESULTS
UST SITE 870 INTRINSIC REMEDIATION EE/CA
HILL AFB, UTAH

WELL	TEST	HYDRAULIC	HYDRAULIC
		CONDUCTIVITY	CONDUCTIVITY
		(feet/sec)	(cm/sec)
EPA 82-A	Rising Head #1	1.19E-05	3.63E-04
EPA-82-E	Rising Head #1	5.50E-04	1.67E-02
EPA-82-E	Rising Head #2	6.08E-04	1.85E-02
EPA-82-F	Rising Head #1	1.36E-04	4.13E-03
EPA-82-F	Rising Head #2	1.08E-04	3.28E-03
EPA-82-H	Rising Head #2	2.48E-04	7.56E-03
EPA-82-H	Rising Head #3	2.73E-04	8.31E-03
EPA-82-I	Rising Head #1	1.57E-04	4.77E-03
EPA-82-I	Rising Head #2	3.58E-05	1.09E-03
	AVERAGE*	2.65E-04	8.05E-03

^{*} Average of wells EPA-82-E, EPA-82-F, EPA-82-H, and EPA-82-I.

Well EPA-82-A completed in a sandy unit found within the deep silty clay

3.3.3.3 Effective Porosity (n_e)

Because of the difficulty involved in accurately determining effective porosity, accepted literature values for the type of soil comprising the shallow saturated zone were used. Freeze and Cherry (1979) give a range of effective porosity for sand of 0.25 to 0.50. To be conservative (lower effective porosity results in greater ground water velocity), the effective porosity for sediments of the shallow saturated zone is assumed to be 0.25.

3.3.3.4 Advective Ground Water Velocity $(\bar{\nu})$

The advective velocity of ground water in the direction parallel to ground water flow is given by:

$$\tilde{v} = \frac{-K}{n} \frac{dH}{dL}$$

Where: \overline{v} = Average advective ground water velocity (seepage velocity) [L/T] K = Hydraulic conductivity [L/T] (2.65 x 10⁻⁴ ft/sec) dH/dL = Gradient [L/L] (0.048 ft/ft) n_e = Effective porosity (0.25).

Using this relationship in conjunction with site-specific data, the average advective ground water velocity at the site is 4.4 feet per day (ft/day) or approximately 1,600 feet/year.

3.3.3.5 Preferential Flow Paths

Two preferential contaminant migration pathways were identified during the field work phase of this project. The first is a utility corridor on the north side of Sixth Street. This utility corridor runs parallel to Sixth Street. The influence of this corridor on contaminant migration has not been directly investigated but its influence on ground water flow is unlikely because of its relatively shallow depth.

The second potential preferential contaminant migration pathway is a storm sewer that intersects ground water flow in at least a portion of the site near Cambridge Street. This storm sewer is located along Cambridge Street (Figure 3.1). During field work conducted by Parsons ES and RSKERL personnel in August 1993, ground water appeared to be flowing in this storm sewer near the intersection of Cambridge and Princeton streets. The possibility that this water was ground water was supported by ground water elevation data and surveyor's data collected at several points along the storm sewer (e.g., culvert invert elevation data, see Figure 3.3). To determine if contaminated ground water was being intercepted by this storm sewer, two water samples, storm-2 and storm-3, were collected at the locations shown in Figure 1.2. The analytical results for these samples indicated that no ground water contamination was being intercepted by the storm drain in August 1993.

3.3.5 Ground Water Use

Ground water from the surficial aquifer at Hill AFB is not extracted for potable uses. Water is obtained from on-base deep supply wells in the months of October through April. Water is supplied by a combination of deep supply wells and water piped in from the nearby Weber Basin Water Conservancy District during the remainder of the year.

3.4 CLIMATOLOGICAL CHARACTERISTICS

Regional climatological characteristics for the site were obtained from an AWS Climatic Brief. Meteorology at the site is impacted by the Wasatch Range located west of the site. This range is oriented north-south and rises over 5,000 vertical feet above the valley floor in less than 5 miles, causing an abrupt barrier for Pacific frontal systems moving into northern Utah. This barrier, coupled with moisture from the Great Salt Lake, causes fronts to build up over Hill AFB, resulting in low cloud ceilings and prolonged periods of precipitation.

Monthly mean high temperatures range from about 27 °F in January to about 76 °F in July. Recorded extreme high and low temperatures for the period from 1941 to 1984 were 104 °F and - 13 °F, respectively. Mean annual precipitation for this same period is 20.1 inches.

SECTION 4

NATURE AND EXTENT OF CONTAMINATION AND SOIL AND GROUND WATER GEOCHEMISTRY

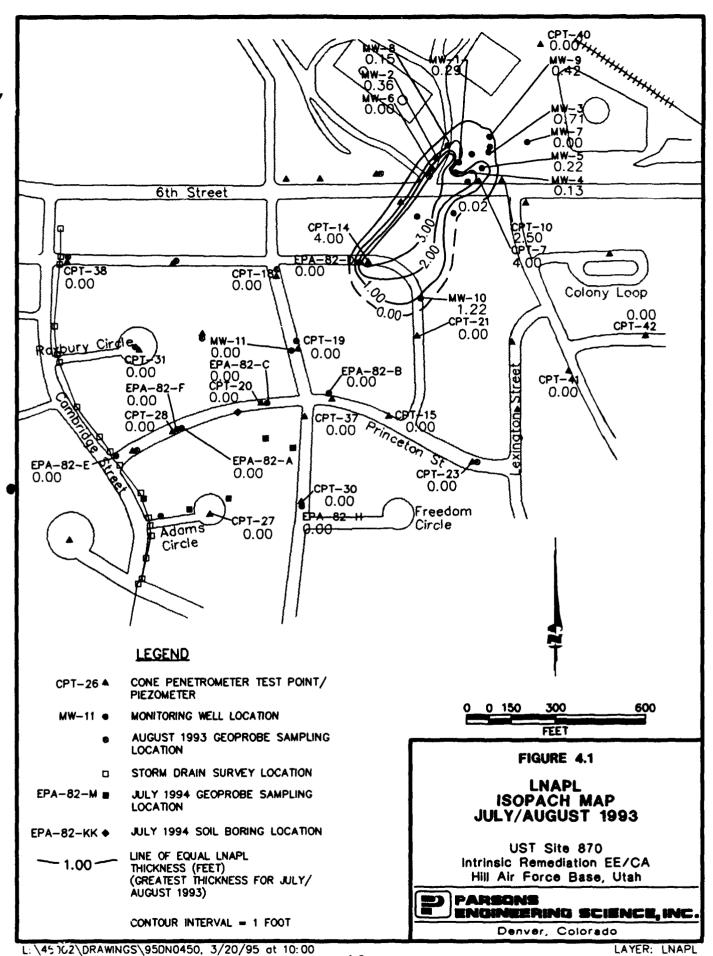
4.1 SOURCE OF CONTAMINATION

The source of contamination at UST Site 870 it not known with any degree of certainty, nor is it known how much fuel leaked into the subsurface. About 700 gallons of LNAPL have been recovered by product recovery systems since their installation in June 1992. Former UST 870.0 may have contributed to the contamination observed at the site, but it is unlikely that leakage from this UST was responsible for all of the contamination. This UST was used to store condensate and residual JP-4 generated by operations at a nearby filter stand. Following the removal of UST 870.0, a new tank equipped with leak-detection equipment was installed in the same excavation. Based on the large quantity of contamination, other potential sources of contamination include: leaky piping associated with the UST, surface spills and releases from operations since the 1940s, and a faulty 6-inch diameter pipe located behind the pump facility Building 870 (pending repairs).

4.2 SOIL CHEMISTRY

4.2.1 Mobile LNAPL Contamination

Mobile LNAPL is defined as the LNAPL that is free to flow in the aquifer and that will flow from the aquifer matrix into a well under the influence of gravity. Mobile LNAPL is present in several monitoring wells and piezometers at the site (Appendix B). Figure 4.1 is an isopach map showing the distribution and measured thickness of mobile LNAPL at the site in July and August 1993. This map was prepared using the greatest mobile LNAPL thickness measured at each location during this period. The LNAPL plume appears to be comprised of weathered JP-4 that emanates from the aboveground storage tank facility. Figure 4.1 suggests that the LNAPL plume extended approximately 750 feet downgradient from the source area in July/August 1993. The areal extent of suspected mobile LNAPL contamination is approximately 225,000 square



4-2

feet. Concentrations of BTEX and trimethylbenzene (TMB) constituents in the mobile LNAPL were quantitated using a sample of LNAPL collected from MW-10 in August 1993. Concentrations of BTEX and TMBs in this sample indicate that the JP-4 comprising the LNAPL plume in this area is significantly weathered. Table 4.1 compares BTEX concentrations in fresh JP-4 to those observed in LNAPL from MW-10. Toluene and benzene concentrations are reduced by 1 to 3 orders of magnitude, respectively, and ethylbenzene and total xylene concentrations are reduced by about one-half.

TABLE 4.1

COMPARATIVE FRESH AND WEATHERED

LNAPL BTEX ANALYTICAL RESULTS

UST SITE 870 INTRINSIC REMEDIATION EE/CA

HILL AFB, UTAH

Contaminant	Concentration in Fresh JP-4 (mg/L)	Concentration in Weathered JP-4 from MW-10 (August, 1993) (mg/L)
Benzene	3750	1
Toluene	9975	134
Ethylbenzene	2775	1020
o-xylene	7575	2380
m -xylene	7200	5500
p-xylene	2625	1070

The relationship between measured LNAPL thickness and the amount of mobile LNAPL in the subsurface at a site is extremely difficult to quantify. Based on soil core data and measured LNAPL thicknesses, there appears to be a significant difference between measured LNAPL thickness and the actual thickness of mobile LNAPL present at the site. It is well documented that LNAPL thickness measurements taken in ground water monitoring wells are not indicative of actual mobile LNAPL thicknesses in the formation (Kemblowski and Chiang, 1990; Concawe, 1979; Abdul et al., 1989; Testa and Paczkowski, 1989; Hughes et al., 1988; Blake and Hall, 1984; Hall et al., 1984; Hampton and Miller, 1988; Mercer and Cohen, 1990; de Pastrovich et al.,

1979; Lehnard and Parker, 1990; Ballestero, et al., 1994). It has been noted by these authors that the thickness of LNAPL measured in a monitoring well is greater that the actual mobile LNAPL thickness present in the aquifer and, according to Mercer and Cohen (1990), measured LNAPL thickness in wells is typically 2 to 10 times greater than the actual mobile LNAPL thickness in the formation.

4.2.2 Residual-Phase (Stationary) LNAPL Contamination

Residual-phase LNAPL is defined as the LNAPL that is trapped in the aquifer by the processes of cohesion and capillarity and therefore will not flow within the aquifer and will not flow from the aquifer matrix into a well under the influence of gravity. The following sections describe the residual-phase LNAPL contamination found at UST Site 870.

4.2.2.1 Soil BTEX Contamination

Residual-phase BTEX contamination resulting from vertically and laterally migrating LNAPL is found over a wide area at UST Site 870. Table 4.2 contains soil BTEX and TPH data. Figure 4.2 is an isopleth map showing maximum observed total BTEX concentrations in soil at UST Site 870. Soil BTEX contamination appears to extend approximately 1,600 feet downgradient from the source area and is approximately 500 feet wide at the widest point. The highest observed concentration of residual-phase BTEX is 554 mg/kg in a soil core sample taken from approximately 18 feet bgs in soil boring EPA-82-I, which is in the suspected source area of JP-4 contamination. This corresponds with the highest measured TPH concentration of 28,300 mg/kg. Measured total BTEX concentrations decrease rapidly in areas devoid of mobile-phase LNAPL contamination, and the majority of the area shown in Figure 4.2 is characterized by total BTEX concentrations of less than 50 mg/kg.

4.2.2.2 Soil TPH Contamination

Figure 4.3 is an isopleth map showing TPH concentrations in soil. This figure shows that elevated TPH concentrations are widespread at the site. TPH levels exceed 28,000 mg/kg at EPA-82-I. TPH contamination appears to extend downgradient from the source area for approximately 1,600 feet with an approximate width of 450 feet. The vertical thickness of TPH

TABLE 4.2
FUEL HYDROCARBON COMPOUNDS DETECTED IN SOIL
UST SITE 870 INTRINSIC REMEDATION EE/CA
HILL AFB, UTAH

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	irn (mg/kg)	Ϋ́	Y X	¥Z.	NA	٧V	¥	¥	¥	A	٧X	٧×	¥	٧X	¥	Ϋ́Z	Ϋ́	¥	¥	ž	٧	٧N	¥Z	٧X	٧	٧N	NA	NA	¥	V.	٧X	Ϋ́Z	¥	¥Z	NA	٧Z	¥	ΝA	٧X
1,2,3-	(mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	10.0 >	< 0.01	< 0.01	< 0.01	10:0 >	10.0 >	0.0>	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	100>	< 0.01	< 0.01	100>	10'0 >	< 0.01	< 0.01	< 0.01	< 0.01	0.0 >
1,2,4	(mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	10.0 >	10.0 >	< 0.01	< 0.01	< 0.01	10.0 ×	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
1,3,5-	(mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	> 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	10 ⁰ >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10:0 >	< 0.01	< 0.01	< 0.01	10.0 >	0.0 >	< 0.01	10.0 >	< 0.01	10.0 >
Total	(mg/kg)	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	10.0>	<0.01	<0.01	<0.01	<0.01	<0.01	10.0>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	10:0>	<0.01	<0.01	<0.01	<0.01	10'0>
Total	Aylenes (mg/kg)	<0.01	<0.01	<0.01	<0.01	<0.01	10.0>	10.0>	10.0>	<0.01	10.0>	10.0>	<0.01	10.0>	10.0>	<0.01	<0.01	<0.01	10.0>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	10.0>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01
	(mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	> 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	_ < 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	10.0 >
M&P.	Aylene (mg/kg)	Ϋ́	VA V	ΥA	NA	NA	Y.A	٧٧	Ϋ́	NA	٧N	٧V	VΑ	٧X	Ϋ́Z	ΑN	٧Z	Ϋ́Z	٧X	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	ΥN	ΥX	٧Z	٧X	NA	NA	ΑN	NA	Y.
	M-Aylene (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	10.u >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
	r-Aylene (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	> 0.01	< 0.01	< 0.01	< 0.01	10'0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Lat. II	(mg/kg) (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01
	(mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10:0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
	(mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Interval	(fi bgs)	19.00	19.25	19.50	19.75	20.00	20.25	20.50	20.75	21.00	21.25	21.50	21.75	22.00	22.25	22.50	22.75	23.00	23.40	23.80	24.20	24.60	25.00	25.40	25.80	26.20	27.30	27.60	27.90	28.20	28.50	28.80	29.10	29.40	29.70	30.00	30.30	30.60	30.90
Sample Interval	(u bgs)	18.75	10.00	19.25	19.50	19.75	20.00	20.25	20.50	20.75	21.00	21.25	21.50	21.75	22.00	22.25	22.50	22.75	23.00	23.40	23.80	24.20	24.60	25.00	25.40	25.80	27.00	27.30	27.60	27.90	28.20	28.50	28.80	29.10	29.40	29.70	30.00	30.30	30.60
	Sample Date	8/17/93	8/17/93	8/17/93	8/11/93	8/17/93	8/11/93	8/17/93	8/11/83	8/17/93	8/11/83	8/11/83	8/11/93	8/17/93	8/17/93	8/11/83	8/17/93	8/17/93	8/17/93	8/11/83	8/11/93	8/17/93	8/17/93	8/17/93	8/17/93	8/17/93	8/17/93	8/17/93	8/17/93	8/17/93	8/17/93	8/17/93	8/11/83	8/11/93	8/17/93	8/17/93	8/17/93	8/11/93	8/17/93
٠	Sample Location	82 A-16	82 A-15	82 A-14	82 A-13	82 A-12	82 A-11	82 A-10	82 A-09	82 A-08	82 A-07	82 A-06	82 A-05	82 A-04	82 A-03	82 A-02	82 A-01	82 A-25	82 A-24	82 A-23	82 A-22	82 A-21	82 A-20	82 A-19	82 A-18	82 A-17	82 A-41	82 A-40	82 A-39	82 A-38	82 A-37	82 A-36	82 A-35	82 A-34	82 A-33	82 A-32	82 A-31	82 A-30	82 A-29

TABLE 4.2 (Continued) FUEL HYDROCARBON COMPOUNDS DETECTED IN SOIL UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

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	TPH (mg/kg)	٧V	NA	NA	٧X	Y.	٧X	Y.	Ϋ́Z	۲×	٧X	٧Z	٧X	٧Z	٧Z	٧Z	¥z	AN	₹ Z.	4Z	¥	۲×	¥	¥	¥	Ϋ́	ž	NA	¥Z	¥	¥Z	¥.	Y.	٧×	٧×	٧Z	NA NA	٧V	Y.
12.3	TMB (mg/kg)	< 0.01	< 0.01	< 0.01	10.0 >	10'0 >	< 0.01	< 0.01	10 ⁰ 0 >	< 0.01	10.0 >	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	10.0 >	< 0.01	10.0 >	< 0.01	0.0 >	< 0.01	< 0.01	< 0.01	< 0.01	10'0 >	< 0.01	10'0 >	10.0 >	< 0.01	< 0.01	10.0 >	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
1.2.4-	TMB (mg/kg)	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	10'0 >	< 0.01	10.0 ×	10.0 >	< 0.01	10.0 >	10.0 >	< 0.01	0.0 >	10.0 >	10.0 >	10.0 >	< 0.01	< 0.01	10.0 >	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	> 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01
13.5-	TMB (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10 ⁰ 0 >	< 0.01	< 0.01	> 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	> 0.01	10.0 >	< 0.01	< 0.01	< 0.01	10:0 >	< 0.01	< 0.01
Total	BTEX (mg/kg)	<0.01	<0.01	<0.01	10.0>	10.0>	<0.01	<0.01	10.0	<0.01	<0.01	<0.01	10:0>	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	10:0>	<0.01	<0.01	10:0>	<0.0>	<0.01	<0.01	< 0.01	< 0.01	<0.01	<0.01	10.0>	10:0>	10.0>	<0.01	<0.01	10.0>	<0.01	<0.01
Total	Xylenes (mg/kg)	<0.01	<0.01	10.0>	<0.01	10.0>	<0.01	13.0>	10.0>	<0.01	<0.01	<0.01	<0.01	10.0>	<0.01	<0.01	10.0>	70.0>	10:0>	(0.0)	10.0>	<0.01	<0.01	<0.0	<0.01	<0.01	<0.01	< 0.01	< 0.01	<0.01	10.0>	10.0>	<0.01	10.0>	<0.01	<0.01	<0.01	<0.01	<0.01
	O-Xylene (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	> 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
M&P-	Xylene (mg/kg)	NA	NA	NA	NA	NA NA	Ϋ́Z	Ϋ́	ΥN	Ϋ́	ΥN	VA	VA V	٧V	Ϋ́Z	VΝ	Y.	ΥN	¥	NA NA	ΑN	٧X	ΝA	Ϋ́N	Ϋ́	NA	NA	NA	NA	Y.	٧Z	ΥN	NA	٧Z	N.	٧X	NA A	NA	٧V
	M-Xylene (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	> 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
	P-Xylene (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 ×	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
	Ethylbenzene (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
	Toluene (mg/kg)	< 0.01	< 0.01	< 0.01	10'0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01
	Benzene (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	10'0 >	< 0.01	< 0.01	10.0 >	< 0.01	< 0.01	< 0.01
nterval	Bottom (ft bgs)	31.20	31.50	31.80	32.10	32.40	32.70	33.00	33.30	33.FA	33.90	34.20	34.50	34.80	35.10	35.40	20.30	20.60	20.90	21.20	21.50	21.80	22.10	22.40	22.70	23.00	23.30	23.60	23.90	24.10	24.40	24.70	25.00	25.30	25.60	25.90	26.10	26.40	26.70
Sample Interval	Top (ft bgs)	30.90	31.20	31.50	31.80	32.10	32.40	32.70	33.00	33.30	33.60	33.90	34.20	34.50	34.80	35.10	20.00	20.30	20.60	20.90	21.20	21.50	21.80	22.10	22.40	22.70	23.00	23.30	23.60	23.90	24.10	24.40	24.70	25.00	25.30	25.60	25.90	26.10	26.40
	Sample Date	8/11/83	8/17/93	8/11/83	8/11/83	8/17/93	8/11/83	8/11/83	8/11/83	8/12/93	8/11/83	8/11/83	8/11/83	8/11/83	8/11/93	8/11/83	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	66/81/8	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93
	Sample Location	82 A-28	82 A-27	82 A-54	82 A-53	82 A-52	82 A-51	82 A-50	82 A-49	82 A-48	82 A-47	82 A-46	82 A-45	82 A-44	82 A-43	82 A-42	82 B-12	82 B-11	82 B-10	82 B-09	82 B-08	82 B-07	82 B-06	82 B-05	82 B-04	82 B-02	82 B-01	NSN	NSN	82 B-24	82 B-23	82 B-22	82 13-21	82 B-20	82 B-19	82 B-18	82 B-17	82 B-16	82 B-15

TABLE 4.2 (Continued)
FUEL HYDROCARBON COMPOUNDS DETECTED IN SOIL
UST SITE 870 INTRINSIC REMEDATION EE/CA
HILL AFB, UTAH

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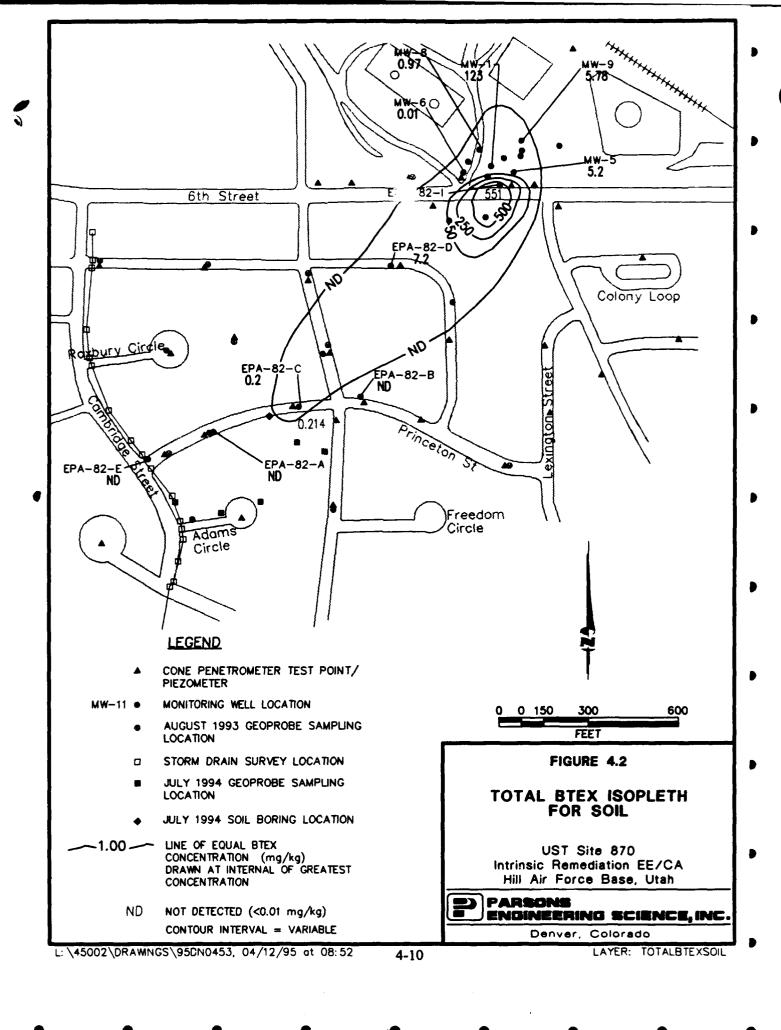
				_	_	, ,	_	_		_			_		_	_		-					_							_									
	H	(mg/kg)		۲	Y'A	0.01 >	< 10.0	0 01 >	0'01 >	352	173	580(EST)	444	< 10.0	> 10.0	٧Z	< 10.0	0 01 >	001>	> 10.0	2	001	001 >	0 01 ×	¥X	¥Z.	AN.	< 10.0	0.01 ×	> 10.0	< 10.0	Ϋ́Z	٧Z	۲Z	Ϋ́	YZ YZ	AN	A'N	ž
	1,2,3- TMB	(mg/kg)		< 0.01	< 0.01	0.0145	0.0229	0.00363	0.00813	0.905	0.208	0.0553	0.108	0.00491	< 0.01	10.0 >	BLOI	0.0548	000311	BIOI	N C) 	0.817	BLOI	< 0.01	0.00821	< 0.01	< 0.01	0.0213	0.0127	0.00518	BLQI	BLQ1	0.0163	BLQI	0.0384	< 0.01	10.0 ×	10.0 ×
	1,2,4. TMB	(mg/kg)		< 0.01	< 0.01	0.0371	0.054	0.0168	0.0741	4.42	708	1.03	1.16	0.0167	< 0.01	< 0.01	0.00498	0.225	0.00885	BLOI	0.0000	0 44	=	00111	0.0031	0.078	BLQ1	BLQI	0.0399	0.0303	0.0695	0.00572	0.00416	0.0373	BLQ1	0 0 1 0 7	< 0.01	< 0.01	100>
	1,3,5- TMB	(mg/kg)		× 0.01	> 0.01	0.029	0.0388	0.0148	0.0801	37	2.34	1.5	1.65	0.0135	< 0.01	< 0.01	BLQ1	0.195	0.0174	0.00416	0 00744	0.373	2.53	0.0304	0.00477	0.0882	0.0258	0.0147	0.0365	0.0433	0.0637	0.00871	0.00632	0.0439	0.0077	0.0733	< 0.01	< 0.01	< 0.01
- 1 - 1 - 1 - 1 - 1	BTEX	(mg/kg)	,	10.0>	>0.01	0.07856	0.1002	0.03735	0.02733	0.20377	0.07451	0.06649	0.10/01	<0.01	<0.01	<0.01	BLQI	0.06132	0.00671	0.02549	0.04454	1.368	7.503	0.1937	0.10833	0.11855	0.03232	0.0276	0.37704	0.3144	0.2305	0.19931	0.15654	0.3754	0.1847	0.35609	-0°0 	<0.01	<0.01
10,01	Xylenes	(mg/kg)	100	0.0	10.0	0.000/0	0.06/8	0.0294	0.0294	61519	0.04606	0.04271	0.0828	10.02	10.0>	<0.01	BLQ1	0.05261	0.00336	BLQ1	0.02364	0.975	5.752	0.013	0.00303	0.04986	BLQ!	BLQI	0.2811	0.1923	0.0856	0.03981	0.02124	0.173	0.0189	0.1807	10 O	900	-0.0 -0.0
	O-Xylene	(mg/kg)	100	10.0	10.0	0.00/16	0.0130	BLQI	BLQ	BLOI	BLQI	0.00401	10.0	0.01	> 0.01	< 0.01	BLQI	0.00451	BLQI	BLQ1	0.00359	0.144	0.732	BLQI	BLQ!	0.00577	BLQ	BLC	0.045	0.0323	BLQ1	0.00476	BLQI	0.0242	0.00486	0.0692	10.0	< 0.01	< 0.01
H&P.	Xylene	(mg/kg)	V N	5 2	V 2	¥ 2	2 2	Y S	¥ i	¥ S	¥ ×	\$ \$		5	NA.	ž	¥Z	NA	NA	NA	٧V	ΑN	٧V	ΝA	Ϋ́	¥.	¥.	¥:	ž	¥Z,	¥.	¥.	٧.	٧ ک	¥	ž	≨ Ž	ž	¥
	M-Xylene	(mg/kg)	1002	100	8170	0.0410	00100	0.0109	0.00091	0.0002	0.0000	0.0001	1000	10.0	0.0	< 0.01	10.0 ×	0.0345	0.00336	BLQ1	0.0143	0.555	3.4	BLQI	0.00303	0.00529	BLC	5	0.18	0.121	0.0194	0.0275	0.016	171.0	0.00404	0 0	0.0	10.0	< 0.01
	P-Xylene	(mg/kg)	100>	100>	0.0178	0.0271	00100	0010	0.0867	0.003/	0000	0.042	100>	100		10.01	BLQI	0.0136	BLQI	BLOI	0.00575	0.276	1.62	0.013	BLOI	0.0388	2010	10000	0.031	0.039	0.0002	0.00/35	0.00434	0.03/0	200	coro	10.0		< U.UI
	Ethylbenzene	(Mg/Kg)	100>	10.0 >	81100	0.0124	0.00795	0.00642	786	0.00558	819000	8100	100>	100	100	10.0	מרכו	0.00871	0.00335	0.0159	0.0106	0.264	1.48	0.111	0.0949	0.0004	0.0344	1900	87800	0.0078	0.124	0.141		1,10	0.137	0.128	10.0	000	10.01
	Toluene	(Mg/Kg)	< 0.01	> 0.01	BLOI	1019	BIO	BIOI	000	0.0197	9/10/0	100>	100>	100>		70		DICO.	BCC)	BCO	BLQI	BLQ	BLQI	BLQ1	200		3 0	0.00304	2002	2018	200	7 2			00000	40000	1000	000	10.0
	Benzene	(IIIE/AB)	< 0.01	< 0.01	BLOI	BLOI	BLOI	BLOI	0.00327	0.00367	10.0 ×	0.00621	< 0.01	Τ	Τ	Т	T	DEC.	7,	7	1	ヿ゙	T	0.0697	7	+		T	十	Ť	+	✝	Ť	†	Ť	†	T	T	1
Sample Interval	Bottom	(11.083)	27.10	27.40	20.20	20.50	20.80	21.10	21.40	21.55	21.70	22.00	22.30	22.60	21.80	22.10	22.40	22.40	22.80	24:00	24.10	24.40	24.70	36.55	26.50	26.20	26.50	26.80	27.00	27.30	27.60	27.80	28.20	28 50	28.80	88	330	\$ 25	1
Sample	Top (a hos)	(", UE3)	26.70	27.10	19.90	20.20	20.50	20.80	21.10	21.40	21.55	21.70	22.10	22.30	21.50	21.80	22.10	22.10	73.90	24.00	24.00	24.10	25.40	0/ 57	25.60	25.90	26.20	26.50	26.80	27.00	27.30	27.60	28.00	28 20	28 50	2.70	3.00	4 90	1
	Sample	7,000	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/18/93	8/20/93	8/20/93	8/20/03	8/20/03	6/10/03	6/20/63	6/20/20	6/20/93	6/20/9	6/20/93	8/20/03	8/20/93	8/20/93	8/20/93	8/20/93	8/20/93	8/20/93	8/20/93	8/20/93	8/20/93	8/20/93	8/21/93	8/21/93	8/21/93	
	Sample		82 B-14	82 B-13	82 C-26	82 C-25	82 C-24	82 C-23	82 C-22	82 C-21	82 C-20	82 C-19	82 C-16	82 C-14	82 D-06	82 D-05	82 D-04	82 D.03	87 701	20.00	62 17-7	82 D-24	67 17 29	82 D.21	82 D-19	82 D-18	82 D-17	82 D-16	82 D-15	82 D-14	82 D-13	82 D-12	82 D-40	82 D-39	82 D-38	82 E-03	82 E-02	82 E-17]

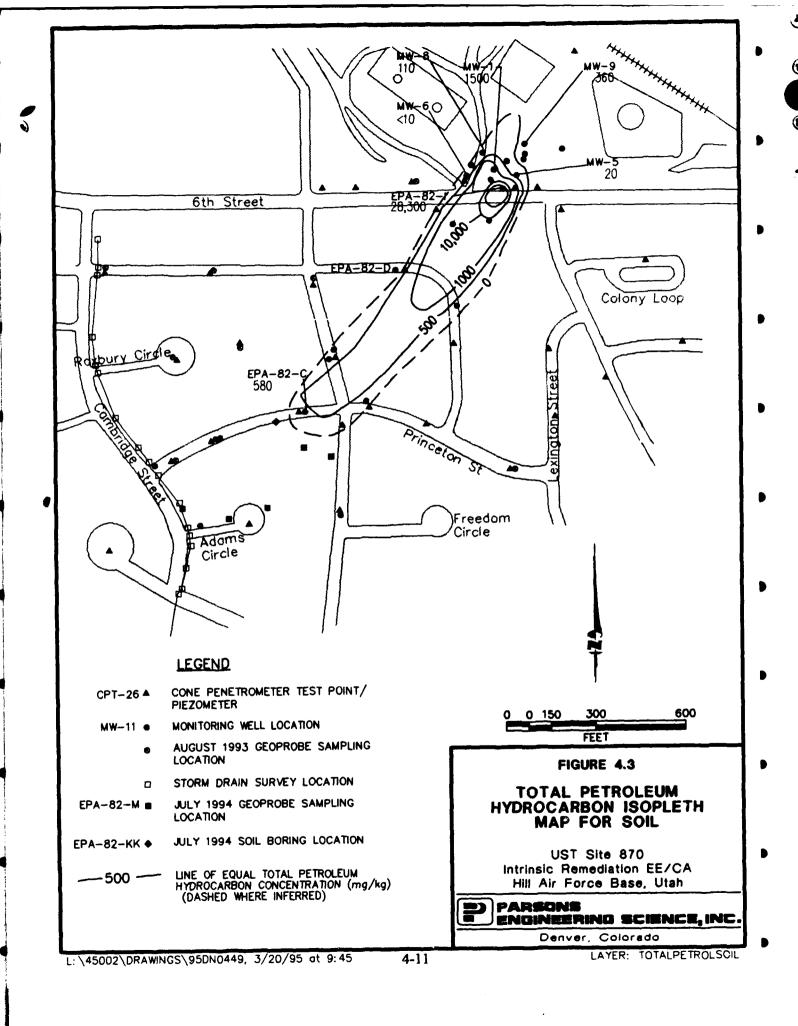
TABLE 4.2 (Continued)
FUEL HYDROCARBON COMPOUNDS DETECTED IN SOIL
UST SITE 870 INTRINSIC REMEDATION EE/CA
HILL AFB, UTAH

	TPH (me/kg)	4×	Ϋ́	¥X	٧X	NA A	٧X	¥X	٧Z	¥z	¥z	138	139	3530	۲Z	11500	28300	5160	6080	< 10.0	> 10.0	< 10.0	< 10.0	< 10.0	0 01 ×	¥	¥	¥	276	856(EST)	0.01 >	643	< 10.0	< 10.0	6	> 100	< 10.0	< 10.0	< 10 0
1,2,3-	TMB (mg/kg)	10.0 >	10.0 >	< 0.01	BLQI	10.0 >	BLQ1	BLQI	BLQ1	BLQI	< 0.01	BLQI	BLQ1	18.5	19.3	15.4	59.2	25.3	17.1	0.272	8560	6060.0	0 0749	0.155	6680.0	0.0783	0.0709	8/2/0.0	1.25	2 34	0.472	2.03	0.823	0.031	1.5	0 00937	< 0.01	100 >	100>
1,2,4-	TMB (mg/kg)	10.0 >	10.0 ×	10.0 >	BLQI	49.9	6.08	42.7	167	8.69	4.43	0 724	2.54	0.244	0.195	0.402	0.246	0.206	161.0	0.222	4.72	8.37	2.33	8.45	3.3	0.113	5.38	17.2	BLQI	10.0 >	BLQ1								
1,3,5-	TMB (mg/kg)	< 0.01	< 0.01	< 0.01	BLQI	BLQI	BLQI	BLQI	BLQ1	BLQI	BLQI	BLQI	BLQ1	28.1	29.3	23.3	88.8	36.8	2.3	0.384	1.24	0.103	0.0743	0.157	0.0938	9620.0	0.0747	0.0843	1.62	3.04	0.857	2.94	1.27	0.031	2.32	0.0121	BLQI	10'0 >	BLQI
Total	BTEX (mg/kg)	10:0>	<0.01	<0.01	<0.01	BLQI	0.00543	BLQ1	0.00408	BLQ1	BLQI	BLQI	BLQI	105.3592	119.414	110.482	553.98	200.801	7.198	5.787	14.009	2.77	2.25	4.087	2.1866	2.025	1.8616	1.9595	7.374	19.494	6.87	24.181	6.8594	0.797	20.224	0.3316	0.02201	16.1073	271172
Total	Xylenes (mg/kg)	<0.01	<0.01	<0.01	<0.01	BLQI	0.00543	BLQ1	0.00408	BLQI	BLQI	BLQI	BLQI	8:06	106.4	105.4	499	170.3	6.5	3.19	8.48	1.486	1.154	2.154	1.172	1.166	1.128	1.076	5.318	14.86	5.03	20.80	90.6	0.3422	19.91	0.2112	0	0	
	O-Xylene (mg/kg)	< 0.01	< 0.01	< 0.01	BLQI	BLQI	BLQI	BLQI	BLQI	BLQ1	BLQI	BLQI	BLQI	18.2	19.9	20.8	100	36.6	19.1	0.725	2.04	0.403	0.31	0.567	0.318	0.321	0.303	0.316	2.31	5.28	1.72	5.58	1.03	0.129	4.79	0.085	BLQI	< 0.01	< 0.01
M&P-	Xylene (mg/kg)	Ϋ́N	NA	٧X	Ϋ́	٧×	NA VA	٧V	NA	N A	NA	¥.	V.	Ϋ́	۲	NA A	Y.	NA A	NA	NA.	ΝA	Ϋ́	Y X																
	M-Xylene (mg/kg)	< 0.01	< 0.01	< 0.01	BLQ:	BLQI	0.00543	BLQI	0.00408	BLQI	BLQI	BLQ1	BLQ1	52.7	63.1	62.3	294	99.3	3.67	1.84	4.74	0.802	0.616	1.16	0.621	0.612	0.604	0.517	9860	4.89	1.83	10.5	2.28	0.0592	7.86	0.0898	< 0.01	< 0.01	< 0.01
	P-Xylene (mg/kg)	< 0.01	< 0.01	< 0.01	BLQ1	BLQI	BLQI	BLQ1	BLQ1	BLQ1	BLQI	BLQI	BLQ1	19.9	23.4	22.3	105	34.4	1.22	0.625	1.7	0.281	0.228	0.427	0.233	0.233	0.221	0.243	2.02	4.69	1.48	4.81	1.75	0.154	3.96	0.0364	BLQI	< 0.01	< 0.01
	Ethylbenzene (mg/kg)	< 0.01	< 0.01	< 0.01	BLQI	BLQ1	BLQ1	BLQ1	BLQI	BLQI	BLQI	BLQI	BLQi	14.5	11.2	4.83	47.7	17.5	0.556	0.377	1.03	0.187	0.15	0.283	0.15	0.159	0.152	0.16	1.31	1.39	1.12	3.72	1.31	0.121	2.72	0.0238	BLQI	16.1	27.1
	Toluene (mg/kg)	< 0.01	< 0.01	< 0.01	BLQ1	BLQ!	BLQI	BLQI	BLQI	BLQI	BLQI	BLQ1	BLQI	0.0266	0.204	0.235	2.73	12.6	0.142	1.73	3.75	0.231	0.159	0.2	0.0936	0.035	0.0436	0.0455	0.117	0.591	0.304	1.07	0.0674	0.0188	0.182	0.0154	0.0137	0.0073	0.0122
	Benzene (mg/kg)	< 0.01	< 0.01	< 0.01	< 0.01	BLQI	BLQI	BLQI	< 0.01	BLQ1	BLQI	BLQ1	BLQ1	0.0326	1.61	0.517	4.55	0.401	BLQ1	0.49	0.749	0.866	0.787	1.45	0.771	0.665	0.538	0.678	0.629	0.633	0.333	0.501	0.422	0.315	0.712	0.0812	0.00831	< 0.01	< 0.01
Sample Interval	Bottom (ft bgs)	5.95	6.30	6.65	14.00	14.40	14.80	15.20	15.56	15.92	16.28	16.64	17.00	17.36	17.36	17.72	18.08	18.44	18.80	19.12	19.45	19.77	20.09	20.42	20.74	21.06	21.38	21.71	22.03	22.33	22.68	23.00	23.20	23.40	23.76	24.12	24.48	24.84	72.20
Sample	Top (fl bgs)	9.60	5.95	6.30	13.80	14.00	14.40	14.80	15.20	15.56	15.92	16.28	16.64	17.00	20.7	17.36	17.72	18.08	18.44	18.80	19.12	19.45	19.77	20.09	20.42	20.74	21.06	21.38	77.77	22.03	22.35	22.68	23.00	23.20	23.40	23.76	24.12	24.48	74.84
	Sample Date	8/21/93	8/21/93	8/21/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	10/21/93	56/1/6	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/77/93	8/27/93	8/22/93	8/27/93	8/22/93	8/22/93	8/22/93	8/22/93	8/22/93	8/777/8
	Sample Location	82 E-15	82 E-14	82 E-13	82 1-14	82 1-13	82 1-12	82 1-11	82 I-10	82 1-09	82 1-08	82 1-07	82 I-06	82 1-05	\$2 1-03	82 1-04	82 1-03	82 1-02	82 1-01	82 1-27	82 1-26	82 1-25	82 1-24	82 1-23	82 1-22	82 1-21	82 1-20	67 1-19	97-1-19	/1-1 79	97 1-10	82 1-15	65-178	82 1-48	82.1-37	82 1-36	82 1-35	821-34	82 1-33

TABLE 4.2 (Concluded) FUEL HYDROCARBON COMPOUNDS DETECTED IN SOIL UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

8/22/93 8/22/93 8/22/93 8/22/93 8/22/93 8/22/93 6/18/92 6/17/92	(ft bgs) 25.20 25.26 26.28 26.64 11.00 15.50	(ft bgs)	(ma/ka)	_	1										
	25.20 25.26 26.28 26.64 11.00 15.50	25 56	(mg/kg)	(mg/kg)	(mg/kg)	(mg/kg)	(mg/kg)	(mg/kg)	(mg/kg)	(me/ke)	(me/ke)	(me/ke)	(me/ke)	IMB (mo/Le)	TPH (me/ke)
	25.20 25.56 26.28 26.64 11.00 15.50	75.55										10.0		142.3	/32.2
++++	25.56 26.28 26.64 11.00 15.50	2000	0.0136	0.032	1.24	1.05	1.79	NA NA	0.0376	2.8776	4.1632	131	7.62	3.00	AIMECT
	26.28 26.64 11.00 15.50	25.92	< 0.01	0.0114	0.101	> 0.01	0.0128	Ϋ́N	BLOI	0.0128	0.1252	0.418	16100	0,250	(1001 ×
	11.00	26.64	< 0.01	0.0157	BLQI	BLQ1	BLOI	ΥN	BLÓI	0	0.0157	BI 01	RIOI	RIOI	A N
	11.00	27.00	< 0.0!	8910.0	BLQI	BLOI	0.00884	ΥN	BLOI	0.00884	0.02564	RIOI	0.00524	N O	1
+	15.50		< 0.01	0.0111	BLQ1	BLQI	BLQ1	¥	BLOI	0	11100	BLOI	RIO	20	Y X
1	15.50	11.50	< 0.005	0.031	0.12	Y.	AN	Ϋ́N	Ϋ́	0.92	0.963	YZ	Y Z	Y	9
	2	16.00	2	0.11	0.26	¥Z	¥X	ΑN	Ϋ́	2.8	5.17	ž	ž	ž	2
\dagger	20.01	17.00	0.15	0.129	0.057	ΝA	VA V	0.203	0.115	0.318	0.654	ΥN	Ϋ́N	¥	< 10.0
MW-01A 6/29/92	00/1	17.50	2	23	16	٧×	Y.	Ϋ́	Ϋ́	74	123	¥Ν	Ϋ́Z	ž	1500
1	8.08	19.00	0.564	0.145	0.341	NA	ΑN	1.64	609.0	2.249	3.299	¥Ζ	₹Z	ž	983
	71.00	21.50	0.000	< 0.005	< 0.005	Y.	Y V	Ϋ́	Ϋ́	10.0 >	600.0	٧×	¥Z.	¥Z.	< 10.0
	29.50	00:09	< 0.005	< 0.005	< 0.005	ΥN	Ϋ́N	ΥN	Ϋ́	< 0.01	0	ź	¥	¥Z	001×
4	17.00	17.50	0.1	0.1	0.18	NA.	Ϋ́	Ϋ́	Ϋ́	5.4	5.78	₹Z	¥Z	¥Ž	360
-	11.00	12.00	9.4	115	2 99	Ϋ́	ΑN	494	140	634	2214	Ϋ́Z	٧X	¥Z	1790
4	15.00	16.00	0.0432	0.0513	0.0522	NA	Ϋ́N	0.365	0.0923	0.4573	06399	Ž	¥2	\$ \\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \	21,7
-	17.00	18:00	0.013	0.0602	0.0577	NA A	Ϋ́	0.386	0.123	0.509	0.604	ž	ž	Ž	33
	19.00	20.00	0.338	0.595	0.138	٧X	٧N	0.867	0.276	1.143	825.1	¥	Ž	¥Z	V 100
SB870A-03 d 11/7/91	19.00	20.00	22.2	187	83.1	ΥN	¥X	567	177	744	1036 3	¥2	12	2	00131
 All samples with an 82 prefix are from EPA-82 series wells 	fix are from	1 EPA-82 ser	ies wells								2000		5	4	3161
See Appendix C for analytical methods	al methods														
BLQ1 = Detected Below Limit of Quantification of 0.01 µg/mL	nit of Quan	tification of	0.01 µg/mL												
NA = Sample not analyzed for this parameter	or this paran	meter)												
EST = Estimated value reported by lab	ted by lab														
NSN = No sample number															
d = Duplicate sample															





contamination at concentrations above 100 mg/kg in the soil is approximately 7 feet at EPA-82-I, which is in the vicinity of the initial fuel release into the soil. This 7-foot-thick zone of elevated TPH concentrations extends above and below the ground water table. Downgradient areas with residual-phase contamination have TPH levels as high as 580 mg/kg, but the contaminated zones are less than 1 foot thick. Theoretically, because BTEX is a subset of TPH, the areas of BTEX and TPH contamination should be the same. However, because of the higher detection limit associated with the TPH analytical method, the area of detected TPH is slightly smaller than the area with elevated BTEX concentrations at this site.

4.2.3 Total Organic Carbon

TOC concentrations are used to estimate the amount of organic matter sorbed on soil particles or trapped in the interstitial passages of a soil matrix. The TOC concentration in the saturated zone is an important parameter used to estimate the amount of contaminant that could potentially be sorbed to the aquifer matrix. Sorption results in slowing (retardation) of the contaminant plume relative to the average advective ground water velocity. Background measurements of TOC were taken from core samples obtained from soil boring EPA-82-E. The TOC in the soil at this point ranges from 0.069 to 0.094 percent (Table 4.3).

TABLE 4.3

TOTAL ORGANIC CARBON IN SOIL

UST SITE 870 INTRINSIC REMEDIATION EE/CA

HILL AFB, UTAH

Sample Location	Soil Filtrate (% OC)	Solids (% OC)	Total Soil (% OC)	Mean + 1 Standard Deviation Soil % TOC
82E-12-1 (6.65 - 7.00 feet bgs)	0.007	0.046	0.053	
82E-12-2 (6.65 - 7.00 feet bgs)	0.009	0.056	0.065	0.069+0.019
82E-12-3 (6.65 - 7.00 feet bgs)	0.007	0.083	0.09	
82E-14-1 (5.95 - 6.30 feet bgs)	0.007	0.074	0.081	
82E-14-2 (5.95 - 6.30 feet bgs)	0.006	0.062	0.068	0.070+0.011
82E-14-3 (5.95 - 6.30 feet bgs)	0.006	0.054	0.06	
82E-15-1 (5.60 - 5.95 feet bgs)	0.014	0.071	0.085	
82E-15-2 (5.60 - 5.95 feet bgs)	0.018	0.074	0.092	0.087+0.004
82E-15-3 (5.60 - 5.95 feet bgs)	0.012	0.073	0.085	<u></u>
82E-17-1 (4.90 - 5.25 feet bgs)	0.011	0.101	0.112	
82E-17-2 (4.90 - 5.25 feet bgs)	0.011	0.078	0.089	0.094+0.017
82E-17-3 (4.90 - 5.25 feet bgs)	0.012_	0.068	0.08	
LECO STANDARD DEVIATION	SOIL	1.022		
		1.034		
LECO STANDARD DEVIATION	SOIL T.V.	1.00+0.04		

feet bgs = feet below ground surface.

Soil TOC samples were collected just below the phreatic surface for accurate estimates of TOC in the shallow saturated zone. EPA-82-E was selected as a TOC sampling location because it was located outside of mobile or residual LNAPL contaminated soils (which would compromise TOC readings) and directly downgradient of potential plume migration. As a result, the soil TOC at EPA-82-E is indicative of the potential sorptive potential in the shallow aquifer directly downgradient of anticipated plume migration. The TOC estimate compares favorably with literature values defining TOC contents in relatively clean, sandy soils (0.01 percent TOC).

4.3 GROUND WATER CHEMISTRY

4.3.1 Dissolved-Phase BTEX Contamination

Laboratory analytical results for ground water samples collected during previous site investigations indicated the presence of fuel-hydrocarbon contamination in the shallow saturated zone in the vicinity of UST Site 870. Ground water samples collected in August 1993 by Parsons ES and RSKERL personnel confirmed these results. Additional ground water samples collected in July 1994 suggest that natural attenuation of BTEX compounds is occurring at this site. Table 4.4 summarizes available ground water contaminant data. Two ground water samples from the site appear to have unrealistically high total BTEX concentrations ranging from 52.7 mg/L (TP-07 = CPT-07) to 14,400 mg/L (CPT-14). The work of Smith et al. (1981) suggests that the maximum dissolved-phase BTEX concentration that can result from the equilibrium partitioning of BTEX compounds from JP-4 into ground water is approximately 30 mg/L. Unrealistically high total BTEX concentrations generally result from LNAPL emulsification during sampling. The highest dissolved-phase total BTEX concentration observed at the site that can be considered reliable is 26.576 ug/L. This sample was collected from well MW-03 in August, 1992. This well contained mobile LNAPL but this total BTEX concentration is within the range suggested by Smith et al. (1981) and is consistent with samples collected from other wells containing mobile LNAPL (EPA-82-I = 21,475 μ g/L and EPA-82-J = 16,336 μ g/L).

To evaluate trends in BTEX loss over the site, data sets from different sampling periods were combined to form BTEX isopleth maps for 1993 and 1994 (described in proceeding paragraphs). Although generally not a concern, the various ground water analytical methods used to sample ground water from different site characterization studies (1992 to 1994) were judged for their

TABLE 4.4 FUEL HYDROCARBON COMPOUNDS DETECTED IN GROUND WATER UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				6	-	100		3	7 4 9 7		Total	Total	1,3,5-	1,2,4-	1,2,3-
Sample	Sampie		Marking	Denzene	loluene	Emyloenzene		M-Ayiche	M-Ayiene M&P-Aylene	C-Aylene	Aylenes	BIEX	gw (I WB	1 MB
Location	Dalc	Casting	Norming	(TARH)	(T/AH)	(HB/L)	(HR)(F)	(TAME)	(1/8/H)	(TABAT)	(T/Birl)	(T/MIT)	(TABAT)	(7,841	(Tight)
					MO	MONITORING WELL SAMPLING LOCATIONS	TELL SAMPI	LING LOCA	TIONS						
EPA-82-A	8/19/93	1546.62	2945.1	Ī>	l>	⊽	l>	⊽	¥Z	⊽	⊽	I>	⊽	⊽	v
EPA-82-A	11/8/93	1546.62	2945.1	1>	BLQI	1>	1>	 	¥Ν			BLQ1	1.14	0.965	BLQ1
EPA-82-A	1/94	1546.62	2945.1	-1>	>	 	l>	>	ΥN	⊽	⊽	>	>		<u> </u>
EPA-82-B	8/07/8	2062.23	3063.44	l>	4.29	1>	l>	l>	¥z	⊽	√	4.29	80.	1.43	⊽
EPA-82-B	11/8/93	2062.23	3063.44	!>	l>		I>	⊽	Ϋ́Z	⊽	⊽	ĪŸ	⊽	⊽	⊽
EPA-82-B d	11/8/93	2062.23	3063.44	l	l>		l>	I>	Ϋ́Z	⊽	⊽	Ī	⊽	 	⊽
EPA-82-B d	7/94	2062.23	3063.44	V	i>		⊽	Ī	Ϋ́N	⊽	⊽	⊽	⊽	⊽	⊽
EPA-82-C	8/20/93	1840.49	3035.78	4.92	3.13	26.5	42.8	47.2	ΑN	2.62	92.62	127.17	238	324	120
EPA-82-C	11/9/93	1840.49	3035.78	⊽	6.38	6.81	20.2	6.38	Ϋ́N	1.82	28.4	41.59	79.7	689	- 49
EPA-82-C	7/94	1840.49	3035.78	7.28	9.74	22.7	25.9	18.3	Ϋ́N	3.18	47.38	87.1	144	143	429
EPA-82-D	8/21/93	2167.57	3507.69	95.8	10.4	147	149	383	Ϋ́N	103	635	888.2	129	183	888
EPA-82-D	11/9/93	2167.57	3507.69	174	4.64	30.8	141	293	Ϋ́	57.5	491.5	700.94	89.4	119	77.1
EPA-82-D	7/94	2167.57	3507.69	458	17.6	454	272	442	ž	50.7	764.7	1686.41	125	176	409
EPA-82-E	8/22/93	1345.36	2845.36	l>	1>		l	⊽	¥Z	⊽	V	IV	Ī	⊽	⊽
EPA-82-E	11/8/93	1345.36	2845.36	⊽	⊽	⊽	⊽	⊽	Ϋ́	⊽	12	Ī	Ī	⊽	⊽
EPA-82-E	7/94	1345.36	2845.36	⊽	1>	⊽	⊽	⊽	Y.	Ī	⊽	I>	I>	⊽	⊽
EPA-82-F	8/21/93	1543.19	2943.57	l>	>	<u>-</u>	·	⊽	Ϋ́	⊽	⊽	⊽	₽	⊽	₹
EPA-82-F	11/9/93	1543.19	2943.57	1>	l>	 >	I>	ľ	Ϋ́	⊽		I>	⊽	⊽	<u>~</u>
EPA-82-F	7/94	1543.19	2943.57	QN	QN	l>	1>	[>	ΥN	QN	 -	l>	ΩN	V	Q
EPA-82-F d	7/94	1543.19	2943.57	ND	ΩN	QN	>	 >	NA.	QN		1>	ΩN	 	ND
EPA-82-H	8/21/93	1964.51	2719.71	-1>	l>	 	l>	1>	NA VA	l>	l>	l>	l>	١٧	
EPA-82-H	11/8/93	1964.51	2719.71	✓	<1	!>		1>	NA	 >	l>	l>	0.942	BLQI	BLQI
EPA-82-H	7/94	1964.51	2719.71	>	1>	l>	1>	l>	AN	QN	1>	J>	QN	⊽	Q
EPA-82-I (a)	11/93	2520.42	3771.26	2740	372	486	784	1370	ΝA	1140	3294	6892	162	495	240
EPA-82-1	7/94	2520.42	3771.26	2600	5870	955	1620	2130	NA	2300	9050	21475	417	1270	436
EPA-82-J	7/94	Ϋ́	Ϋ́Z	4260	3910	816	1370	4220	ΥV	1760	7350	16336	485	1310	515
MW-01	11/18/91	2475.32	3841.98	305	069	132	Ϋ́	¥Z	Ϋ́Z	٧V	2283	3410	Ϋ́Α	NA	٧V
MW-0I	12/93-1/94	2475.32	3841.98	475	88	183	٧	٧X	Ϋ́Z	٧×	1160	1906	330	089	٧V
MW-02	12/93-1/94	2389.21	3846.24	51	56.3	73.3	¥	Ϋ́Z	Ϋ́Z	٧×	776	926.6	350	750	٧V
MW-03	08/6/92	2533.09	3882.19	12179	6728	<\$	Ϋ́	Ϋ́Z	4300	3369	7669	26576	٧V	٧V	٧V
MW-03	10/92	2533.09	3882.19	12.18	6.73		¥	٧Z	Ϋ́	ΝA	7.67	26.58	٧×	NA	NA NA
MW-03	12/93-1/94	2533.09	3882.19	2320	1300	376	Ϋ́Z	٧Z	Ϋ́	ΝA	5470	9466	480	1000	٧V
MW-04	12/93-1/94	2446.7	3798.05	930	1830	450	Ϋ́	NA	NA	NA	5120	8330	550	1500	٧V
MW-05	09/30/92	2536.47	3813.49	74	<\$0	160	VΑ	Ϋ́	NA	NA	006	1134	٧X	٧	¥
MW-05 d	09/30/92	2536.47	3813.49	76	<50	150	NA	ΑN	٧N	NA	068	9111	٧N	٧V	¥Z
MW-05	12/93-1/94	2536.47	3813.49	416	250	246	ΥN	NA	ΝA	NA	2508	3420	450	960	٧V
MW-06	9/92	2389.06	3794.35	<25	<25	<25	Ϋ́	NA	ΝA	NA	<25	<25	Y.	NA	٧X
MW-06	09/04/92	2389.06	3794.35	<25	<25	<25	¥	VA V	٧X	NA	<25	<25	ΝA	NA	٧×
MW-06	12/93-1/94	2389 06	3794.35	24.5	101	18.6	¥	¥	¥Z	¥	155.9	2091	650	1500	¥Z

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TABLE 4.4 (Continued) FUEL HYDROCARBON COMPOUNDS DETECTED IN GROUND WATER UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

	J			П				Γ	Γ		Γ		Γ	Γ			Γ	П	Γ	Γ	П			Γ	Г	Γ	Π				Γ	Γ	Г	Γ	Γ	Γ		
1,2,3. TMB	7.0	٧	٧X	NA	ΥN	٧N	٧N	۲×	ž	٧X	209	683	212	161	Ν	€69	ž	287	⊽	٧×	٧N	13.3	NA	٧V		▽	>	l>	1.08	>	330	ž	▽	⊽	⊽	۱۷	▽	⊽
1,2,4- TMB	(17.74)	¥	٧X	NA	>	280	989	٧×	٧Z	ΑA	828	974	297	303	NA	165	¥	25.7	⊽	٧X	ΝA	36.2	1113	1400		▽	ļ>	1>	1.1	1>	735	ΥN	l>	>	⊽	>	>	ŀ
1,3,5- TMB	77.22	Ϋ́	NA	NA	>	140	150	NA	٧X	ΑN	575	713	174	215	NA	71.8	¥Z.	30	 	NA.	NA	686	470	929		>	<	<1	<1	<1	295	ΑN	I>	Ī	V	<1	>	
Total BTEX	77.44	\$	\$>	<\$	 >	373.1	692	2.06	127	127	4884	5724	2044.34	1734.7	260	1634.3	260	563.8	l>	329	339	35.47	9129	9756		2.2	 	-l>	1.27	<ا	5095.4	٧٧	1>	Ī	١٧	>	<	⊽
Total Xylenes	77.44	\$	<\$	<\$	>	314.4	558	0.27	110	110	4151	4841	1784	1478	180	6901	081	372.4	>	300	300	34.57	4280	5510		2.2	>	<1	BLQ1	دا	4583	٧V	ŀ	I>	l>	>	1>	▽
O-Xylene	77.74	ΝA	٧Z	NA	NA.	NA	NA	٧X	٧X	NA	1280	1490	505	44]	ΝA	204	۲	86.4	>	NA	NA	17.3	NA	NA		2.2	>	<1	< <u> </u>	<1	984	٧V	l>	۱۷	>	<	<1	 >
M&P-Xylene	77.64	Ϋ́Z	Ϋ́	NA	ΑN	NA	AN	ΥA	Ϋ́	AN	ΥN	NA	¥	Ϋ́	NA	NA	¥	NA	٧N	NA	NA	NA	NA			NA	NA	NA	NA	NA	NA	NA	NA	ΝA	NA	NA	NA	¥
မွ	1 (7,64)	¥	٧X	NA	٧V	NA	ΑN	¥	ΑN	ΝA	2470	2880	0601	847	٧V	635	¥	221	ŀ	٧V	ΥN	9.45	NA	٧V	SAMPLING LOCATIONS	>	1>	>	BLQ1	l>	2730	ΝA	>	l>	>	>	>	V
P-Xylene	17.84	ΨN	ΥN	NA	NA	NA	AN	۸N	ΥN	NA	401	471	681	<u>8</u> 2	NA	230	¥Z	l I		NA	. 1		1	ΝA	SAMPLING	<ا	>	>	<1		698	٧V	l>	l>		<	>	>
Ethylbenzene	1 (7,841	\$	<\$	<\$	i>	29.3	35	90:0	<0.5	<\$	443	543	061	182	21	139	21	39.9	۱>	29	59	6.0	589	505	GEOPROBE	<1	>	<1	<	<1	461	NA	۱>	1>	<ا	1>		
ų,	77.44	\$	\$	<\$	>	8.01	27	0.57	17	1.1	290	340	62.9	54.7	33	90.3	33	М	П	П				П		BLQI			1.27	-</td <td>BLQI</td> <td>ΥN</td> <td>BLQI</td> <td>l></td> <td> ></td> <td> </td> <td> ></td> <td>⊽</td>	BLQI	ΥN	BLQI	l>	>		>	⊽
Benzene	7.74	\$	\$>	<\$		9.81	72	1.16	\$>	\$>	<10	2	7.44	20	76	336	26	105	QN	<>	10	[>	2690	941		l>	<1	<1	>	<1	51.4	VΑ	<1		<1		<1	
Modbins	giiini	3900.79	3900.79	3900.79	3900.79	3893.96	3930.05	3397.6	3397.6	3397.6	3397.6	3397.6	3397.6		3213.91	3213.91	3213.91	3213.91		3650.34	3650.34		SDNA	SDNA		3772.45	3493.12	3493.12	3457.77	3457.77	3215.91	3215.91	2835.21	2863 23	2863.23	3205.92	3205.92	3205.92
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TABLE 4.4 (Continued) FUEL HYDROCARBON COMPOUNDS DETECTED IN GROUND WATER UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

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 | ┡╶┡ ═╫ ╬╏┈┟╌╃┈┞┈╂┈╂┈╂┈╂┈╂┈╂┈╂┈╂┈╃┈╂┈╃┈╂ ╌╇┈╂╌╇┈╂╌ | ┡╶┡╼╠╠┡╒╃╒╇╒╇╒╇╒╇╒╇╒╇╒╇ ╌╇ ╒╇╒╇ ╌╇ | ┺╌┡═╠╠┈┟╼┇╶╏┈┞┈╄┈╂┈╂┈╂┈╂┈╂┈╂┈╂┈╂┈╂┈╂┈╂┈ ╂┈ |
╇╒╇╒┋┡╒╇╒╇╒╇╒╇╒╇╒╇╒╇╒╇╒╇╒╇╒╇╒╇╒╇╒╇ ╌╬ ╌╇╸ | ╬┈┡═╬╠╎╏╒╃╶╄═╇┈╇╌╂╌╂╌╂╌╂╌╂╌╂╌╂╌╂╌╃╌╂╍╇ ╌╬ ═╄ ═╉╌ | ╏╶┧═╚ ╏ ╴╏╌╏╶╏╸╏╶╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏ ┈╂ ┈╏┈╏┈╏╸╏╸╏ | ┩╶┩┈╠╠╒┋╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒ |
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(ug/L) (| 1 |
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 | HHH | ├ ┼┤├┼┼ | ┡╺╏ ┙╸┠ ╸╏╸╏╸ | | ┡╺╏ ┩╸┠ ╸╏╸╏╸╏╸╏ | ╽╸┧ ╸┧╸ ╏╸╏╸╏╸╏╸╏╸╏

 | ╘┋ | ╘╏ ┩ | ╘╏ ┩╏╃╫╫ | ╘╏ ┩╏ ╏╏╏╏╏
 | ╘╏ ┩╏ ╏╏╏╏╏ | ┧ ╌┩╸ ╏╸╏╸╏╸╏╸╏╸╏╸╏╸╏╸╏╸╏╸ | ╘╏┩╒╃╬╬╬╬╬╬╬╇╇╇╇ | ╘╏┩╒┋┋┋┋┋┋┋┋┋ | ╘╏┩╒╃╄╄╄╄╄╇╇╇╇ | ╘╏╸ ┩╒ ╏╏╏╏╏

 | ╘╏ ┩╏ ┪╏╏╏╏╏╏ | ┡╅ ┩ ╒╬╄┋╋╂╇╂╇╂╇╇╇╇╇╇╇

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╏╏╏╏╏╏╏╏╏╏╏ | ┡╒ ┩╒ ╬╒┋┋┋╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒╒ | ┡╃┩┡╃╄╂╄╂╂┼┼┼╇╇╇╇╇╇╇╇╇╇╇╇ | ┡╃┩┡╅╄╇╇╂╇╃╇╇╇╇╇╇╇╇╇╇╇╇╇╇ |
| | Northing | 1 | 4145.21 | 4145.21 | 4145.21 | 2656 22 | 2834.32 | 2834.32 | 2834 32 | 2698.09 | 2698.09 | 2738 09 | | 2688.82 | 2688 82
2865 35 | 688.82 | 2688.82
2865.35
3772.45 | 2688.82
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3772.45 | ┺┋ ┩╟╇╇╋ | ┡┋ ┩ | ┺╂┩┠╄╂╋ ┺ | ╏╏ ┩╏ ╏╏╏ ╬┼┼┼

 | ╏┋ ┩ | ┇┋ ┩ | ┺ ╃┩┠ ╇╏╇ ╅╇╇┩ | ┺┺┩┡╋┸╋ ╈╋╃
 | ┺ ╅┩┠ ╇╏╋ ╅╋╋╋ | ┺╃┩┡╇╀╇╩╇╇╇╇╇╇╇╇╇ | ┺╄┩┡╇╀╬╬╅╋╇╇╇╄╇╇╇ | ┺╄┩┡╇┺╬┷╅╇╇╇╇╇╇╇╇ | ┺ ╇┩┠ ╇╏╬╏╅╄╇╄┩╘╅╄╬ ╄┥ | ┺ ╇┩┠ ╇╏╬╏╅╊╃╄┩╂╅╄╇╄

 | ┇╃┩╏╃╀╇╙╃╂╄╄╄╃╄╄╄╇╄╄╄ | ┇╃┩╏╃╀╇╙╃╂╄╃╇╃╄╇╄╇╄╇╄╇

 | ┇╃┩╏╃╏╇╏╃┢╂╇╃╘╃╄╇╄╄╄╇╇ | ┇╇ ┩┠ ╇╏╇╙╄╅╘╂╇┩╘╂╇╇╏╂┞╇╇╄ | ┖╃┩┡╃╄╬┡╬╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇ | ┇╅ ┦┠
╃╏╇╙╅╘╂╄┩╠╃╄╂╄╄╇╇╇╄╄╄ | ┇╅ ┦┟ ╀╏ ╩ ╏┪╏╂╂┞╏╏┩╏╏╏ | ┇╃┩╏╃╏╬╏╬╏╂┞╃╃╏╇╇╇╂╂╂╂┞┡┡┡ ┼┼ | ┇╃┩╏╃╏╇╚╅╂╄╃╇╃╄╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇ |
| _ | Easting | 1 | 275865 4 | ╀ | ╁ | ╀ | + | ╀ | ₽ | 1700.5 | ╀ | 1425.23 | 1 | ₽ | ╁╁┤ | ┸┾┩┟ | ╄┩╟ | ┞╞ ┩┠ ╏ ╅ | ┡╺┋ | ╊╌╂╌┦╴┠╌╂╌╂╼╂ | ╏ ╌╁╌┦╴┠╌╂╌╂╌╂═╅╌╁ | ╏╶╏╸ ┦╴┠ ╶╏╸╏ ╶╂ ═ ╅╌╁═╅

 | ╻╶┢┈ ┦╴┠ ┈┠┈╏┈╏┈╏┈╏┈╏ ┈ | ╏╶╏╸ ┦╴┠ ╶╏╌╏╴╏═╏╶╏═ ╬╌╋═┩ | ┩ ╌┾╾┦╴┠ ╶╂┈┞ ╶╂ ═╏ ╌╂═╋╌╂═╋╌╂═╋┉┤ | ┩ ╌╂═┦╴┠ ┈╂┈╂┈╂═╅╌╂═╂╌╂═┦┈╂═ ┤
 | ┩╶┢╌ ┦╴ ┠┈╂┈╂┈╂┈╂┈╂┈╂┈╂┈╂ ┈╂ | ┩╶┢╌ ┦╴ ╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏┈╏╸╏┈╏╸ | ┩╶┢╌ ┦╴┠ ╶╂╌╂┈╂═╅┈╂═╂╌╃═╂ ╌╃ | ╻╻ ╸╻ ╻╻╻ | ╻ ╁┩╏ ╏╏╏╏╏ | ╻ ┾┩╏ ╏╏╏╏

 | ┡╺ ┩╒ ╒╒┩╒╃╒╇╒╇╒ ╇╇ | ╻ ┾┩╏ ╏╏╏╏╏╏

 | ╏ ┾┩╏ ╏╏╏╏╏╏╏ | ╏ ┾┩╏ ╏╏╏╏╏╏╏ | ╏ ┾┩╏ ╏╏╏╏╏╏╏╏ | ┡ ┾┩
╒┋╏┪╏┪╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇ | ╏ ┾┦╏ ┆╏╏┪╏╅╬╬╬╬╇╇╇╇╇╇╇ | ┡╒ ┩ ╒┋┋┋┋┋┋┋┋┋┋┋ | ╏ ┾┦ ╏╏╏╏╏╏╏╏╏ |
| _ | Sample Date | - | 8/5/03 | \dagger | ╁ | + | † | t | t | 7/94 | ╁ | Н | | 1/94 | H | ┝┼┤┟ | ┝┼┤┟╉ | ┝╃╢╶┞╼╇╍╂ | ┝╀╌┤╎╌╃╌╁╌╅ | ┝╃┦╶┞╃╃┸╋╇ | ┝╾╀╌┨╴┠╼╃╌╂┈┾╼╂╍┥ | ┝╾╀╌┦╴┠╼╂╍╂┈╊╼╂╍╋═╂

 | ┝╾╀╌┨╴┠╼╀╾╂┈┾╼╂╼┼═┦═ | ┝╌╀╌┨╴┠╼╂╌╂┈╂╼╂╼╃═╀═┽═┤ | ┝╾╀╌┦┈┠╼╀╾╂┈╂╾╃╼┼═┼═┼═┼ | ┝╾╀╌┨╴┠╼╂╾╂┈╂╾╂╼╂╾╀╼┼╾╂╾┦
 | ┝╾╀╌┦╴┠ ╌╃╌╏┈┝╌╬╌┢╌┞┈┼┈┞╸╃╌╋ ╍┪ | ┝ ╸┩ ╌┦╴ ╏┈┩╌╏┈╂╸┩┈┩╸┦┈┼╸┦╸┞╸┩╸ ╋ ╸ ┩ | ┝╾╀╌┨╴┠ ╌╂╌╏┈┠╌╬╌╬═┞┈╏ ╌╂╾ ┦═╏ ╌╂ ═ | ┝ ╸┩ ╌┨╴┠ ╌┩╌╏┈╊╌╬┈╅╌┞┈┼┈╂═╄═╄═╋┈╂═╇ ╾┥ | ╒╶┩ ╌┨ ╞╒╇╌╏┈┡═╬╌╬═╄═╇═╄═╇═╇═╋═╋ ═╋ ╒ ╋═╇ | ╒╃╶┨╎╒╃╍╏┈┾╌╬╌╃═┞┈┽═┾═╄═╋┈╂═╋╌╂═╋ ╌╋═

 | ╒╃╶ ┨ ╏╒╃╍╂┈┾╼╂╍╅═┞╌╂═╂═╇═╋═╋═╋═╋ ═╋═╋ | ┝ ╺┩╌ ┨┊ ╒┋╍╏┈┾╌╬╍╅═┞═╫┈╂═╇═┞═╋┈╂═╇╌╂┈╋ ═╋ ╸

 | ┝ ╺┩╌ ┨┈ ╞╼╂┈╄╼╂┈╅═╀═╃═╂═╇═╋═╋═╋═╋═╋═╋═╋ ═╋═╋═╋ | ┝╺┩╌┨ ┈ ┠╸┩╌╂╌╂╌╃═┦╌┦┈╂═╃╌┞═╋╶╂═╋╌╂═╋╌╂═╋ ╌╋ ═ ╋ | ╒╃┩╟╇╬╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇ |
╒╃┩┝╇╃╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇ | ╒╃ ┨ ╒╃┩╄╇╇╃╃╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇ | ╒╃ ┨┞ ╃╃╄╇╇╃╃╇╂╇╂╇╂╄╃╄╇╇╇╇╇ | ╒╃┩╟╃╃╇╇╇╃╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇╇ |
| | Sample | io incompact | 71.30 CPT (Jenth 1) | 71-30 CPT (denth 2) | 71-39 CPT (denth 2)d | FPA.82.K | FPA-82-1 1 | FPA-82-12 | EPA-82-L3 | EPA-82-M | EPA-82-M d | EPA-82-N | | EPA-82-0 | EPA-82-O
EPA-82-P | | | | | | |

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TABLE 4.4 (Concluded) FUEL HYDROCARBON COMPOUNDS DETECTED IN GROUND WATER UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

-lamo?	Comple			Benzene	Toluene	Eshvibenzene	D Vylene	M. Yulana	M&P.Xvlene	O. X.ylana	Total	Total	1,3,5- TMR	1,2,4-	1,2,3-
Location	Date	Easting	Northing	(µg/L)	(µg/L)	(µg/L)		(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(#g/L)
			S 1		1	CTODIA CENTER CAMBINIC LOCATIONS	i larte a	T-100 101	3140						
CTODA 3	20/8	1430 1	2443 08	V	1	SI ONNI SEW	CR SAIMITLE	TV TV	ZNO.	Ī	V	V	V	V	Į
STORM-3	8/93	1445 12	2511.52	V	. ▽	Į	V	V	¥	V	\ <u>\</u>	. □	. ▽	. ▽	· -
					Σ	MISCELLANEOUS SAMPLING LOCATIONS	JUS SAMPI	ING LOCA	TIONS						
870-WS-1/32"	11/23/92	SDNA	SDNA	17.4	1.8	BLQ1	NA NA	Ϋ́N	4.9	13	6.2	25.4	YN.	٧X	٧×
870-WS-1/42	11/23/92	SDNA	SDNA	30.5	113	56.4	Ϋ́Z	¥z	369	103	472	611.9	٧×	ž	ž
870-WS-1/52'	11/24/92	SDNA	SDNA	27	59.3	21.6	٧N	٧×	101	36.4	143.4	251.3	٧×	¥	ž
870-WS-2/49 d	11/24/92	SDNA	SDNA	6.5	7.8	1.7	Ϋ́N	¥Z	12.2	3.4	15.6	31.6	¥Z	٧X	¥
870-WS-2/49	11/24/92	SDNA	SDNA	8.4	13.8	4.5	ΥN	¥	30.2	9.4	39.6	663	٧	¥Z.	ž
870-WS-2/59	11/24/92	SDNA	SDNA	24	89	50.7	٧X	٧X	294	93.7	387.7	530.4	₹z	¥	ž
870-WS-2/69	11/24/92	SDNA	SDNA	43.5	7.17	38.2	¥z	¥χ	258	63.6	321.6	475	٧×	٧X	¥
GWS-01	08/14/92	SDNA	SDNA	195	946	72	٧X	Ϋ́Z	62	27	68	1302	٧X	¥	ž
SGS-01	08/05/92	SDNA	SDNA	191	12645	46	Ϋ́Α	¥	\$	295	295	13147	ΑN	¥	ž
SGS-1	08/01/92	SDNA	SDNA	1.7	\$	5.5	ΨN	٧X	8.8	61	27.8	4	¥	٧N	٧
See Appendix C for analytical methods	analytical met	hods													
(a)=Headspace data															
d = Sample dunlicate															

d = Sample duplicate
BLQ1=Detected below Limit of Quantification of 1 µg/L
BLQ2=Detected below Limit of Quantification of 4 µg/L
BLQ3=Detected below Limit of Quantification of 2 µg/L
BLQ3=Detected below Limit of Quantification of 10 µg/L

NA = Sample not analyzed for this parameter EST = Estimated value reported by lab SDNA=Surveyor's data not available

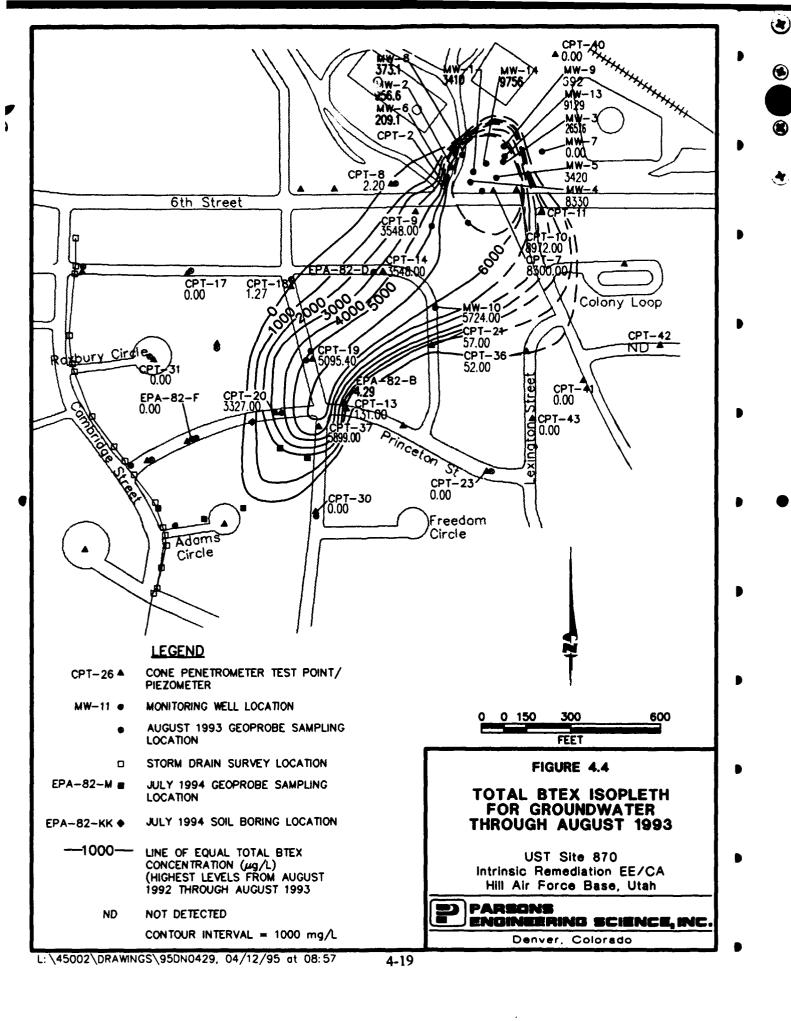
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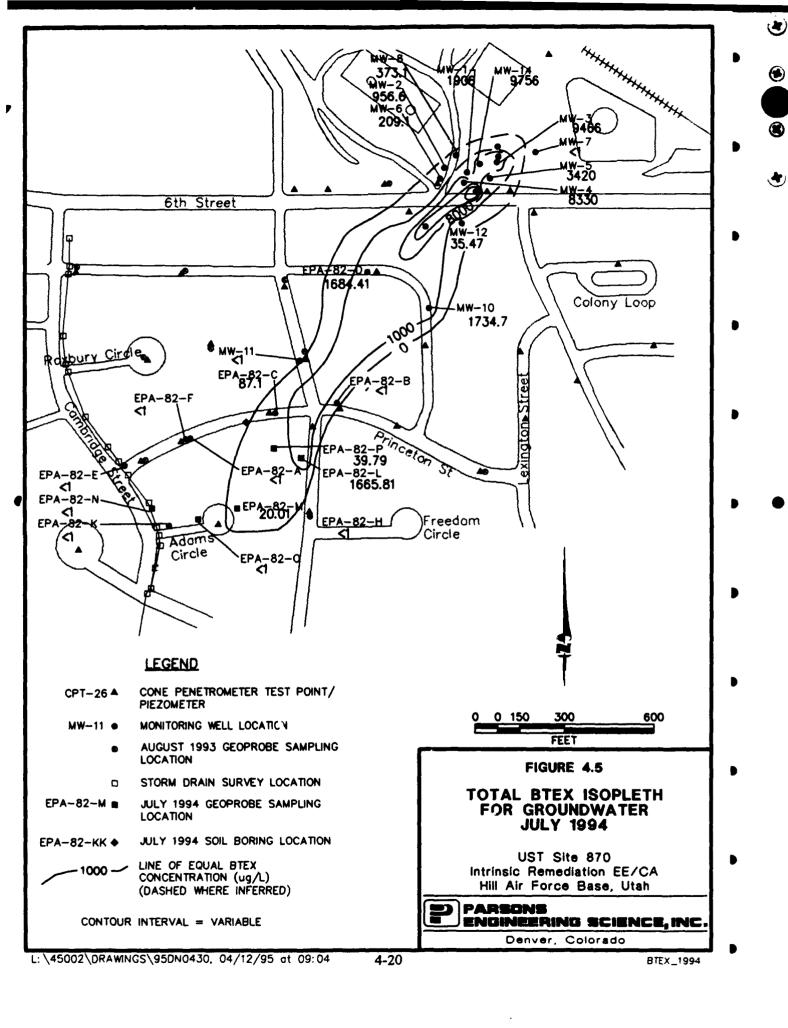
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quantitative comparability. Method RSKOP-124 was used by Parsons ES to quantitate aqueous BTEX concentrations during August 1993 and 1994 sampling events. RSKOP-124 is a dual-column, gas-chromatograph/mass spectroscopy (GC/MS) technique that has resolution capabilities that are superior to EPA SW-846 Methods 8020/602, 8015M, and 8240 (used for volatile and semi-volatile organic analysis by JMM in 1992). All analytical techniques used for VOC analysis in the different site characterization studies from 1992 to 1994 had identical, achievable detection limits of 1 µg/L and adequate compound resolution capabilities. Hence, comparison of different ground water data sets are not compromised by underestimation or overestimation of a particular analytical technique. Groundwater extraction and preparation techniques used by JMM in 1992 are not available; however, potential differences in sampling technique were predicted to be minor because ground water sampling techniques are fairly standardized.

Figure 4.4 is an isopleth map that shows the distribution of total BTEX dissolved in ground water through August 1993. Because this figure was used for Bioplume II model input (to be conservative) the highest total BTEX concentrations observed in ground water between August 1992 and August 1993 were used to prepare this figure. This figure also includes data collected from monitoring wells in the source area north of Sixth Street in December 1993/January 1994 (MW-01, MW-02, and MW-04 through MW-09). These wells cover a very small area relative to the areal extent of the plume and in some cases these data represent the only data available for this area. As a result, Figure 4.4 represents the most conservative representation of the 1993 BTEX plume based on available data. BTEX contamination is migrating to the southwest in the direction of ground water flow. During the period through August 1993, the BTEX plume was approximately 1,650 feet long and 750 feet wide at the widest point.

Figure 4.5 is an isopleth map that shows the distribution of total BTEX dissolved in ground water in July 1994. Like Figure 4.4, this figure also includes data collected from monitoring wells in the source area in December 1993/January 1994 (MW-01 through MW-09) to illustrate the BTEX plume for 1994. Comparison of Figures 4.4 and 4.5 suggests that a reduction in the areal extent of the BTEX plume occurred between September 1992/August 1993 and July 1994. With the exception of total BTEX concentrations in some of the monitoring wells located in the area containing mobile LNAPL (wells MW-05, MW-06, EPA-82-D), dissolved-phase total BTEX concentrations were seen to decline over this period. The increased concentrations in these wells could be the result of a fresh spill in the source area. Figure 4.4 shows that through





August 1993, the majority of the dissolved-phase BTEX plume had concentrations in excess of 5,000 micrograms per liter (μ g/L), whereas Figure 4.5 shows that in July 1994, the majority of the dissolved-phase BTEX plume had concentrations below 2,000 μ g/L. Because Figure 4.4 was prepared with the highest BTEX concentrations observed between August 1992 and August 1993, comparison of these two figures may suggest rates of intrinsic remediation that are somewhat high. Available geochemical data suggest that this reduction in the areal extent and concentration of the total BTEX plume was primarily the result of biodegradation, as discussed in the following sections.

(4)

4.3.2 Inorganic Chemistry and Geochemical Indicators of Biodegradation

Microorganisms obtain energy for cell production and maintenance by catalyzing the transfer of electrons from electron donors to electron acceptors. This results in the oxidation of the electron donor and the reduction of the electron acceptor. Electron donors at UST Site 870 are natural organic carbon and fuel hydrocarbon compounds. Fuel hydrocarbons are completely degraded or detoxified if they are utilized as the primary electron donor for microbial metabolism (Bouwer, 1992). Electron acceptors are elements or compounds that occur in relatively oxidized states and include oxygen, nitrate, ferrous iron, sulfate, and carbon dioxide. Microorganisms preferentially utilize electron acceptors while metabolizing fuel hydrocarbon (Bouwer, 1992). Dissolved oxygen is utilized first as the prime electron acceptor. After the DO is consumed, anaerobic microorganisms use electron acceptors in the following order of preference: nitrate, ferrous iron, sulfate, and finally carbon dioxide. Anaerobic destruction of the BTEX compounds is associated with the accumulation of fatty acids, production of methane, solubilization of iron, and reduction of nitrate and sulfate (Cozzarelli et al., 1990; Wilson et al., 1990).

4.3.2.1 Dissolved Oxygen

DO concentrations were measured at Geoprobe locations and monitoring points/wells in August 1993, November 1993, December 1993/January 1994, and July 1994. Table 4.5 summarizes DO concentrations. Figure 4.6 is an isopleth map showing the distribution of DO in ground water in August 1993. This figure includes data collected from monitoring wells in the source area north of Sixth Street in December 1993/January 1994. These wells cover a small area and these data represent the only data available for this area. Figure 4.7 is an isopleth map showing the distribution of DO in ground water in July 1994. This figure also includes data collected from monitoring wells in the source area in December 1993/January 1994. Comparison

		11/20	2	100										1001		
Sample	Sample	Temp	Oxygen	Potential	Alkalinity	Conductivity		Chloride	Sulfate	Iron	Ammonia	Nitrate	Nitrite	Nitrogen	Methane	
Location	Date	(c)	(mg/L)	(mV)	(mg/L)	(mS/cm)		(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
						MONITORI	Н	SAMPLINGI	CCATIONS							
EPA-82-A	\$6/61/8	16.5	0.4	170	576	1677	7.2	170	66.4	<0.05	<0.05	٧X	٧X	0.14	100.0	4.2
EPA-82-A	11/8/93	14.8	0.3	NA	NA	VA	7.4	159	60.5	0.17	ΥN	Ϋ́	Ϋ́	80.0	0.001	2.2
EPA-82-A	46/L/L	16.3	<0.5	240	530	1622	7.2	156.0	58.4	<0.05	ž	٧X	¥z	<0.05	0.001	2.8
EPA-82-B	8/20/93	16.9	1	213	450	1421	6.9	163	6.92	<0.05	<0.05	٧×	٧N	0.25	0.001	2.1
EPA-82-B	€6/8/11	12.9	1.2	NA	NA	NA	7.5	144	72.2	0.11	٧Z	٧X	¥X	0.37	<0.001	3.1
EPA-82-B		19.1	<0.5	125	428	1406	7.2	145.0	74.2	0.1	٧×	٧×	٧×	0.15	100.0	2.2
EPA-82-C	(15.5	0.5	-125	745	1828	6.9	164	49.9	2.1	<0.05	ΥN	¥Z	0.13	0.002	9.6
EPA-82-C duplicate		Ϋ́	ΑA	ΥA	٧×	¥X	٧×	191	Υ×	٧×	٧×	٧×	ž	¥	٧X	5.6
EPA-82-C	i	14.2	0.4	ΝA	Ϋ́	Ϋ́Z	6.3	<u>601</u>	17.2	0.84	٧×	ž	٧×	80.0	0.002	ç
EPA-82-D	8/21/93	15.9	[13	40	656	2520	7.3	198	193 (EST)	9.0	0.07	¥Ζ	¥	0.53	100°0>	8.1
EPA-82-D duplicate	8/21/93	NA	NA	NA	٧	٧×	Ϋ́	Ϋ́	٧×	¥z	0.08	¥	¥	0.53	٧×	∀ 2
EPA-82-D	86/6/11	14.1	8.0	ΥV	Ϋ́	٧×	7.2	151	116	<u></u>	٧×	Ϋ́Z	¥	0.13	[00:0>	\$.2
EPA-82-D duplicate	11/9/93	NA	ΝA	ΝA	Ϋ́	٧X	∀ Z	Ϋ́Z	ΥN	ΥN	٧X	٧X	¥	ž	٧×	53
EPA-82-D	()	17	<0.5	-138	657	1905	7.3	221.0	<0.5	7.4	¥Ν	٧×	ž	<0.05	0.002	10.3
EPA-82-E	8/22/93	22.8	9.6	192	349	1042	7.3	77.1	39.6	<0.05	<0.05	٧X	¥	4.4	100∵>	6.1
EPA-82-E duplicate		¥Z	٧X	٧X	¥	٧×	Ϋ́Z	78.3	39.8	¥Ν	¥χ	٧×	ž	ž	¥	Ϋ́χ
EPA-82-E	•	16.5	2.7	Ϋ́	ΥN	¥Z	7.4	76.4	8.59	0.02	٧X	٧×	¥	19'5	100.0>	6.1
EPA-82-E	ı	22.6	3.7	901	357	2020	1,	354.0	37.0	<0.05	٧×	٧×	¥X	4.39	100.0	1.7
EPA-82-F	8/21/93	22.6	1:1	243	850	1275	7.5	68.5	63.9	<0.05	<0.0>	Ϋ́Z	¥	7.41	610.0	2.2
EPA-82-F duplicate	8/21/93	NA	NA	ΝA	NA.	٧V	٧N	71.8	6.79	ž	<0.05	¥z	ž	7.46	۲ ۲	¥z
EPA-82-F	11/9/93	16.8	1.1	٧V	NA	NA	7.6	60.2	\$5.5	0.04	YZ.	¥Z	¥z	\$.07	900.0	61
EPA-82-F duplicate	11/93	NA	VΑ	ΝA	ΝA	ΝA	ΝA	60.7	55	ΝA	ΥN	¥Ζ	٧V	90.5	٧N	Y Z
EPA-82-F	7/7/94	21.5	<0.5	-70	490	1172	7.3	46.9	52.3	0.5	ΝA	AN	٧V	1.67	0.577	4.4
EPA-82-H	8/22/93	81	6.3	190	485	1400	7.1	136	59.7	<0.05	<0.05	٧X	٧V	2.12	100.0>	2.2
EPA-82-H	11/8/93	15.7	5.4	NA	NA	NA	7.4	104	55.7	61.0	ΥN	٧X	٧X	2.01	<0.001	9.1
EPA-82-H	7/7/94	14.7	5.9	272	492	1384	7.2	129.0	62.3	<0.05	٧×	٧X	٧V	181	100.0	2.6
EPA-82-1	[_11/93_]	NA	NA	NA	ΝA	VΑ	NA	ΑN	٧V	٧X	ΑN	¥Z.	٧Z	¥Z	89.0	٧Z
EPA-82-I	7/8/94	16.3	0.7	% -	491	1124	7.1	7.97	<0.5	10.3	AN	VΑ	٧V	<0.05	1.886	67.1
EPA-82-J	7/12/94	14.7	2.2	٧V	430	1280	7.0	158.0	<0.5	1.3	٧V	ΥN	٧N	0.05	0.052	46
MW-01	12/93-1/94	¥	0.3	Ϋ́Z	ž	¥ Z	٧×	ΝA		8.01	٧V	<0.05	<0.01	<0.0\$	0.041	VV
MW-01 duplicate	12/93-1/94	ž	¥	٧ ٧	¥	V V	¥	ΝA	٧×	٧	ΥN	٧V	Ϋ́	×	0.042	٧
MW-02	12/93-1/94	ž	0.4	٧	¥	٧×	NA A	Y'A	40	50.5	NA.	0.25	<0.01	0.25	<0.0003	٧X
MW-03	12/93-1/94	ž	1.5	∀ Z	ž	٧	٧×	NA	4	8.2	٧V	<0.05	0.025	<0.05	0.459	٧V
MW-04	12/93-1/94	ž	1.4	¥	ž	Y 2	٧X	ΥN	4	13.6	٧V	1.68	0.637	2.32	0.012	٧×
MW-05	12/93-1/94	ž	0.7	٧	¥	٧	ΑN	NA VA	4	6.41	ΝA	<0.05	<0.01	<0.05	2.04	٧X
MW-06	12/93-1/94	٧X	0.8	Ϋ́	Ϋ́	Vγ	NA	NA NA	21	10.3	٧×	0.04	0.031	0.07	0 002	٧X
MW-07	12/93-1/94	₹ Z	4.6	¥ Z	۷ 2	٧×	٧V	VΑ	26	1.36	ΝA	11.78	0.021	8.11	100.0>	٧z
MW-08	12/93-1/94	٧X	0.2	ΝA	٧	ΝA	۲X	٧N		5.22	٧X	0.28	10:0>	0.28	900.0	¥z
MW-09	12/93-1/94	¥Z	٧	Ϋ́Z	¥	٧X	ΝA	NA	22	2.07	NA	0.4	0.577	0.4	900.0	٧X
MW-10	8/18/93	15.4	9.0	125	518	1162	7.1	44.7	63.2	<0.05	<0.05	VA V	٧X	91.6	0.004	27.8
MW-10	11/9/93	15	1.5	٧	Ϋ́	VA	7.4	33.9	53.1	0.22	Y.	٧X	٧V	17.4	0.001	53
MW-10 duplicate	11/9/93	٧Z	٧X	Ϋ́Z	¥	ΥV	NA	NA	NA	VΥ	AN	VΑ	٧N	171	¥Z	Y.
MW-10	7/2/94	16.6	<0.5	9-1-	505	9/01	7.3	47.1	19.5	80	Ϋ́	¥Z	¥	2.67	900'0	9.3

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TABLE 4.5 (Concluded) GROUND WATER GEOCHEMICAL DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

L	_ ا	Dissolved		Total					Ferrous				NO2+NO3		
e Temp. Oxygen Potential	Oxygen Potential	tential	Alk	Alkalinity	Conductivity		Chloride	Sulfate	Iron	Ammonia	Nitrate	Nitrite	Nitrogen	Methane	5
Date (°C) (mg/L) (mV) (mg/L	(mg/L) (mV) (mg/I	ľ/gm)	(mg/L	1	.) (uS/cm)	된	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
1 77	177	13	63	ξĹ	NITOKING W	31	ING LOCA	IONS (Con	inued)	36.0	NA.	417	71.0	6110].
AN AN	AN AN	+	Ž	Т	NAME OF THE PERSON NAME OF THE P		¥Z	2 8	: 6	YN YN	¥ 2	Ž	¥Z	2600	•
╀	AN 1.0	-	¥z	_	Ϋ́Z	7.4	29.5	1.42	0.05	ž	¥	¥X	0.17	0.022	-
NA NA NA	NA NA		NA		٧×		٧×	ΥN	٧×	¥Z	ΥN	Ϋ́	٧×	ΥN	3.8
15.8 <0.5 140	<0.5 140	Н	504		1125	7.0	27.0	0.66	<0.05	٧V	NA	٧V	<0.05	0.005	3.5
15.3 <0.5 171	<0.5 171	Н	450	_	656	7.1	13.2	29.2	<0.05	NA	NA	٧V	7.73	0.005	2.4
NA NA NA	NA NA		ΑN		NA	NA	NA	3	10.3	NA	90.0	0.037	1.0	0.498	٧V
NA NA NA	NA NA		٧V		NA	NA	NA	NA	NA	٧V	٧V	NA	٧X	0.483	٧×
NA NA NA	NA NA	H	Ν		Ϋ́Α	٧V	ΑĀ	27.0	2.96	Ϋ́	1.12	0.187	161	0.023	ž
\dashv	NA NA	\dashv	ΨV	_1	NA	VV	NA	Y	¥	YY V	¥Z	4×	¥	0.023	¥
136	136	-	100	L	GEOP	OBE SAM	LINGLOCA	TIONS	300			1	96 (77000	1
8/3/61 22 24 SOL	55 NA	$\frac{1}{1}$	Ş Ž		Y N	¥	¥	¥.	Z Y	ž	£ \$	Ž	××××××××××××××××××××××××××××××××××××××	¥ ×	ž
1.1 22 1.1	01- 1.1	-	451	1	1495	7.3	189	8.05	0.2	0.21	¥	¥	2.13	0.0064	-7
AN AN AN	YZ YZ		Ϋ́	L	Ϋ́Z	٧X	109	34.8	0.2	0.26	٧×	¥	1.85	0000	ž
NA NA NA	NA NA	Ľ	VΑ		NA	NA	108	34.6	NA	0.17	VΑ	Ϋ́	161	NA	٧×
20 1 1.1 180	1.1 180	Ц	440		1151	7.4	90.2	39.4	<0.05	0.11	NA	٧V	3.89	0.0017	9.1
NA NA NA	NA NA		AN	L	NA	NA	90.3	39.8	9.0	AN	NA	٧V	٧V	٧N	Y.
25 0.5 -63	0.5 -63	H	612		1196	7.1	50.5	5.68	9.0	66.0	NA	¥	61.0	0.0564	5.4
NA NA NA	NA NA	Ц	NA		ΥV	ΝA	VΑ	NA	NA	NA NA	٧V	¥	ΥA	0.0552	٧×
19 NA 274	NA 274	Н	632		1451	7.4	118	51.2	0.1	0.14	٧V	٧Z	2.7	0.0001	2.1
18.7 4.3 NA	4.3 T NA 1	Н	٧N		ΝA	ΥN	٧V	NA	NA	ΥN	٧V	Ϋ́	NA	٧٧	NA
2 99	2 99	Н	457		1604	7.1	٧V	NA	<0.05	0.3	٧٧	٧¥	1.4	0.0007	2.7
22.5 NA :137	NA -137		452		1256	7.	107	52.6	<0.05	<0.05	ž	ž	3.9	0.0541	6
AN AN	AN AN	\dashv	¥Z		¥2	¥	٧X	¥Z.	٧	¥	٧×	۲ ۲	¥	٧×	2
NA NA	AX Y	+	₹	_	YZ.	¥	¥	¥.	¥.	61.0	≱	≱ Ž	1.59	YN V	ž
AN AN AN	4 5 NA	+	Ž V	Т	NA N	Y X	V V	NA NA	- N	O V	¥ 2	¥ 2	S V	ZCOO O	7 2
L	4.2 152	L	378	Т	1082	7.3	116	47.4	<0.05	<0.0>	¥	¥	469	0.0111	61
NA NA NA	NA NA	H	Ϋ́	П	Ϋ́	NA	170	58	Ϋ́	<0.05	٧Z	¥	3.77	0.035	33
NA NA NA	NA NA	Н	٧X	П	ΝA	NA	٧X	Ϋ́	VΑ	٧V	ΝĀ	ΑN	NA.	٧N	3.3
18 1.8 56	1.8 56		646		1628	7.3	Ϋ́Z	٧×	<0.05	Ϋ́	٧×	ž	٧Z	٧×	ž
21 NA 179	NA 179	\mathbb{H}	_ \$92	П	1525	7.7	191	\$6.8	0.05	<0.05	٧×	¥	4.17	0.0141	2.8
Ϋ́	YZ YZ	\dashv	ž	7	Ϋ́	٧×	¥	¥	∀ Z	¥	ž	ž	ž	0.0219	2.9
24 NA 207	NA 207	+	451		1321	8.3	114	31.5	<0.05	<0.05	ž	¥	4.13	ž	4 Z
NA NA NA	NA NA	Ц	Ϋ́		NA	XX	911	X.	٧×	Ϋ́	NA.	٧×	٨V	٧V	٧V
NA NA NA	NA NA		NA NA		NA	NA	VΥ	NA	V.	NA	٧V	٧Z	NA	0.0212	80
901- <0.5 -106	901- 5:0>		730		1662	7.1	112.0	<0.5	2.4	٧×	٧×	¥z	<0.05	8100	3.6
NA NA NA	NA NA	L	٧×	, –	¥	٧×	٧×	AN	YX	ž	٧×	٧X	<0.05	Ϋ́N	4.4
17.6 <0.5 -30	<0.5 -30	L	732	_	1584	7.1	86.4	36.0	1.0	٧×	¥z	٧Z	0.05	0.003	3.1
<0.5	<0.5	L	38	Γ	1530	7.3	1.06	019	0.1	٧×	¥Z	٧X	0.3	0 00	2.4
1.2 208	1.2 208	\vdash	999		1450	7.3	73.8	35.4	<0.05	٧×	ž	ž	1.8	0.121	50
20.6 2.0 250	2.0 250	H	256		1278	7.4	120.0	42.6	<0.05	ž	¥z	¥	1.14	7000	3.7
17.7 0.5 120	0.5 120	Н	995		1403	7.4	78.4	37.1	<0.05	٧V	VΑ	٧	1.63	1000	2.8
2.0 197	2.0 197		865		1171	7.8	0.09	8.65	<0.05	NA.	NA	٧¥	4.44	0.003	24
NA <0.5 NA	VA 0.5	\dashv	792	П	1671	7.4	148.0	<0.5	0.2	¥	¥	ž	<0.05	0 004	8 9

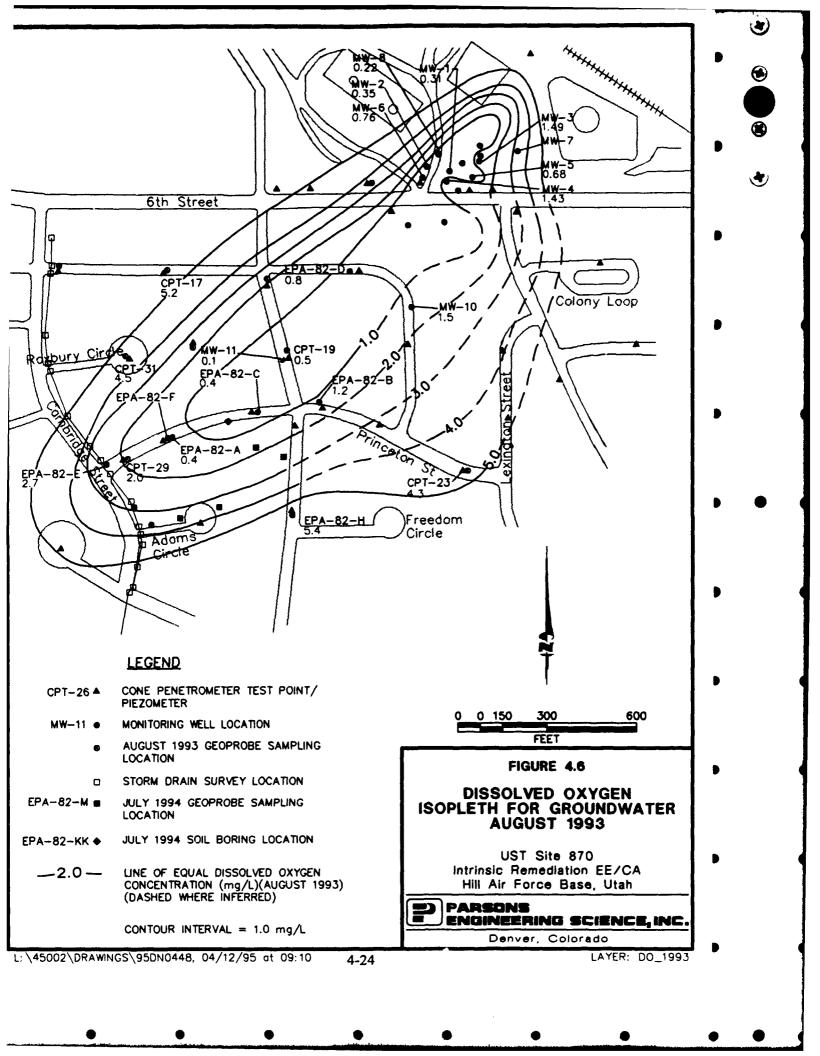
| EPA-82-P | 7/11/94 | No. See Appendix C for analytical methods EST=Estimated value reported by lab

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of Figures 4.4 and 4.6 and Figures 4.5 and 4.7 shows graphically that areas with elevated total BTEX concentrations have depleted DO concentrations. This is a strong indication that aerobic biodegradation of the BTEX compounds is occurring at the site.

In the absence of microbial cell production, the oxidation (biodegradation) of benzene to carbon dioxide and water is given by:

$$C_6H_6 + 7.5O_2 \rightarrow 6CO_2 + 3H_2O$$

Therefore, 7.5 moles of oxygen are required to mineralize 1 mole of benzene. On a mass basis, the ratio of oxygen to benzene is given by:

Molecular weights: Benzene 6(12) + 6(1) = 78 gm/moleOxygen 7.5(32) = 240 gm/mole

Mass Ratio of Oxygen to Benzene = 240/78 = 3.08:1

In the absence of microbial cell production, 3.08 mg of oxygen are required to completely mineralize 1 mg of benzene. Similar calculations can be completed for toluene (3.13 mg oxygen to 1 mg toluene), ethylbenzene (3.17 mg oxygen to 1 mg ethylbenzene), and the xylenes (3.17 mg oxygen to 1 mg xylene). The average mass ratio of oxygen consumed to total BTEX degraded is thus 3.14:1. This means that approximately 0.32 mg of BTEX is mineralized to carbon dioxide and water for every 1.0 mg of DO consumed. With a background DO concentration of approximately 6 mg/L, the shallow ground water at this site has the capacity to assimilate 1.9 mg/L (1,900 μ g/L) of total BTEX. This is a very conservative estimate of the assimilative capacity of DO because microbial cell mass production was not taken into account by the stoichiometry shown above.

When cell mass production is accounted for, the mineralization of benzene to carbon dioxide and water is given by:

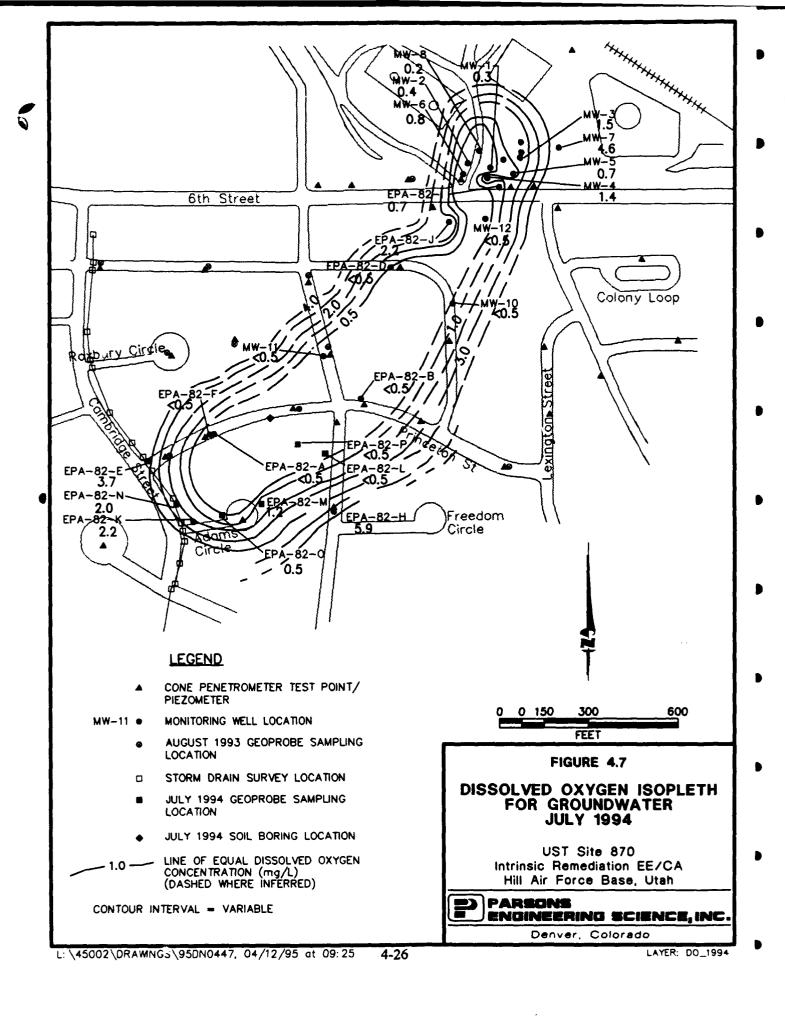
$$C_6H_6 + 2.5O_2 + HCO_3 + NH_4 \rightarrow C_5H_7O_2N + 2CO_2 + 2H_2O$$

From this it can be seen that only 2.5 moles of DO are required to mineralize 1 mole of benzene when cell mass production is taken into account. On a mass basis, the ratio of DO to benzene is given by:

Molecular weights: Benzene 12(6) + 1(6) = 78 gm/mole

Oxygen 2.5(32)= 80 gm/mole

Mass Ratio of Oxygen to Benzene = 80/78 = 1.03:1



Based on these stoichiometric relationships, 1.03 mg of oxygen are required to mineralize 1 mg of benzene. Similar calculations can be made for toluene, ethylbenzene, and the xylenes. Based on this, approximately 0.97 mg of BTEX is mineralized to carbon dioxide and water for every 1.0 mg of DO consumed. With a background DO concentration of approximately 6 mg/L, the shallow ground water at this site has the capacity to assimilate 5.8 mg/L (5,800 μ g/L) of total BTEX if microbial cell mass production is taken into account.

4.3.2.2 Nitrate/Nitrite

Concentrations of nitrate + nitrite (as N) were measured at Geoprobe locations and monitoring points/wells in August 1993, November 1993, December 1993/January 1994, and July 1994. In addition, ground water samples were collected and analyzed for ionic nitrate and nitrite in December 1993/January 1994. Table 4.5 summarizes measured nitrate and nitrite concentrations. Figure 4.8 is an isopleth map showing the distribution of nitrate + nitrite (as N) in ground water in August 1993. Figure 4.9 is an isopleth map showing the distribution of nitrate + nitrite (as N) in ground water in July 1994. These figures include data collected from monitoring wells in the source area north of Sixth Street in December 1993/January 1994. These wells cover a small area and these data represent the only data available for this area. Comparison of Figures 4.4 and 4.8 and Figures 4.5 and 4.9, shows graphically that areas with elevated total BTEX concentrations have depleted nitrate + nitrite concentrations. Comparison of Figures 4.6 and 4.8 and Figures 4.7 and 4.9, shows graphically that areas with depleted DO concentrations have depleted nitrate + nitrite concentrations. These relationships provide strong evidence that anaerobic biodegradation of the BTEX compounds is occurring at the site through the microbially mediated process of denitrification.

In the absence of microbial cell production, the biodegradation of benzene to carbon dioxide and water is given by:

$$6NO_3^- + 6H^+ + C_6H_6 \rightarrow 6CO_{2(g)} + 6H_2O + 3N_{2(g)}$$

Based on this relationship, 6 moles of nitrate are required to mineralize 1 mole of benzene. On a mass basis, the ratio of nitrate to benzene is given by:

Molecular weights:

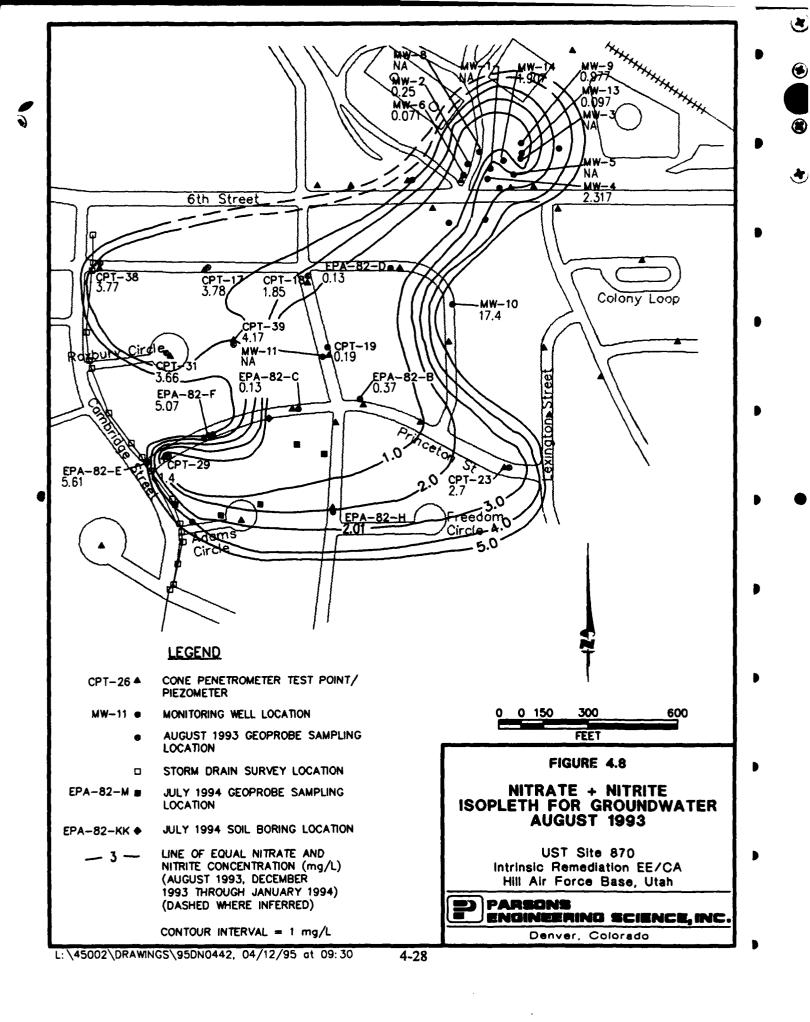
Benzene

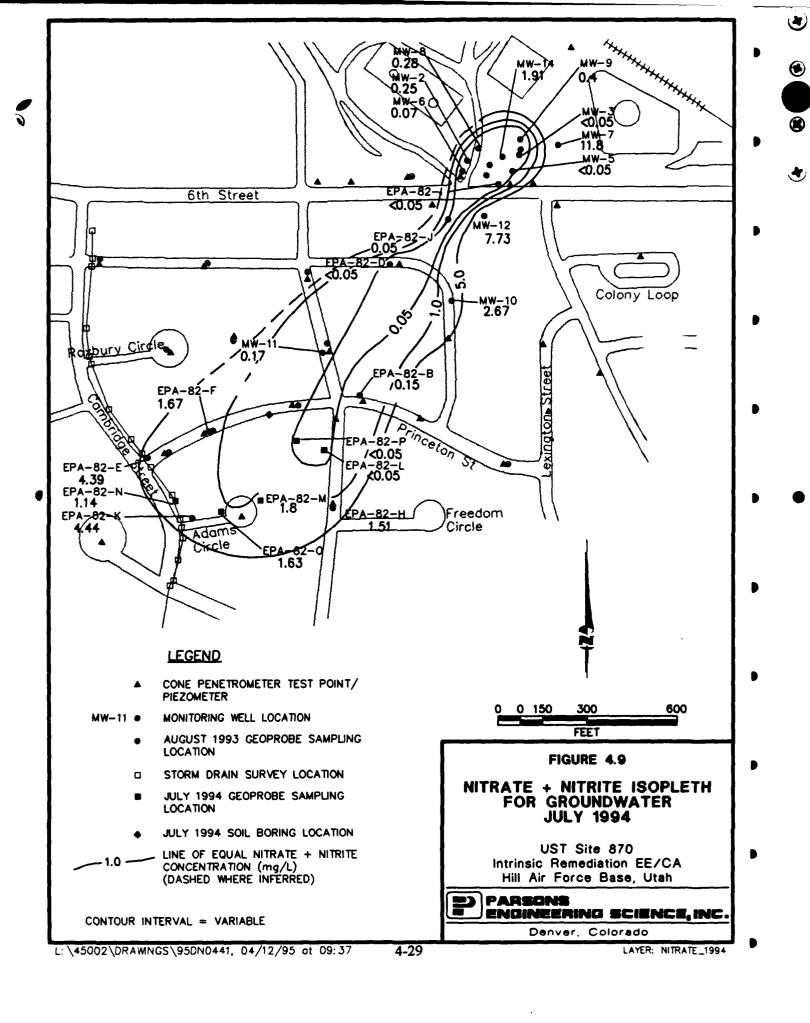
6(12) + 6(1) = 78 gm/mole

Nitrate

6(62) = 372 gm/mole

Mass ratio of nitrate to benzene = 372/78 = 4.77:1





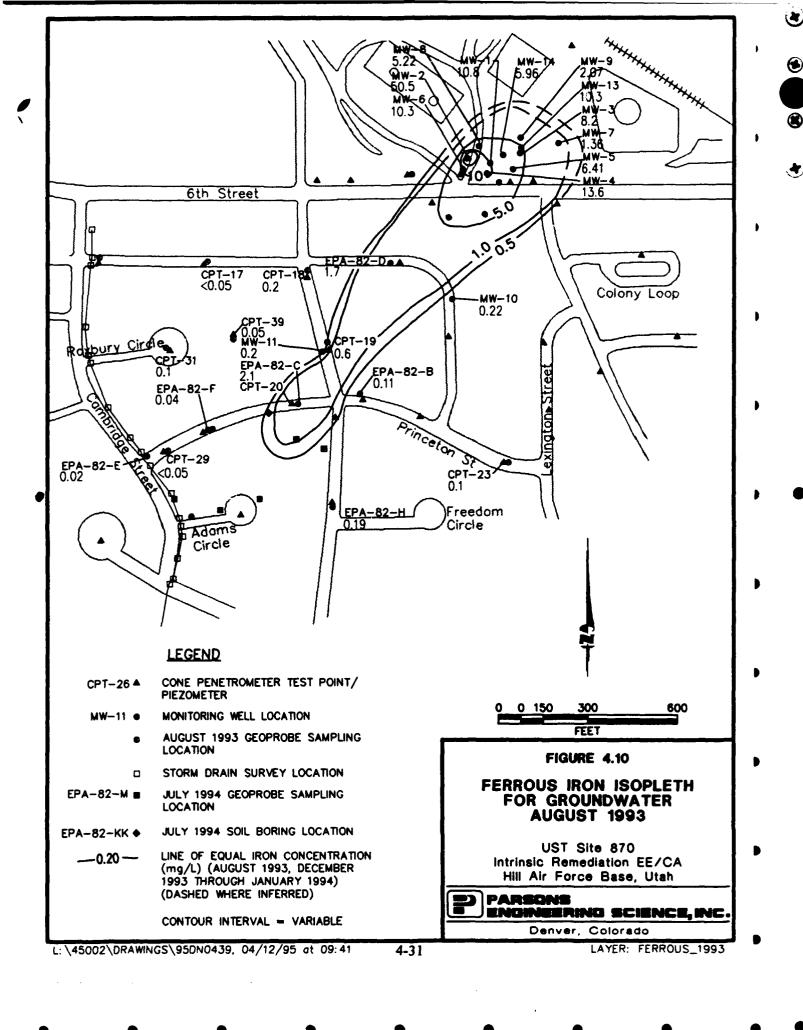
In the absence of microbial cell production, 4.77 mg of nitrate are required to completely mineralize 1 mg of benzene. Similar calculations can be completed for toluene (4.85 mg nitrate to 1 mg toluene), ethylbenzene (4.92 mg nitrate to 1 mg ethylbenzene), and the xylenes (4.92 mg nitrate to 1 mg xylene). The average mass ratio of nitrate consumed to total BTEX degraded is 4.9:1. This means that approximately 0.21 mg of BTEX is mineralized for every 1.0 mg of nitrate consumed. With a background nitrate concentration of approximately 17 mg/L, the shallow ground water at this site has the capacity to assimilate 3.57 mg/L (3,570 µg/L) of total BTEX during denitrification. This is a very conservative estimate of the assimilative capacity of nitrate because microbial cell mass production has not been taken into account by the stoichiometry shown above (see Section 4.3.2.1).

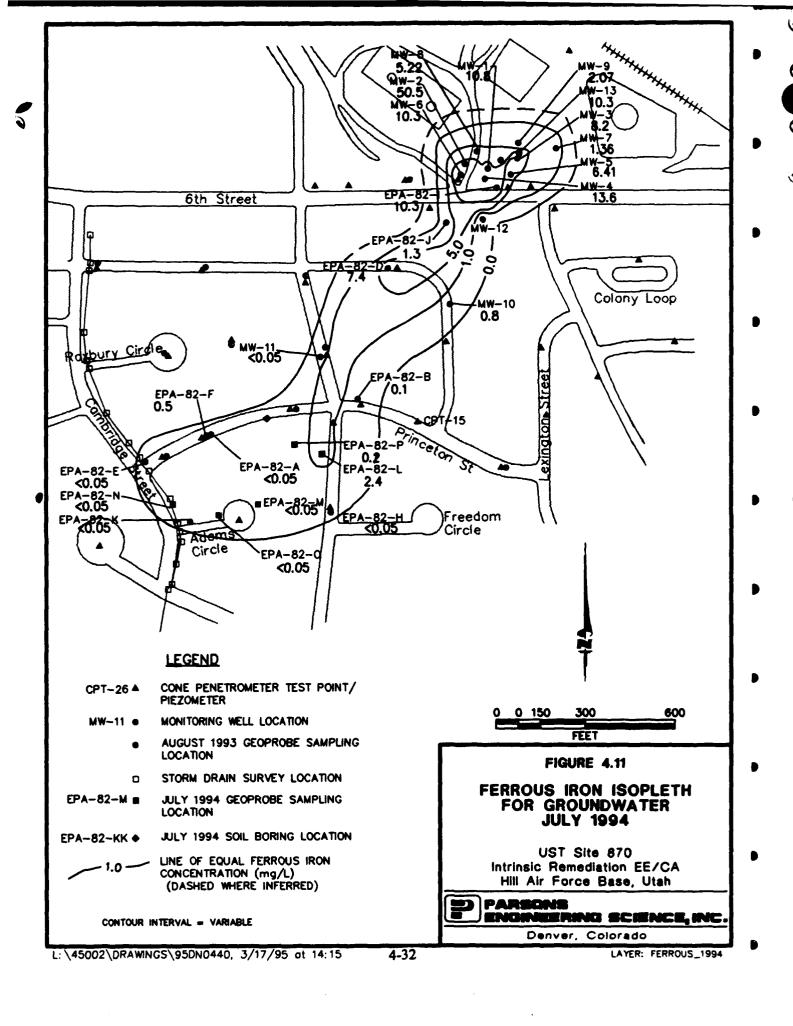
4.3.2.3 Ferrous Iron

Ferrous iron concentrations were measured at Geoprobe locations and monitoring points/wells in August 1993, November 1993, December 1993/January 1994, and July 1994. Table 4.5 summarizes ferrous iron concentrations. Figure 4.10 is an isopleth map showing the distribution of ferrous iron in ground water in August 1993. Figure 4.11 is an isopleth map showing the distribution of ferrous iron in ground water in July 1994. These figures include data collected from monitoring wells in the source area north of Sixth Street in December 1993/January 1994. These wells cover a small area and these data represent the only data available for this area. Comparison of Figures 4.4 and 4.10 and Figures 4.5 and 4.11 shows graphically that areas with elevated total BTEX concentrations have elevated ferrous iron concentrations. This is an indication that ferric iron is potentially being reduced to ferrous iron during biodegradation of BTEX compounds. However, it is possible that sulfate reduction at the site is reducing the redox potential of the ground water to sufficiently low levels to cause the dissolution of iron-bearing minerals in the shallow saturated soils at the site, thus elevating ferrous iron concentrations through non-biological processes. The highest measured ferrous iron concentration was 50.5 mg/L at monitoring well MW-02. Background levels of ferrous iron are at or below 0.05 mg/L, as measured at wells located outside of known BTEX contamination depicted on Figures 4.4 and 4.5.

The following equations describe the overall stoichiometry of benzene biodegradation by iron reduction through microbial biodegradation. In the absence of microbial cell production, the biodegradation of benzene is given by:

$$60H^{+} + 30Fe(OH)_{3,a} + C_{6}H_{6} \rightarrow 6CO_{2} + 30Fe^{2+} + 78H_{2}O$$





Therefore, 30 moles of Fe(OH)₃ are required to mineralize 1 mole of benzene. On a mass basis, the ratio of Fe(OH)₃ to benzene is given by:

Molecular weights:

Benzene

6(12) + 6(1) = 78 gm/mole

Fe(OH)₃

30(106.85) = 3205 gm/mole

Mass ratio of Fe(OH)₃ to benzene = 3205.41/78 = 41.1:1

Therefore, in the absence of microbial cell production, 41.1 mg or Fe(OH)₃ are required to completely mineralize 1 mg of benzene. Alternatively, the mass ratio of ferrous iron produced during respiration to benzene degraded can be calculated and is given by:

Molecular weights:

Benzene

6(12) + 6(1) = 78 gm/mole

Fe²⁺

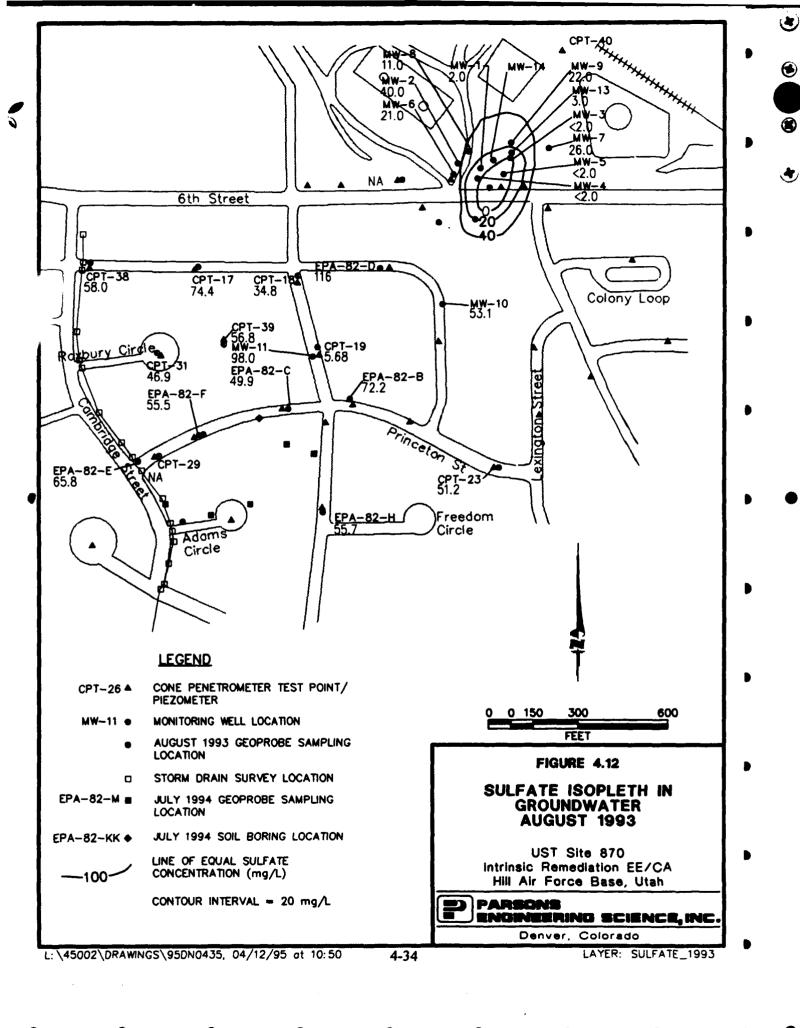
30(55.85) = 1675.5 gm/mole

Mass ratio of Fe^{2+} to benzene = 1675.5/78 = 21.5:1

Therefore, 21.5 mg of Fe²⁺ are produced during biodegradation of 1 mg of benzene. Similar calculations can be completed for toluene (21.86 mg of Fe²⁺ produced during biodegradation of 1 mg of toluene), ethylbenzene (22.0 mg of Fe²⁺ produced during biodegradation of 1 mg of ethylbenzene), and the xylenes (22.0 mg of Fe²⁺ produced during biodegradation of 1 mg of xylene). The average mass ratio of Fe²⁺ produced during total BTEX biodegradation is thus 21.8:1. This means that approximately 1 mg of BTEX is mineralized for every 21.8 mg of Fe²⁺ produced. The highest measured Fe²⁺ concentration was 50.5 mg/L. This suggests that the shallow ground water at this site has the capacity to assimilate 2.3 mg/L (2,300 µg/L) of total BTEX during iron reduction. Again, this is a very conservative estimate of the assimilative capacity of iron because microbial cell mass production has not been taken into account by the stoichiometry shown above (see Section 4.3.2.1). In addition, this calculation is based on observed ferrous iron concentrations and not on the amount of ferric hydroxide available in the aquifer. Therefore, iron assimilative capacity could be much higher.

4.3.2.4 Sulfate

Sulfate concentrations were measured at Geoprobe[®] locations and monitoring points/wells in August 1993, November 1993, December 1993/January 1994, and July 1994. Table 4.5 summarizes measured sulfate concentrations. Figure 4.12 is a map showing sulfate concentrations in ground water in August 1993. There does not appear to be any clear trend between BTEX and sulfate concentrations downgradient of the source (compare Figure 4.12 to Figure 4.5) and near the leading edge of BTEX contamination in August 1993. However,



localized sulfate reductions are seen in the source area. Figure 4.13 is an isopleth map showing the distribution of sulfate in ground water in July 1994. This figure includes data collected from monitoring wells in the source area north of Sixth Street in December 1993/January 1994. These wells cover a small area and these data represent the only data available for this area. Comparison of Figures 4.5 and 4.13, shows graphically that by July 1994, areas with elevated total BTEX concentrations had depleted sulfate concentrations. This is a strong indication that the rate of anaerobic biodegradation of the BTEX compounds through sulfanogenesis increased from 1993 to 1994. It is possible that the redox reactions required for sulfate reduction to proceed in the ground water environment in 1993 were not microbially mediated, and that the depletion of other available electron acceptors by 1994 likely increased the importance of sulfate reducing processes.

3

The following equations describe the overall stoichiometry of BTEX oxidation by sulfate reduction caused by anaerobic microbial biodegradation. In the absence of microbial cell production, the biodegradation of benzene is given by:

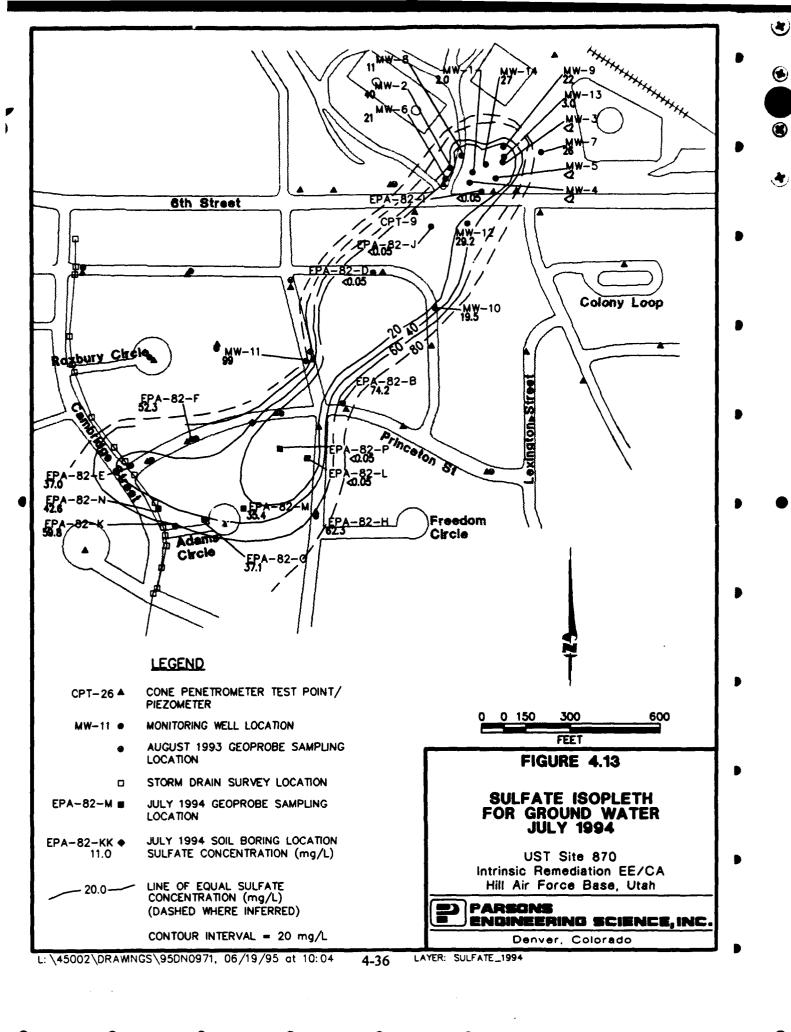
$$7.5H^{+} + 3.75SO_{4}^{2-} + C_{6}H_{6} \rightarrow 6CO_{2(g)} + 3.75H_{2}S^{0} + 3H_{2}O$$

Therefore, 3.75 moles of sulfate are required to mineralize 1 mole of benzene. On a mass basis, the ratio of sulfate to benzene is given by:

Molecular weights: Benzene 6(12) + 6(1) = 78 gm/moleSulfate 3.75(96) = 360 gm/mole

Mass ratio of sulfate to benzene = 360/78 = 4.6:1

Therefore, in the absence of microbial cell production, 4.6 mg of sulfate are required to completely mineralize 1 mg of benzene. Similar calculations can be completed for toluene (4.7 mg sulfate to 1 mg toluene), ethylbenzene (4.75 mg sulfate to 1 mg ethylbenzene), and the xylenes (4.75 mg sulfate to 1 mg xylene). The average mass ratio of sulfate to total BTEX is thus 4.7:1. This means that approximately 0.21 mg of BTEX is mineralized for every 1.0 mg of sulfate consumed. Assuming a background sulfate concentration of 100 mg/L, the shallow ground water at this site has the capacity to assimilate 21 mg/L (21,000 µg/L) of total BTEX during sulfanogenesis. Again, this is a very conservative estimate of the assimilative capacity of sulfate because microbial cell mass production has not been taken into account by the stoichiometry shown above (see Section 4.3.2.1).



4.3.1.5 Methane

Methane concentrations were measured at Geoprobe locations and monitoring points/wells in August 1993, November 1993, and December 1993/January 1994. Table 4.5 summarizes methane concentrations. Background levels of methane appear to be below 0.001 mg/L at wells located outside areas with known BTEX contamination. The highest methane concentration observed at the site was 2.04 mg/L in MW-5. Figure 4.14 is an isopleth map showing the distribution of methane in ground water in August 1993. Figure 4.15 is an isopleth map showing the distribution of methane in ground water in July 1994. These figures include data collected from monitoring wells in the source area north of Sixth Street in December 1993/January 1994. These wells cover a small area and these data represent the only data available for this area. Comparison of Figures 4.4 and 4.14 and Figures 4.5 and 4.15, shows graphically that areas with elevated total BTEX concentrations have elevated methane concentrations. This is a strong indication that anaerobic biodegradation of the BTEX compounds is occurring at the site through the microbially mediated process of methanogenesis.

Comparison of Figures 4.14 and 4.15 suggests that methanogenesis, like sulfanogenesis, may have become a more important BTEX-degradation mechanism between August 1993 and July 1994. This is consistent with other electron acceptor data found at the site with the area having elevated methane concentrations being confined to areas with depleted DO, nitrate, and sulfate concentrations and elevated ferrous iron concentrations (compare Figures 4.6 through 4.15). In addition, comparison of Figures 4.14 and 4.15 suggests that methanogenesis is becoming a more important BTEX degradation mechanism as the BTEX plume matures.

The following equations describe the overall stoichiometry of benzene biodegradation by methanogenesis. In the absence of microbial cell production, the biodegradation of benzene is given by:

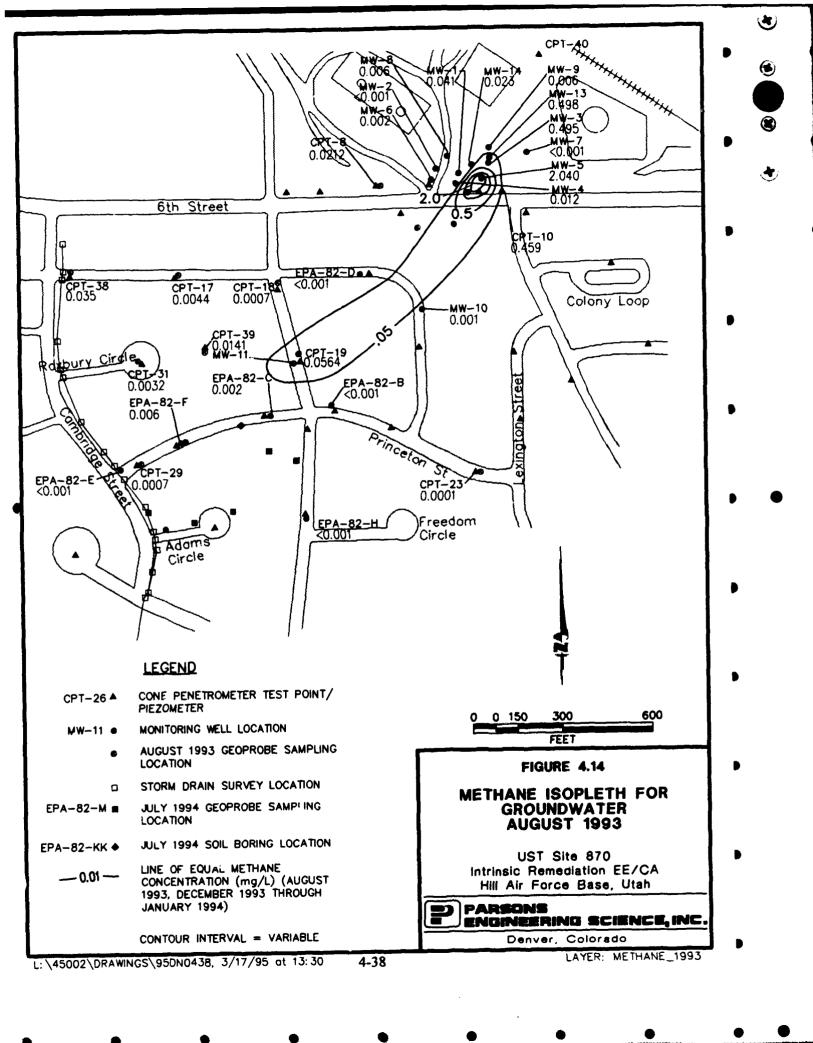
$$C_6H_6 + 4.5H_2O \rightarrow 2.25CO_2 + 3.75CH_4$$

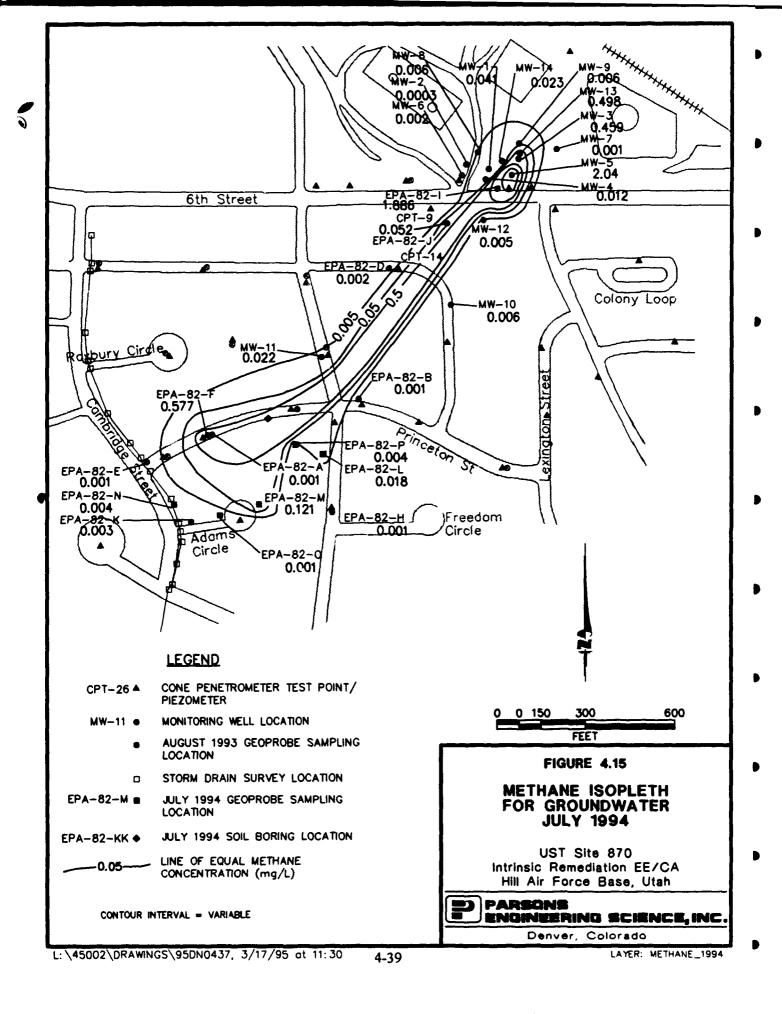
The mass ratio of methane produced during respiration to benzene degraded can be calculated and is given by:

Molecular weights: Benzene 6(12) + 6(1) = 78 gm/mole

Methane 3.75(16) = 60 gm/mole

Mass ratio of methane to benzene = 60/78 = 0.77:1





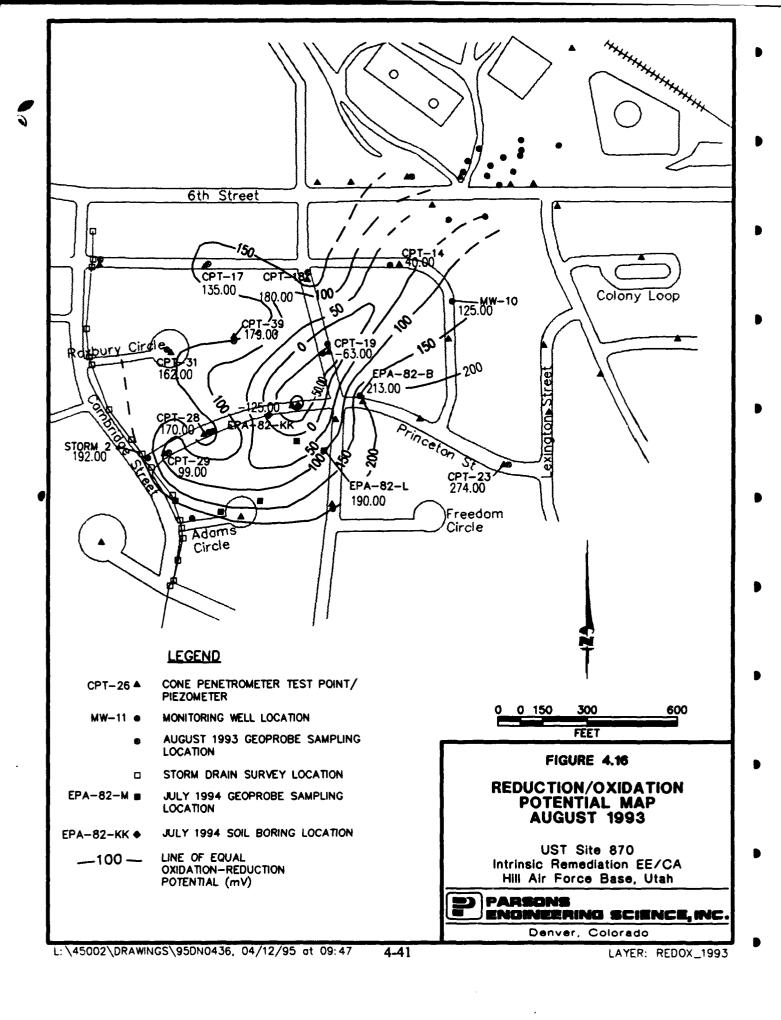
Therefore, 0.77 mg of methane is produced during biodegradation of 1 mg of benzene. Similar calculations can be completed for toluene (0.78 mg of methane produced during biodegradation of 1 mg of toluene), ethylbenzene (0.79 mg of methane produced during biodegradation of 1 mg of ethylbenzene), and the xylenes (0.79 mg of methane produced during biodegradation of 1 mg of xylene). The average mass ratio of methane produced during total BTEX biodegradation is thus 0.78:1. This means that approximately 1 mg of BTEX is mineralized for every 0.78 mg of methane produced. The highest measured methane concentration was 2.04 mg/L. This suggests that the shallow ground water at this site has the capacity to assimilate 2.6 mg/L (2,600 µg/L) of total BTEX during methanogenesis. Again, this is a very conservative estimate of the assimilative capacity of methanogenesis because microbial cell mass production is not taken into account by the stoichiometry shown above (see Section 4.3.2.1). In addition, these calculations are based or observed methane concentrations and not on the amount of carbon dioxide available in the aquifer. Therefore, methanogenic assimilative capacity could be much higher.

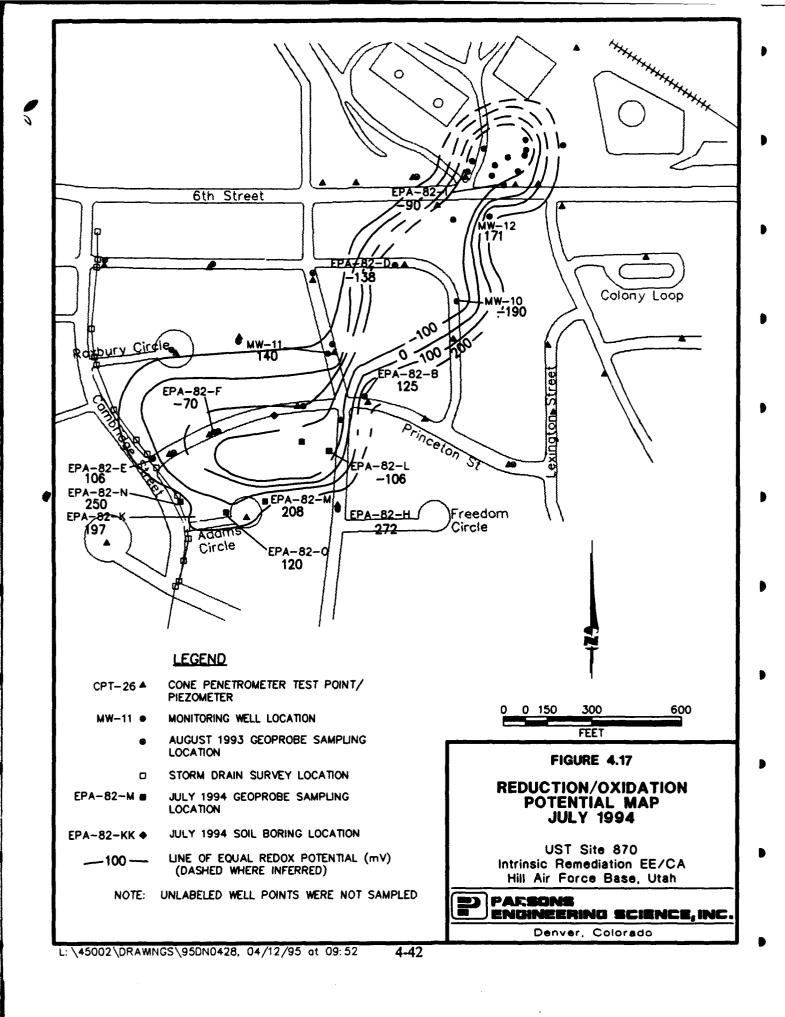
4.3.2.6 Reduction/Oxidation Potential

Redox potentials were measured at Geoprobe® locations and monitoring points/wells in August 1993, November 1993, December 1993/January 1994, and July 1994. Redox potential is a measure of the relative tendency of a solution to accept or transfer electrons. The redox potential of a groundwater system depends on which electron acceptor is being reduced by microbes during BTEX oxidation. The redox potential at UST Site 870 ranges from 274 millivolts (mV) to -137 mV. Table 4.5 summarizes available redox potential data. Figures 4.16 and 4.17 graphically illustrate the distribution of redox potentials in August 1993 and July 1994, respectively. Redox potential is decreased to a low value of -190 mV in MW-10. Areas at the site with low redox potentials coincide with areas with high BTEX contamination, low DO, nitrate, and sulfate concentrations, and elevated ferrous iron and methane concentrations (compare Figures 4.4 through 4.17). This suggests that dissolved BTEX at the site may be subjected to a variety of biodegradation processes including aerobic respiration, denitrification, iron reduction, sulfanogenesis, and methanogenesis.

4.3.2.7 Alkalinity

Total alkalinity (as CaCO₃) was measured at Geoprobe[®] locations and monitoring points/wells in August 1993, November 1993, December 1993/January 1994, and July 1994.





These measurements are summarized in Table 4.5. Alkalinity is a measure of a ground water's ability to buffer changes in pH caused by the addition of biologically generated acids. Total alkalinity at the site is fairly high, and varies from 959 mg/L at EPA-82-D to 349 mg/L at EPA-82-E. This amount of alkalinity should be sufficient to buffer potential changes in pH caused by biologically mediated BTEX oxidation reactions.

4.3.2.8 pH

The pH was measured at Geoprobe® locations and monitoring points/wells in August, 1993, November 1993, December 1993/January 1994, and July 1994. These measurements are summarized in Table 4.5. The pH of a solution is the negative logarithm of the hydrogen ion concentration [H⁺]. Ground water pH at UST Site 870 ranges from slightly acidic (6.3) to slightly basic (8.3). The majority of ground water has a pH of between 7.1 and 7.4. This range of pH is optimal for BTEX-degrading microbes.

4.3.2.9 Temperature

Ground water temperature was measured at Geoprobe[®] locations and monitoring points/wells in August 1993, November 1993, December 1993/January 1994, and July 1994. Table 4.5 summarizes ground water temperature readings. Temperature affects the types and growth rates of bacteria that can be supported in the ground water environment. Temperatures in the shallow saturated zone vary from 12.9 degrees Celsius (°C) to 25°.

4.3.3 Expressed Assimilative Capacity

The data presented in the preceding sections suggest that mineralization of BTEX compounds is occurring through the microbially mediated processes of aerobic respiration, denitrification, iron reduction, sulfanogenesis, and methanogenesis. Based on the stoichiometry presented in these sections, the expressed BTEX assimilative capacity of ground water at UST Site 870 is at least 31,370 µg/L (Table 4.6). The calculations presented in these earlier sections are extremely conservative because they do not account for microbial cell mass production. In addition, the measured concentrations of ferrous iron and methane may not be the maximum achievable. The highest plausible dissolved-phase total BTEX concentration observed at the site was 26,576 µg/L in monitoring well MW-03 in August 1992. The total BTEX concentration in this well in

December 1993/January 1994 was 9,466 μ g/L. The highest total BTEX concentration observed in July 1994 was 21,475 μ g/L.

Based on the calculations presented in the preceding sections, and on site observations, ground water at UST Site 870 has enough assimilative capacity to degrade dissolved-phase BTEX that partitions from the LNAPL plume into the ground water before the plume migrates 1,600 feet downgradient from the source area.

TABLE 4.6
EXPRESSED ASSIMILATIVE CAPACITY OF SITE GROUND WATER
UST SITE 870 INTRINSIC REMEDIATION EE/CA
HILL AFB, UTAH

Electron Acceptor or Process	Expressed BTEX Assimilative Capacity (µg/L)		
Dissolved Oxygen	1,900		
Nitrate	3,570		
Ferric Hydroxide	2,300		
Sulfate	21,000		
Methanogenesis	2,600		
Expressed Assimilative Capacity	31,370		
Highest observed Total BTEX Concentration	26,576		

SECTION 5

GROUND WATER MODEL

5.1 GENERAL OVERVIEW AND MODEL DESCRIPTION

In order to estimate degradation rates of dissolved-phase BTEX compounds at UST Site 870, and to help predict the future migration of these compounds, Parsons ES modeled the fate and transport of the dissolved-phase BTEX plume. The modeling effort had three primary objectives: 1) to predict the future extent and concentration of the dissolved-phase contaminant plume by modeling the combined effects of advection, dispersion, sorption, and biodegradation; 2) to assess the possible risk to potential downgradient receptors; and 3) to provide technical support for the natural attenuation remedial option at post-modeling regulatory negotiations. The model was developed using site-specific data and conservative assumptions about governing physical and chemical processes. Because of the conservative nature of model input, the reduction in contaminant mass caused by natural attenuation is expected to exceed model predictions. This analysis is not intended to represent a baseline assessment of potential risks posed by site contamination.

The Bioplume II computer model was used to estimate the potential for dissolved-phase BTEX migration and degradation by naturally-occurring mechanisms operating at UST Site 870. The Bioplume II model incorporates advection, dispersion, sorption, and biodegradation to simulate BTEX plume migration and degradation. The model is based upon the US Geological Survey Method of Characteristics (USGS MOC) two-dimensional (2-D) solute transport model of Konikow and Bredehoeft (1978). The model was modified by researchers at Rice University to include a biodegradation component that is activated by a superimposed DO plume. Based on the work of Borden and Bedient (1986), the model assumes a reaction between the DO and BTEX that is instantaneous relative to the advective ground water velocity. Bioplume II solves the USGS 2-D solute transport equation twice, once for hydrocarbon concentrations in the aquifer and once for a DO plume. The two plumes are combined using superposition at every particle move to simulate the instantaneous, biologically-mediated, reaction between hydrocarbons and oxygen. In recent years it has

become apparent that anaerobic processes such as nitrate reduction (denitrification), iron reduction, sulfate reduction (sulfanogenesis), and methanogenesis can be important BTEX degradation mechanisms (Grbic'-Galic' and Vogel, 1987; Lovely et al., 1989; Grbic'-Galic', 1990; Hutchins, 1991; Beller et al., 1992; Edwards et al., 1992; Edwards and Grbic'-Galic', 1992). As with DO, the reaction between nitrate and BTEX can be assumed to be instantaneous relative to the ground water flow velocity (Wilson, 1994). The Bioplume II model does not allow direct input of nitrate concentrations. Because of this, nitrate concentrations were input as DO-equivalent concentrations. The use of nitrate in this manner allowed the Bioplume II model to more accurately simulate rates of biodegradation at the site. The use of nitrate as a model input parameter is discussed in Section 5.4.5. The following sections discuss in more detail the model setup, input parameters and assumptions, model calibration, and simulation results.

5.2 CONCEPTUAL MODEL DESIGN AND ASSUMPTIONS

Prior to developing a ground water model, it is important to determine if sufficient data are available to provide a reasonable estimate of aquifer hydraulic and geochemical conditions. In addition, it is important to ensure that any limiting assumptions can be justified. The most important assumption made when using the Bioplume II model is that oxygen-limited (and in this case, oxygen/nitrate-limited) biodegradation is occurring at the site. The Bioplume II model assumes that the limiting factors for biodegradation are: 1) the presence of an indigenous hydrocarbon degrading microbial population, and 2) sufficient background electron acceptor concentrations. Data presented in Sections 3 and 4 indicate that oxygen, nitrate, ferric hydroxide, sulfate, and carbon dioxide (methanogenesis) are all being used for aerobic and anaerobic biodegradation. To be conservative, only oxygen and nitrate are used as electron acceptors in the instantaneous reaction simulated by the Bioplume II model presented herein. To model biodegradation with DO and nitrate as electron acceptors, the isopleth maps for these compounds were superimposed and combined to form a "total" electron acceptor isopleth map. These data were then used for model input.

Based on the data presented in Section 3, the shallow saturated zone was conceptualized and modeled as a shallow unconfined aquifer comprised of medium-grained, moderately sorted sands (Figures 3.3 and 3.4.). With the exception of limited mobile LNAPL removal and bioventing in the spill area, contaminated soils at the site have not been remediated.

Additional mobile and residual LNAPL removal would further reduce the continuing source of dissolved-phase BTEX contamination at the site. Several model simulations were conducted; both with LNAPL as a continuing source and with the LNAPL removed through time. Because of the low residual-phase BTEX concentrations observed in soils outside of areas containing mobile LNAPL, it was assumed that these soils represent a minimal source of continuing BTEX contamination. The use of a two-dimensional model is appropriate at Site UST 870 because the saturated interval is thin (generally less than 3 feet) and a relatively impermeable clayey silt and silty clay confining layer directly underlies the saturated zone. In addition, vertical ground water gradients at the site are upward, as is common over much of the Great Salt Lake Basin.

5.4 MODEL INPUT

Input parameters used for this model are based on a review of existing site data and a review of the pertinent literature. Where site-specific data were not available, reasonable assumptions for the types of materials comprising the shallow saturated zone were made based on widely accepted literature values. Table 5.1 lists the input parameters used for the modeling effort. Appendix D contains gridded data used as model input. Model output is presented in Appendix E as a diskette in ASCII format. The following sections describe the Bioplume II model parameters that have the greatest influence on model predictions.

5.4.1 Grid Design

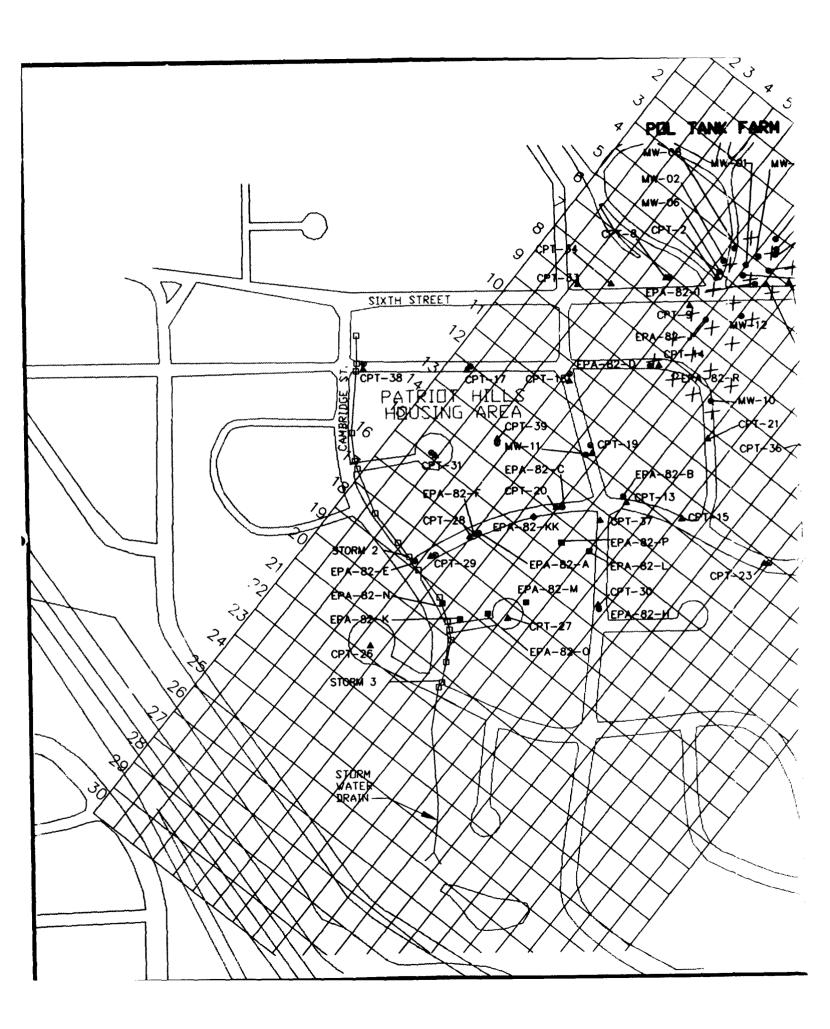
The maximum grid size for the Bioplume II model is limited to 20 columns by 30 rows. The dimension of each column and row can range from 0.1 to 999.9 feet. A 20- by 30-cell grid was used to model the Hill AFB site. Each grid cell was 110 feet long by 85 feet wide. The grid was oriented so that the longest cell dimension was parallel to the direction of ground water flow (Figure 5.1). The model grid covers an area of 5.6 million square feet, or approximately 129 acres.

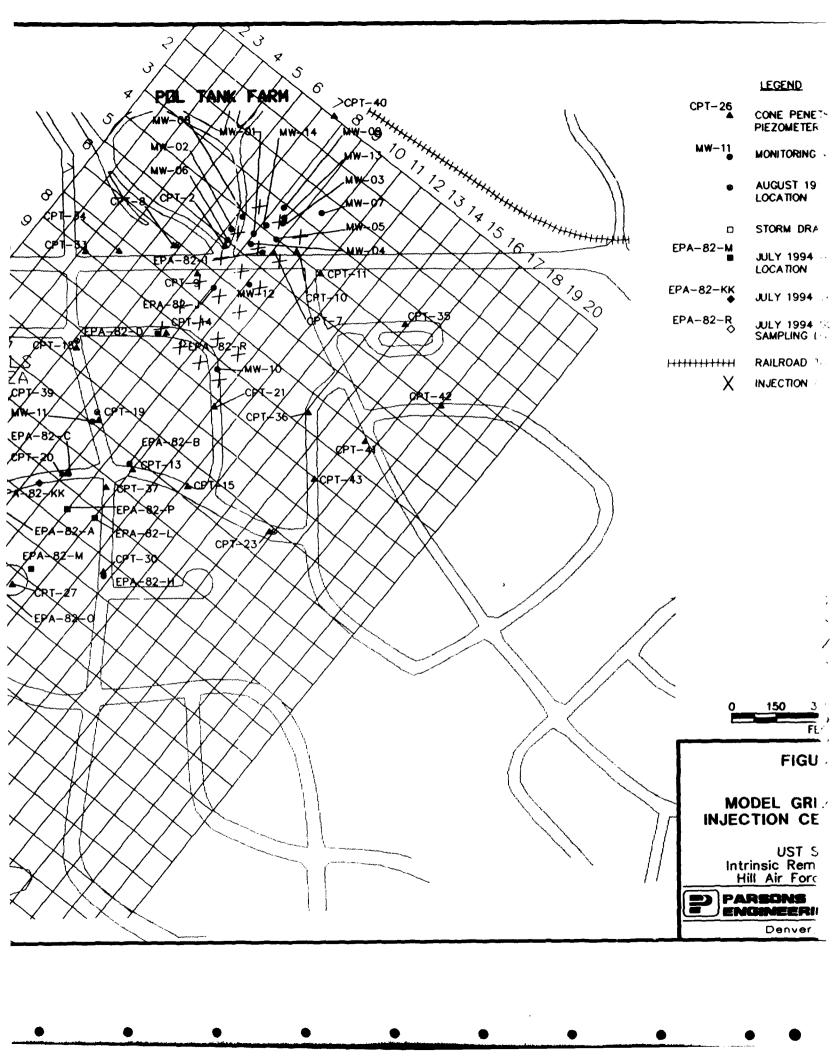
Constant-head boundaries were established along the northeast and southwest perimeter of the model grid to simulate the southwestern flow of ground water observed at the site. These constant-head cells were placed at a sufficient distance from the BTEX plume to avoid potential boundary interferences. Injection cells were used to simulate the

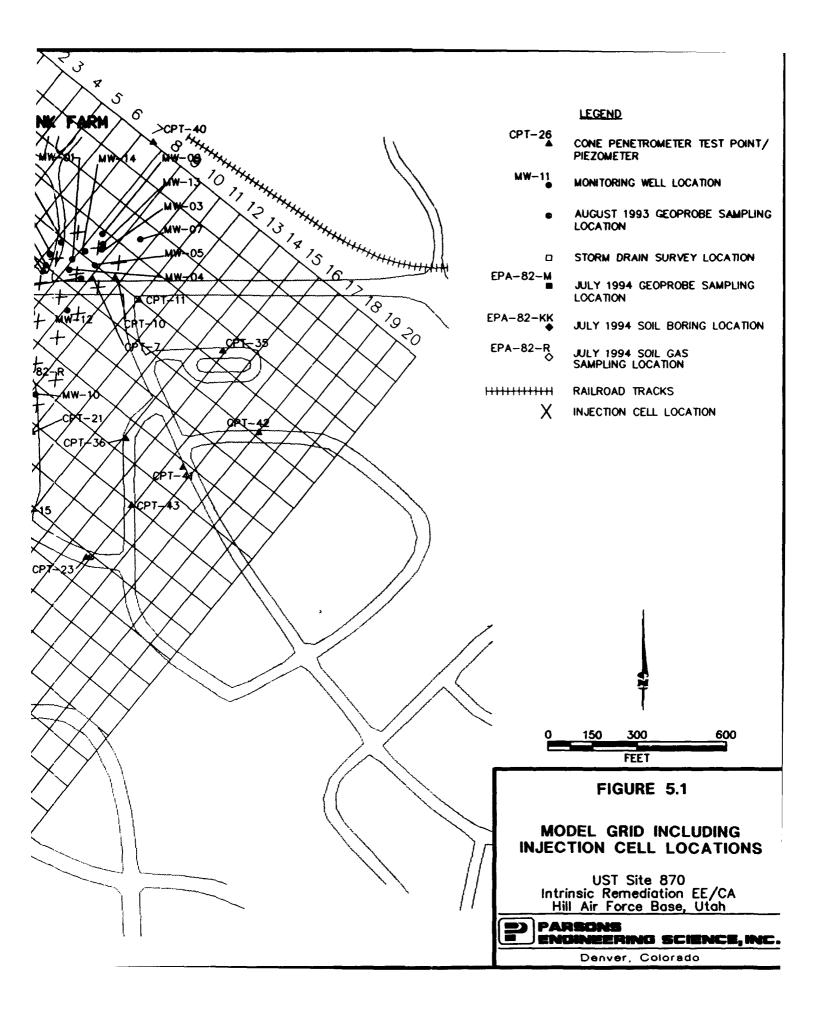
TABLE 5.1 BIOPLUME II MODEL INPUT PARAMETERS UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

Parameter	Description Outstand				
		Calibrated	Hill-A	Hill-B	Hill-C
		Model Setup			
NTIM	Max. number of time steps in a pumping period		15	2	2
NPMP	Number of Pumping Periods		1	25	12
NX	Number of nodes in the X direction		20	20	20
NY	Number of nodes in the Y direction		30	30	30
NPMAX	Maximum number of Particles		5290	5290	5290
	NPMAX=(NX-2)(NY-2)(NPTPND) +		İ	1	
	(Ne)(NPTPND) + 250				
NPNT	Time step interval for printing data	1	1	1	1
NITP	Number of iteration parameters	7	7	7	7
NUMOBS	Number of observation points		5	5	5
ITMAX	Maximum allowable number of iterations in ADIP	200	200	200	200
NREC	Number of pumping or injection wells		20	0	0
NPTPND	Initial number of particles per node	9	9	9	9
NCODES	Number of node identification codes		2	2	2
NPNTMV	Particle movement interval (IMOV)	0	0	0	0
NPNTVL	Option for printing computed velocities	2	1	1	1
NPNTD	Option to print computed dispersion	2	1	1	1
	equation coefficients				
NPDELC	Option to print computed changes in concentration	1	1	1	1
NPNCHV	Option to punch velocity data	0	0	0	0
NREACT	Option for biodegradation, retardation and decay	1	1	1	1_
PINT	Pumping period (years)		15	1	1
TOL	Convergence criteria in ADIP	0.001	0.001	0.001	0.001
POROS	Effective porosity		0.25	0.25	0.25
BETA	Characteristic length (long. dispersivity; feet)		53.4	53.4	53.4
S	Storage Coefficient	0 (Steady-	0	0	0
		State)			
TIMX	Time increment multiplier for transient flow		NA	NA	NA
TINIT	Size of initial time step (seconds)		NA	NA	NA
XDEL	Width of finite difference cell in the x direction (feet)		85	85	85
YDEL	Width of finite difference cell in the y direction (feet)		110	110	110
DLTRAT	Ratio of transverse to longitudinal dispersivity	0.1	0.1	0.1	0.1
CELDIS	Maximum cell distance per particle move	0.5	1	0.5	0.5
ANFCTR	Ratio of Tyy to Txx	1	1	1	1
		(Isotropic)			
DK	Distribution coefficient		.05451	.05451	.05451
RHOB	Bulk density of the solid (grams/cubic centimeter)		1.6	1.6	1.6
THALF	Half-life of the solute		0	0	0
DEC1	Anaerobic decay coefficient		0	0	0
DEC2	Reacration coefficient (day¹)		.003	.003	.003

NA = Not Applicable







continuing source of contamination caused by the mobile LNAPL present at the site. Injection vell locations are shown in Figure 5.1 and are explained in detail in Section 5.5.

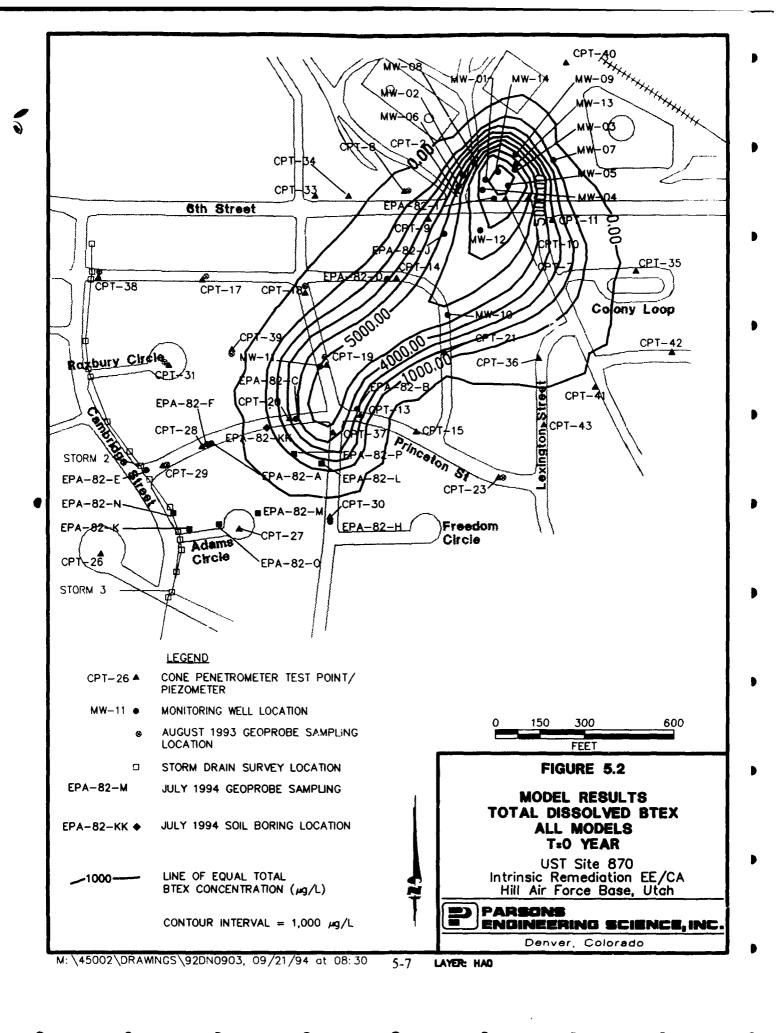
5.4.2 Ground Water Elevation and Gradient

The water table elevation data presented in Figure 3.5 were used as Bioplume II model input. Available site data suggest that there is almost no seasonal variation in ground water flow direction or gradient at the site (Appendix B and MWI, 1994). Ground water flow in the vicinity of UST Site 870 is to the southwest at an average gradient of approximately 0.043 ft/ft between wells EPA-82-I and EPA-82-E. As described in Section 5.5, the ground water flow model was calibrated to the observed water table.

5.4.3 BTEX Concentrations

The highest total-dissolved BTEX concentrations obtained from laboratory analytical data for the period through August 1993 were used for model development. Figure 4.4 shows the spatial distribution of the highest (most conservative) dissolved-phase BTEX compounds detected through August 1993. Table 4.4 contains dissolved BTEX concentration data. Appendix D contains the gridded total BTEX concentrations used as model input.

The BTEX data from Figure 4.4 was used in model development by placing the model grid over the isopleth contours. The total BTEX concentration used in the model, and shown in Appendix D, is an estimated average concentration of all the isopleth lines intersecting the boundaries within each model cell. The highest concentration isopleth lines were not used for allocating BTEX concentrations to model cells because a single isopleth concentration was not representative of the average total BTEX concentrations over the entire 85 feet by 110 feet model cell. Figure 5.2 shows the distribution of the BTEX plume as calculated by the Bioplume II model for T=0 for all models. Comparison of Figures 4.4 and 5.2 shows that there is good agreement between the actual BTEX distribution in the shallow saturated zone and the initial distribution calculated by the Bioplume II model. The initial BTEX plume covers an area of approximately 650,000 square feet (15 acres). The shape and distribution of the total BTEX plume is the result of advective transport of dissolved-phase BTEX contamination downgradient from the LNAPL contamination present in the source area.



Partitioning of BTEX compounds from the LNAPL into the ground water is described in Section 5.5.

5.4.4 Hydraulic Conductivity

Hydraulic conductivity (K) is an important aquifer characteristic that determines the ability of the water-bearing strata to transmit ground water. An accurate estimate of this parameter is important to help quantify advective ground water flow velocities, to define the flushing potential of the aquifer, and to estimate the quantity of electron-acceptor-rich ground water that is entering the site from upgradient locations. Rifai et al. (1988) report that the Bioplume II model is particularly sensitive to variations in hydraulic conductivity. Lower values of hydraulic conductivity result in a slower-moving plume that degrades at a slower rate because less oxygen and nitrate are available for biodegradation. Higher values of hydraulic conductivity result in a faster moving plume that degrades at a faster rate because more oxygen and nitrate are available for biodegradation.

Based on slug tests performed at the site, hydraulic conductivity varies from 1.08x10⁻⁴ ft/s to 6.08x10⁻⁴ ft/s. This is within the accepted range for sandy materials (Freeze and Cherry, 1979). Slug test results used for modeling do not reflect slug test data collected by JMM (1993) at MW-1. MW-1 was screened in a soil interval characterized by silty sands with a large interval (-4 ft) of clayey sand. As a result, slug test data from MW-1 was not considered representative of the fine- to medium- grained sandy soils located around the screened monitoring wells used for Parsons ES slug tests in 1993. The sensitivity of the model to this parameter was evaluated during the sensitivity analysis described in Section 5.6.

5.4.5 Electron Acceptors (Oxygen and Nitrate)

As discussed previously, the Bioplume II model assumes an instantaneous reaction between the BTEX plume and the electron acceptors. As discussed in Section 4, it is apparent that DO, nitrate, ferric hydroxide, sulfate and carbon dioxide (methanogenesis) are being used as electron acceptors for biodegradation of BTEX compounds at UST Site 870. However, to be conservative, the total BTEX plume at UST Site 870 was modeled assuming that oxygen and nitrate were the only electron acceptors being utilized at a rate that is instantaneous relative to the advective ground water velocity for the biodegradation of the BTEX compounds.

The Bioplume II model was calibrated with DO as the only electron acceptor. The result of using DO as the only electron acceptor was a modeled BTEX plume that extended nearly twice as far (and past the Hill AFB boundary) downgradient than the plume observed in 1994. Based on these results, it was clear that DO is not the only electron acceptor being utilized for BTEX biodegradation. Successful calibration of the Bioplume II model required the use of nitrate, which is the most thermodynamically favorable electron acceptor following oxygen. Furthermore, decreases in nitrate concentrations from anaerobic biodegradation processes were observed in areas with reduced DO concentrations (compare Figures 4.6 and 4.7 with Figures 4.8 and 4.9, respectively). This strongly suggests both denitrification and aerobic oxidation are important biodegradation mechanisms at the site. Although some localized areas on the fringe of the BTEX plume overestimated the actual rate of denitrification because of background DO concentrations, both aerobic oxygenation and denitrification of BTEX contamination were widely observed in the same areas. Therefore, simulating nitrate concentrations with DO concentrations in the model was not an overgeneralization of site electron acceptor potential (as might initially be presumed), but instead was an improved representation of site conditions. Related modeling initiatives to improve simulations of BTEX biodegradation in ground water systems are being accomplished by incorporating nitrate, and other potential anaerobic electron acceptors (e.g., ferric iron, sulfate, and carbon dioxide) into the model code, specifically within the code of the soon-to-be released Bioplume III ground water model (Rifai, 1995).

The loss of DO and nitrate in the Bioplume II model was conceptualized with aerobic bacteria using DO, and then with anaerobic bacteria using nitrate as the next available electron acceptor. This assumption is justified based on the observation that aerobic oxidation and denitrification are important biodegradation mechanisms at the site. Once utilized, DO and nitrate will react instantaneously with BTEX relative to the advective groundwater velocity in the aquifer (Borden and Bedient, 1986; Wilson, 1994).

Ground water samples collected in uncontaminated portions of the aquifer indicate that background DO concentrations at the site are about 6.3 mg/L. To be conservative, background DO concentrations were assumed to be 5.0 mg/L for Bioplume II model development. Table 4.5 contains DO data for the site. Figures 4.6 and 4.7 are DO isopleth maps. Gridded oxygen input data are included in Appendix D.

Ground water samples collected in uncontaminated portions of the aquifer indicate that background nitrate (as N) concentrations at the site may be as high as 17 mg/L. However, to be conservative, nitrate (as N) concentrations around the periphery of the plume were assumed to be 5 mg/L for Bioplume II model development. Table 4.5 contains nitrate data for the site. Figures 4.8 and 4.9 are nitrate isopleth maps. Gridded nitrate data are included in Appendix D.

The upgradient constant-head cells in the Bioplume II model require background electron acceptor concentrations to be input as constant concentrations to simulate incoming electron acceptors. To be conservative, a DO concentration of 5 mg/L and a nitrate (as N) concentration of 10 mg/L was used for these cells.

Bioplume II® is capable of tracking only a single electron acceptor as an instantaneous reaction in model simulations (customarily DO) for estimating BTEX biodegradation. Consequentially, the model cannot estimate both DO and nitrate biodegradation mechanisms simultaneously unless one electron acceptor is mathematically converted to an equivalent form of the other. Denitrifying conditions were modeled by converting nitrate concentrations to equivalent oxygen concentrations. On a mass basis, 4.77 mg of ionic nitrate are required to oxidize 1 mg of benzene, whereas, only 3.08 mg of DO are required to oxidize the same mass of benzene. Hence, ionic nitrate has only 64.6 percent of the capacity to biodegrade benzene that DO does. Converted ionic nitrate concentrations were combined with DO concentrations for a total oxygen/ionic nitrate electron acceptor map. The calculations used to convert nitrate (as N) to oxygen equivalent ionic nitrate are discussed below.

Nitrate concentrations at UST Site 870 were reported together with nitrite concentrations as nitrate + nitrite (as N) by RSKERL. Based on these data it is not possible to determine the relative amounts of nitrate and nitrite (as N); however, because nitrite is considered metastable in the ground water environment, it was assumed that the combined nitrate + nitrite (as N) value was all nitrate (as N). The work of von Gunten and Zobrist (1993) supports this assumption as does site-specific data (Table 4.5). These workers conducted column experiments using nitrate as an electron acceptor and noted that only small amounts of nitrite were detected in the column in the early stages of the experiment, and after 20 days, nitrite was no longer detected.

The use of nitrate as an electron acceptor requires that nitrate (as N) concentrations be converted to ionic nitrate concentrations. To do this, the equivalent weight of oxygen must be added back to the nitrate (as N) concentration:

Molecular weight of N = 14 gm/mole Molecular weight of O = 16 gm/mole Molecular weight of NO₃ = 62 gm/mole

The percentage of N in NO_3 is 14/62 = 22.58 percent. Therefore, 1 gm of NO_3 (as N) is valent to 1/0.2258 = 4.43 gm of ionic NO_3 . To convert nitrate (as N) into ionic nitrate centrations, the measured nitrate (as N) concentration must be multiplied by 4.43.

Assuming complete mineralization of benzene to carbon dioxide and water, the reactions for aerobic respiration and denitrification are as follow:

Aerobic Respiration

$$C_6H_6 + 7.5O_2 = 6CO_2 + 3H_2O$$

Denitrification

$$6NO_3^+ + 6H^+ + C_6H_6 = 6CO_2 + 6H_2O + 3N_{2(g)}$$

Based on this stoichiometry, 7.5 moles of DO are required to biodegrade 1 mole of benzene, and 6 moles of nitrate are required to biodegrade 1 mole of benzene. On a mass basis:

$$(7.5 \text{ moles O}_2)(32 \text{ gm/mole O}_2) = 240 \text{ gm O}_2$$

(6 moles NO₃)(62 gm/mole NO₃)= 372 gm NO₃

From these relationships, it is apparent that, on a mass basis, more ionic nitrate than DO is required to oxidize a unit mass of benzene. By dividing the mass of ionic nitrate required to degrade one mole of benzene by the mass of DO required to degrade one mole of benzene, a ratio is derived that can be applied to ionic nitrate concentrations to obtain equivalent oxygen concentrations. This ratio is:

240 gm $O_2/372$ gm $NO_3^- = 0.645$ gm of O_2 equivalent per gram of NO_3^-

Therefore, 10 gm of NO₃ has an O₂ equivalence of:

 $(10 \text{ gm NO}_3)(0.645 \text{ gm of O}_2 \text{ equivalent/gm of NO}_3) = 6.45 \text{ gm}$

4

From these relationships, the following calculation must be performed to convert NO₃⁻ (as N) to an equivalent DO concentration:

 $(NO_3 (as N) (gm/L))(4.43gm NO_3 (ion)/gm NO_3 (as N))(0.65 gm O_2 eq./gm NO_3)$

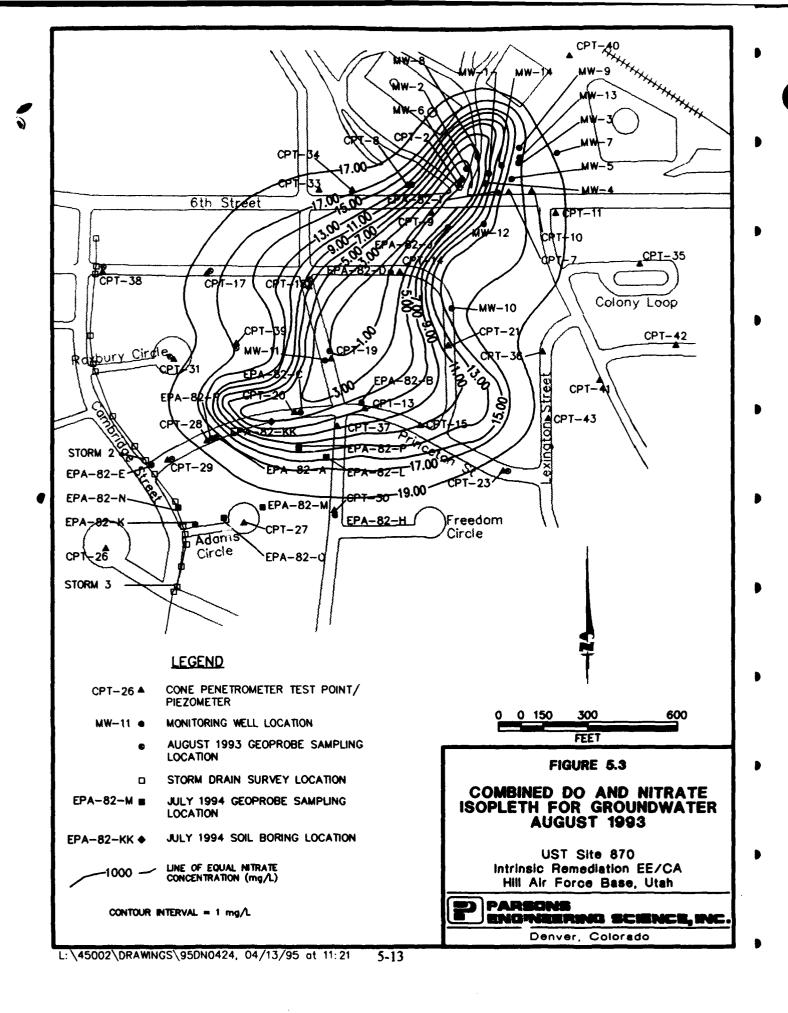
This relationship was used to convert measured nitrate (as N) concentrations into oxygen-equivalent ionic nitrate concentrations. To do this an isopleth map of nitrate (as N) was prepared and gridded. Gridded values of nitrate (as N) were then used in the relationship presented above to determine ionic NO₃ as DO equivalence. These values were then added to existing DO concentrations previously gridded at the site and used as input into the Bioplume II model. Figure 5.3 shows the combined DO and NO₃ (as DO equivalent concentrations) electron acceptor concentrations used in the Bioplume II model.

5.4.5 Dispersivity

Much controversy surrounds the concepts of dispersion and dispersivity. Longitudinal dispersivity values for alluvial sediments range from 0.1 to 200 feet (Walton, 1988). A longitudinal dispersivity of 53.4 feet was used in this model. This dispersivity was estimated by using one-tenth of the distance between the spill source and the longitudinal centroid of the plume. Transverse dispersivity values generally are at least one order of magnitude less than values of longitudinal dispersivity (Domenico and Schwartz, 1990). For this model, Parsons ES used 0.1 for the ratio of transverse dispersivity to longitudinal dispersivity. Use of an estimated value for dispersivity is appropriate because the Bioplume II model exhibits a weak sensitivity to dispersivity (Rifai et al., 1988). In addition, the sensitivity of the model to the parameter was evaluated during the sensitivity analyses described in Section 5.6.

5.4.6 Retardation

Retardation of the BTEX compounds relative to the advective velocity of the ground water occurs when BTEX molecules are sorbed to the aquifer matrix. Based on measured TOC concentrations in an uncontaminated portion of the shallow saturated zone, and assuming a bulk density of 1.6 grams per cubic centimeter (gm/cc) (Freeze and Cherry, 1979), and



published values of K_{∞} for the BTEX compounds (Martel, 1987), the coefficient of retardation for the BTEX compounds was calculated. The results of these calculations are summarized in Table 5.2. To be conservative, the minimum coefficient of retardation calculated for benzene (1.29) was used as model input.

5.4.7 Reaeration

The reaeration coefficient is a first-order decay rate constant used by Bioplume II to simulate the replenishment of oxygen into the ground water by soil gas diffusion and rainwater infiltration. Recent data on first-order biodegradation rate coefficients in groundwater at Hill AFB suggest that biodegradation rates ranged from 0.010 to 0.032 day⁻¹ over the center and periphery of the groundwater contaminant plume (Wiedemeier *et al.*, 1994). To be conservative, a first-order biodegradation rate coefficient of 0.003 day⁻¹ was used in this model. This rate coefficient was increased and decreased by one order of magnitude during the sensitivity analyses described in Section 5.6.

5.5 MODEL CALIBRATION

Model calibration is an important component in the development of any numerical ground water model. Calibration of the flow model demonstrates that a model is capable of matching hydraulic and chemical conditions observed in the field. The numerical model presented herein was calibrated by altering hydraulic parameters, boundary conditions, and stresses (i.e., injection cells) in a trial-by-error fashion until simulated heads and BTEX plumes approximated observed field conditions.

5.5.1 Water Table Calibration

The shallow water table at UST Site 870 was assumed to be influenced only by continuous recharge and discharge at the constant-head cells established at the upgradient and downgradient model boundaries. To be conservative, annual recharge of the aquifer through rainfall was not included in the model. Potential recharge by leaky stormwater sewers, collection ponds, or other sources was omitted because of a lack of reliable data. Only the

TABLE 5.2

RETARDATION CALCULATIONS FOR THE BTEX COMPOUNDS UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

Coeffice Retard Reserve O.30 1.40 0.30 1.95 0.30 3.35 0.30 0.30 0.30 0.30 0.30 0.3	K _{co} Organic Fraction Fraction Fraction Fraction Bulk nd (L/kg [±]) Carbon ^b 0.074 0.055 1.60 190 0.00094 0.00069 0.00859 0.179 0.131 1.60 center 468 0.00094 0.00069 0.00859 0.440 0.323 1.60 center 405 0.00094 0.00069 0.00859 0.381 0.279 1.60 422 0.00094 0.00069 0.00859 0.397 0.291 1.60 357 0.00094 0.00069 0.00859 0.336 0.246 1.60			Maximum	Minimum	Average		-				
K _c Organic O	K _{cc} Organic			Fraction	Fraction	Fraction	Distribution	Coefficient	Bulk		Coeffic	nent of
nd (L/kg [*]) Carbon b Carbon b Maximum cl/ Minimum cl/ Mini	nd (L/kg*) Carbon b Carbon b Carbon b Carbon b Carbon b Maximum c ² /Minimum c ² /Mi		¥		Organic		3	8 6	Density	Effective	Retar	Jation
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zene 468 0.00094 0.00069 0.00859 0.440 0.323 1.60 0.30 3.35 e 405 0.00094 0.00069 0.00859 0.381 0.279 1.60 0.30 3.03 422 0.00094 0.00069 0.00859 0.397 0.291 1.60 0.30 3.12 357 0.00094 0.00069 0.00859 0.336 0.246 1.60 0.30 2.79	zene 468 0.00094 0.00069 0.00859 0.440 0.323 1.60 e 405 0.00094 0.00069 0.00859 0.381 0.279 1.60 422 0.00094 0.00069 0.00859 0.397 0.291 1.60 357 0.00094 0.00069 0.00859 0.336 0.246 1.60	Tolueno	18	0.00094	Ĺ	0.00859	0.179	0.131	1.60	0.30	1.95	1.70
405 0.00094 0.00069 0.00859 0.381 0.279 1.60 0.30 3.03 422 0.00094 0.00069 0.00859 0.397 0.291 1.60 0.30 3.12 357 0.00094 0.00069 0.00859 0.336 0.246 1.60 0.30 2.79	c 405 0.00094 0.00069 0.00859 0.381 0.279 1.60 422 0.00094 0.00069 0.00859 0.397 0.291 1.60 357 0.00094 0.00069 0.00859 0.336 0.246 1.60	Loucille	894	0 00094	690000	0.00859	0.440	0.323	1.60	0.30	3.35	2.72
422 0.00094 0.00069 0.00859 0.397 0.291 1.60 0.30 3.12 357 0.00094 0.00069 0.00859 0.336 0.246 1.60 0.30 2.79	422 0.00094 0.00069 0.00859 0.397 0.291 1.60 357 0.00094 0.00069 0.00859 0.336 0.246 1.60	Eunyidenzene	404	00000	0 00000	0.00859	}	0.279	1.60	0.30	3.03	2.49
357 0.00094 0.00069 0.00859 0.336 0.246 1.60 0.30 2.79	357 0.00094 0.00069 0.00859 0.336 0.246 1.60	m-xylenc	Ş	0.000	0 00069	0.00859	1	0.291	1.60	0.30	3.12	2.55
		o-xylene	357	0.00094	0.00069	١	0.336	0.246	1.60	0.30	2.79	2.31
	NOIES	NOTES:				1						

From technical protocol document (Wiedemeier et al., 1994).
V From Upper Naknek data.

 $^{c1/}$ $K_d = Maximum Fraction Organic Carbon x <math>K_\infty$.

 $^{c2'}$ K_d = Minimum Fraction Organic Carbon x K_{oc}

^d Literature values.

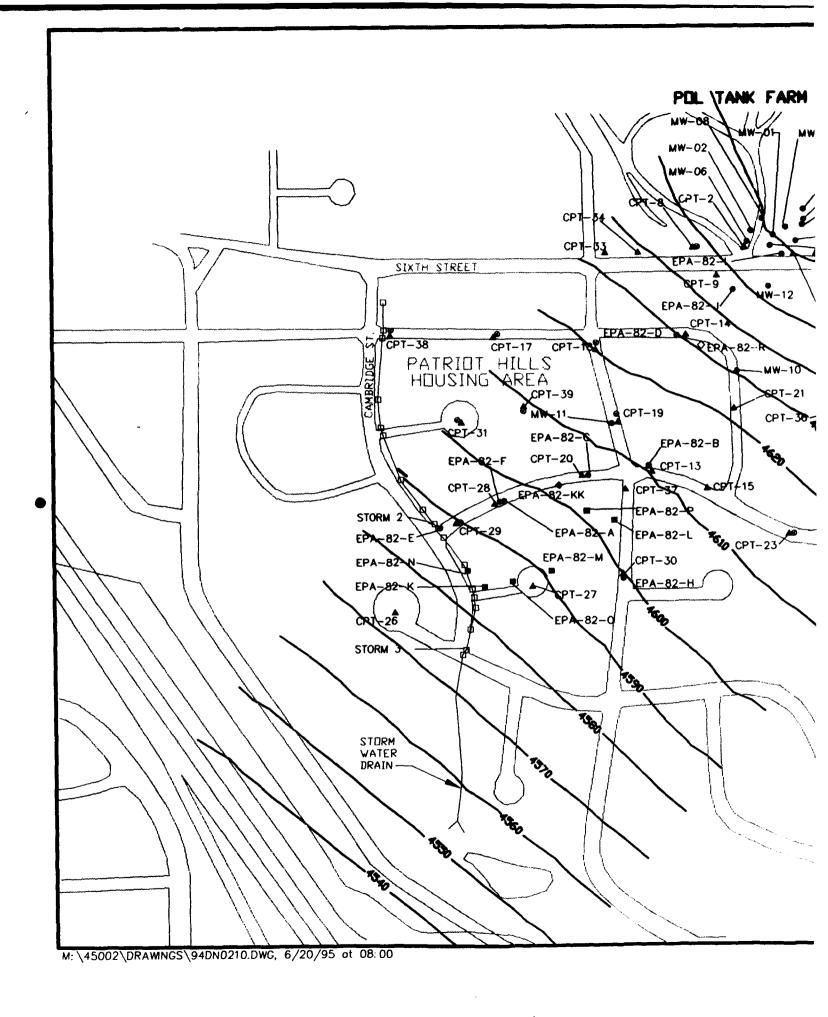
initial water levels at the constant-head cells and the transmissivity were varied to calibrate the water table surface. The model was calibrated under steady-state conditions.

Saturated thickness data from borehole logs, CPT reports, and water level measurements were used in conjunction with the average hydraulic conductivity as determined from slug tests (2.64 x 10⁻⁴ ft/s) to estimate transmissivity. To better match heads in the model to observed values, the transmissivities were progressively varied in rows and blocks until the potentiometric surface approximated the existing potentiometric surface within a 5-percent average variance. Thirteen monitoring wells and piezometer locations were used to compare between the measured and simulated heads of the final calibrations. The 13 selected locations were EPA-82-I, EPA-82-D, EPA-82-B, EPA-82-C, EPA-82-F, EPA-82-E, EPA-82-H, CPT-41, CPT-23, CPT-21, CPT-15, CPT-31, and MW-12. The root-mean-square (rms) error between observed and calibrated values at these points was 3.2 feet which corresponds to a calibration error of 2.5 percent (water levels dropped approximately 130 feet from northeast to southwest across the model grid). A plot of measured vs. calibrated heads shows a random distribution of calibrated heads and is shown in Appendix D. Deviation of points from a straight line should be randomly distributed in computer simulations (Anderson and Woessner, 1992).

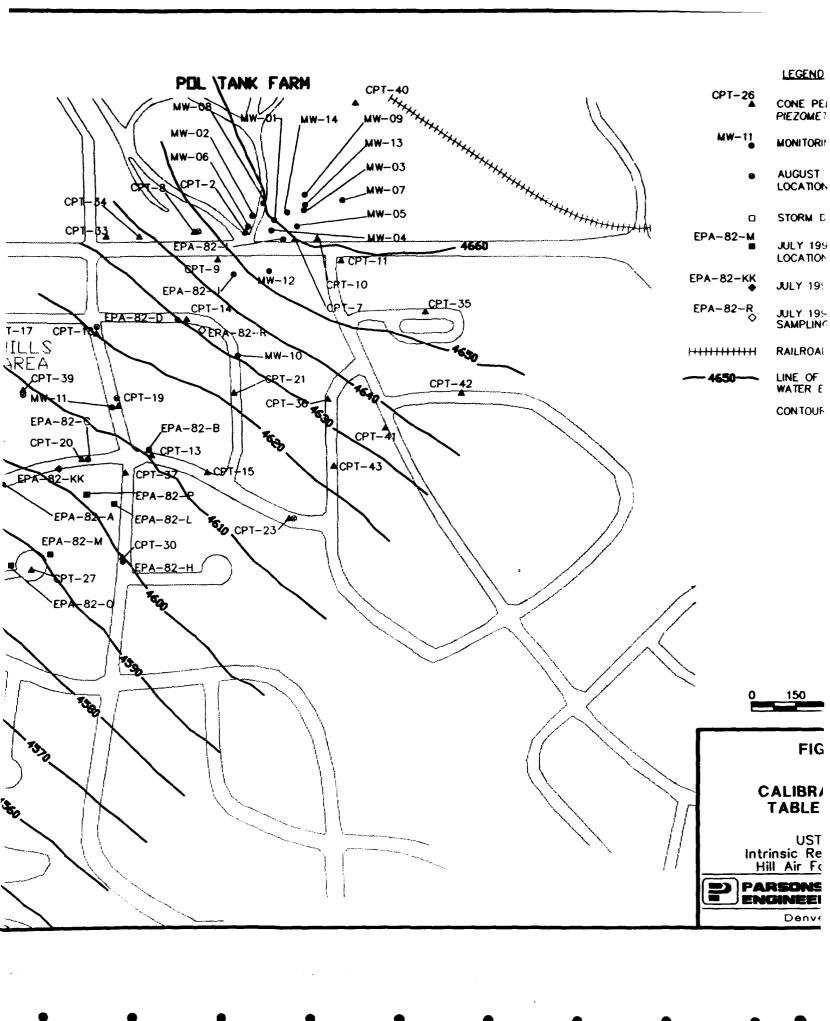
In solving the ground water flow equation, Bioplume II establishes the water table surface and calculates an overall hydraulic balance that accounts for the numerical difference between flux into and out of the system. The hydraulic mass balance for the calibrated model was excellent, with 99.95 percent of the water flux into and out of the system being numerically accounted for. Figure 5.4 shows the calibrated water table.

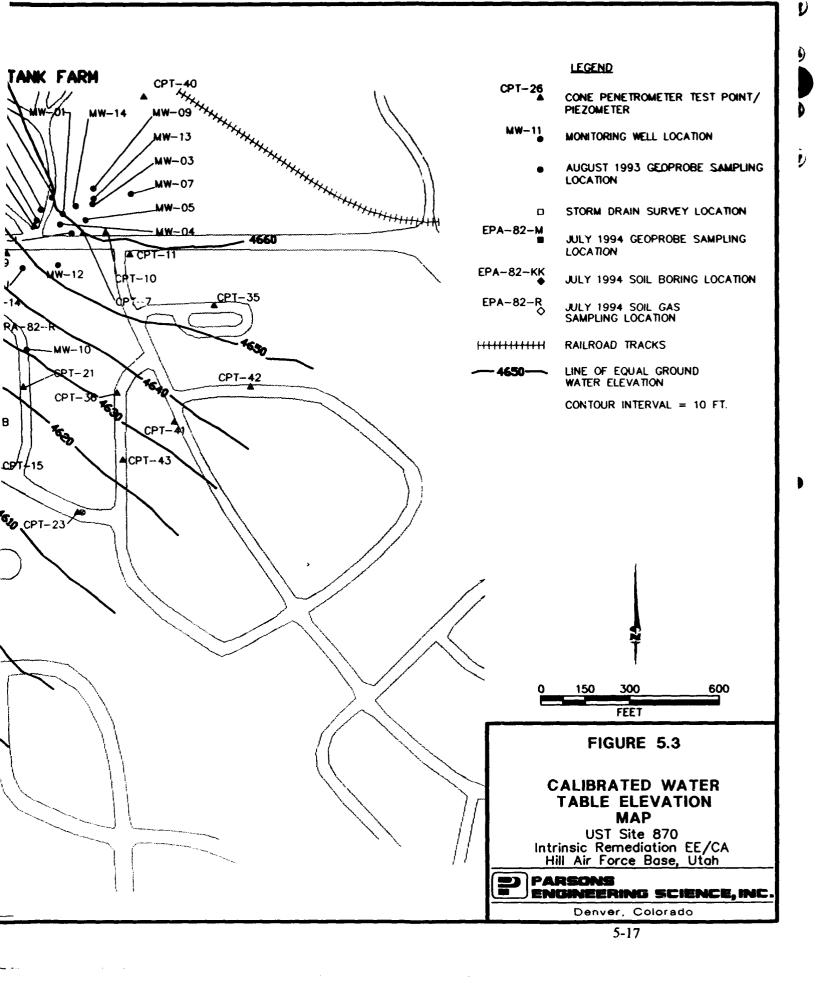
5.5.2 BTEX Plume Calibration

Model input parameters affecting the distribution and concentration of the simulated BTEX plume were modified so that initial model results closely matched dissolved-phase total BTEX concentrations observed in August 1993, and model predictions approximated dissolved-phase total BTEX concentrations observed in July 1994. The extent of dissolved-phase BTEX contamination in 1993 and 1994 is described in Section 4.3.1. Because LNAPL is present at the site, it was necessary to include 20 injection cells to simulate partitioning of BTEX compounds from the LNAPL into the ground water. The location of the injection cells is shown on Figure 5.1. Chemical analysis of LNAPL from MW-10 indicate that the



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LNAPL at the site is probably dominated by JP-4 jet fuel. LNAPL contamination is estimated to cover an area of approximately 225,000 square feet (Figure 4.1).

The injection rate of the cells was set at 5 cubic feet per day (cfd), a value low enough so that the ground water elevation calibration was not affected Total BTEX injection concentrations were determined by varying the injection concentration in the various cells from 1 to 1,650 mg/L until the initial total BTEX plume generated by the model approximated the total BTEX plume observed in August 1993, and the model predictions approximated the change in dissolved-phase total BTEX concentrations that occurred between August 1993 and July 1994. Relatively high BTEX concentrations were injected in upgradient injection cells because of the influx of 34 mg/L of combined oxygen and ionic nitrate electron acceptor concentrations (5 mg/L DO and 10 mg/L nitrate as N) introduced at the upgradient constanthead cells. This high replenishment of available electron acceptors quickly degraded BTEX concentrations at the head of the plume as they flushed through the aquifer, which in turn required large injection concentrations of BTEX to maintain observed BTEX contours. By varying the injection well concentrations, the BTEX plume was calibrated reasonably well to the change in the total BTEX plume between August 1993 and July 1994 in terms of migration distance and BTEX concentrations directly under the LNAPL contamination.

5.6 SENSITIVITY ANALYSIS

The purpose of the sensitivity analysis is to determine the effect of varying model input parameters on model output. Based on the work of Rifai et al. (1988), the Bioplume II model is most sensitive to changes in the coefficient of reaeration, the coefficient of anaerobic decay, and the hydraulic conductivity of the media, and is less sensitive to changes in the retardation factor, porosity, and dispersivity. A first-order anaerobic decay coefficient was not used because nitrate was included in the original oxygen map to simulate anaerobic biodegradation at the site. Because the coefficient of anaerobic decay was set to zero, the sensitivity analysis was conducted by varying the hydraulic conductivity (and therefore transmissivity) and the coefficient of reaeration. Because of the potential for large dispersivity values at the site, a sensitivity analysis was also performed on this parameter.

To perform the sensitivity analyses, an individual run of the model was made with the same input as the calibrated model, except that one of the aforementioned parameters was varied. The models were run for 10 years so that the independent effect of each variable could be

assessed. As a result, six sensitivity runs of the calibrated model were made, with the following variations:

- 1) Hydraulic conductivity uniformly increased by a factor of 5;
- 2) Hydraulic conductivity uniformly decreased by a factor of 0.2;
- 3) Longitudinal dispersivity increased to 100;
- 4) Longitudinal dispersivity decreased to 5.34;
- 5) Reaeration coefficient increased to 0.03 day⁻¹; and
- 6) Reaeration coefficient decreased to 0.0003 day⁻¹.

The results of the sensitivity analyses are shown graphically in Figures 5.5, 5.6, and 5.7. These figures display the modeled BTEX concentrations versus distance along the centerline of the plume. This manner of displaying data is useful because the plume is narrow and maintains a constant plume migration direction parallel to the model grid. Furthermore, the figures allow easy visualization of the changes in BTEX concentration caused by varying model input parameters.

Uniformly increasing the hydraulic conductivity in the model by half an order of magnitude (model H1) drastically increased the migration rate and biodegradation rate of the plume (Figure 5.5). Plume migration and influx of fresh electron acceptors was so rapid that no appearance of BTEX concentrations was predicted by the model. This was caused by an abnormally high influx of electron acceptors in the highly conductive aquifer that immediately biodegraded existing and injected BTEX concentrations. In contrast, decreasing the hydraulic conductivity by a half-order of magnitude slowed plume migration, which in turn caused an increase in measured BTEX levels in the source area. Increased BTEX concentrations in the source area are caused by a reduction in the amount of electron acceptors being brought into contact with the plume from upgradient locations.

The ef ect of varying the coefficient of reaeration is shown in Figure 5.6. Decreases in total BTEX mass in ground water caused by increasing the reaeration coefficient from 0.003 day⁻¹ to 0.03day⁻¹ was significant, and complete biodegradation of all existing and injected

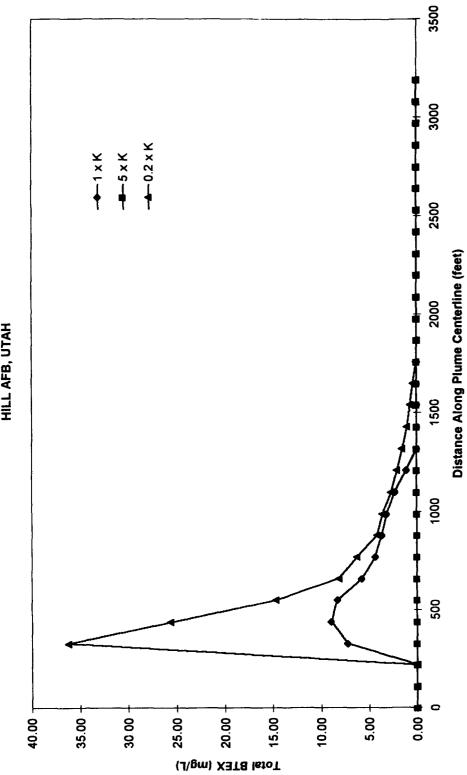
FIGURE 5.5
PLOT OF TOTAL BTEX VS DISTANCE ALONG PLUME
CENTERLINE WITH VARYING HYDRAULIC CONDUCTIVITY
UST SITE 870 INTRINSIC REMEDIATION EE/CA
HILL AFB, UTAH

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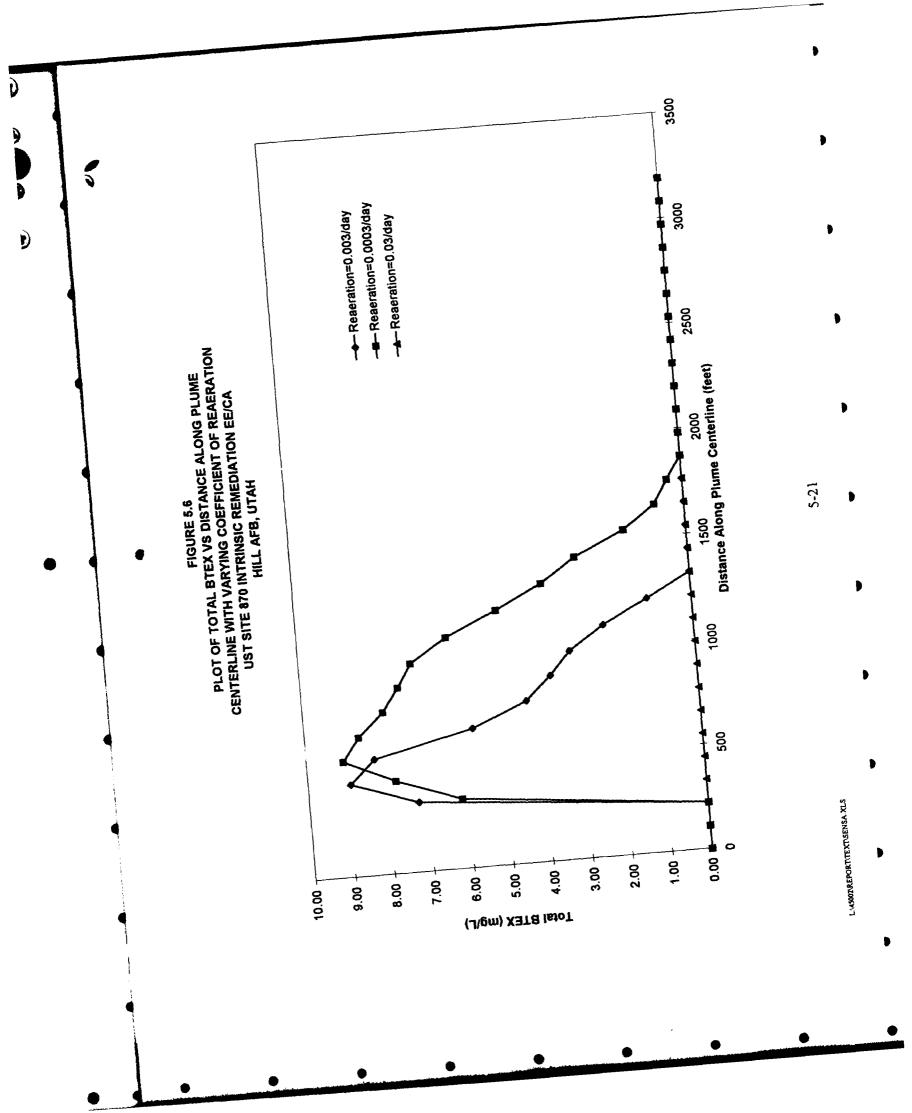
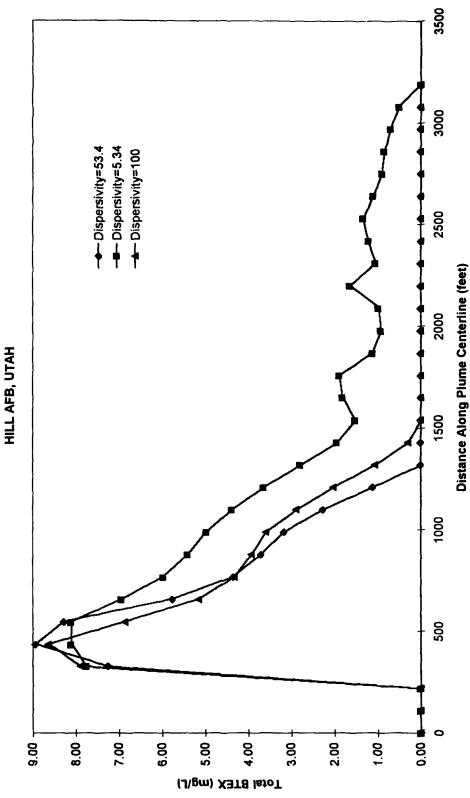


FIGURE 5.7
PLOT OF TOTAL BTEX VS DISTANCE ALONG
PLUME CENTERLINE WITH VARYING DISPERSIVITY
UST SITE 870 INTRINSIC REMEDIATION EE/CA

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5-22

BTEX occurred instantaneously. By reducing the reaeration coefficient by an order of magnitude, a more modest change in the shape of the plume occurred. The downgradient end of the plume extended approximately 500 feet past its observed location.

Figure 5.7 illustrates the effects of varying longitudinal dispersivity. Decreasing the dispersivity resulted in a larger migration distance for the BTEX plume. This occurs because lowering the dispersivity keeps the plume from spreading out into more electron acceptor-rich portions of the aquifer. Increasing the dispersivity resulted in faster dilution of BTEX in the source area; however, the migration distance of the BTEX was only slightly altered by increasing the dispersivity.

The results of the sensitivity analysis suggest that the calibrated model used for this report is reasonable. Increasing the coefficient of reaeration or the hydraulic conductivity greatly affects the predicted BTEX concentration and distribution. Lowering the values of these variables causes an abnormal lengthening of the plume to beyond reasonable distances based on observations made at the site between August 1993 and July 1994. The calibrated model appears to reasonably simulate the observed BTEX plume.

5.7 MODEL RESULTS

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The Bioplume II[®] model was run under steady-state conditions with no LNAPL removal, 5-percent annual LNAPL removal, and 15-percent annual LNAPL removal until the plume reached steady-state equilibrium (no LNAPL removal) or until the plume disappeared (LNAPL removal scenarios). The model with no LNAPL removal best simulated the current site conditions. As previously mentioned, LNAPL contamination at the site is extensive. LNAPL reduction through source removal, in concert with natural attachment unation can significantly reduce the longevity of the BTEX contamination at the site.

Although the results of each model run varied depending on the amount of LNAPL dissolution over time, two trends were consistently observed, including:

 The plume shape in each simulation is elongated because of the rapid advective transport of BTEX contamination and rapid biodegradation of BTEX at the plume periphery. This is consistent with what was observed between August 1993 and July 1994 (Figures 4.4 and 4.5); 2) A BTEX partitioning threshold develops in the two models that simulate a reduction in the LNAPL source term. In both models the hydrocarbon plume disappears when the BTEX injection concentration is reduced to approximately 55 percent of its original value. This occurs because replenished electron acceptor concentrations greatly exceed the BTEX contamination introduced into the aquifer by the prescribed biodegradation ratio of DO and DO-equivalent nitrate to BTEX of 3.1:1

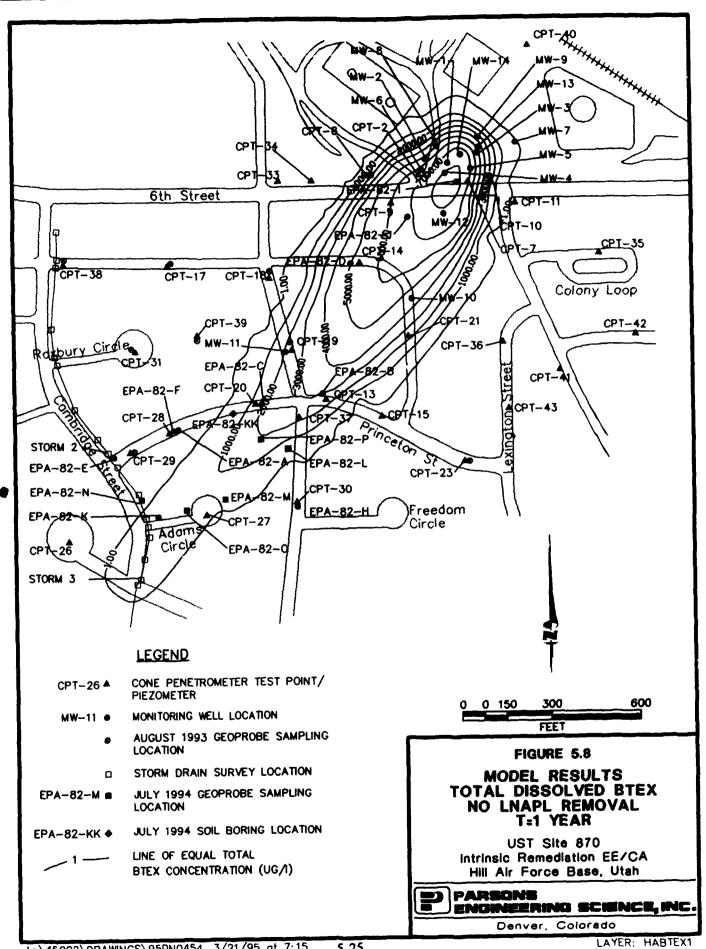
The following sections describe the results of each model scenario.

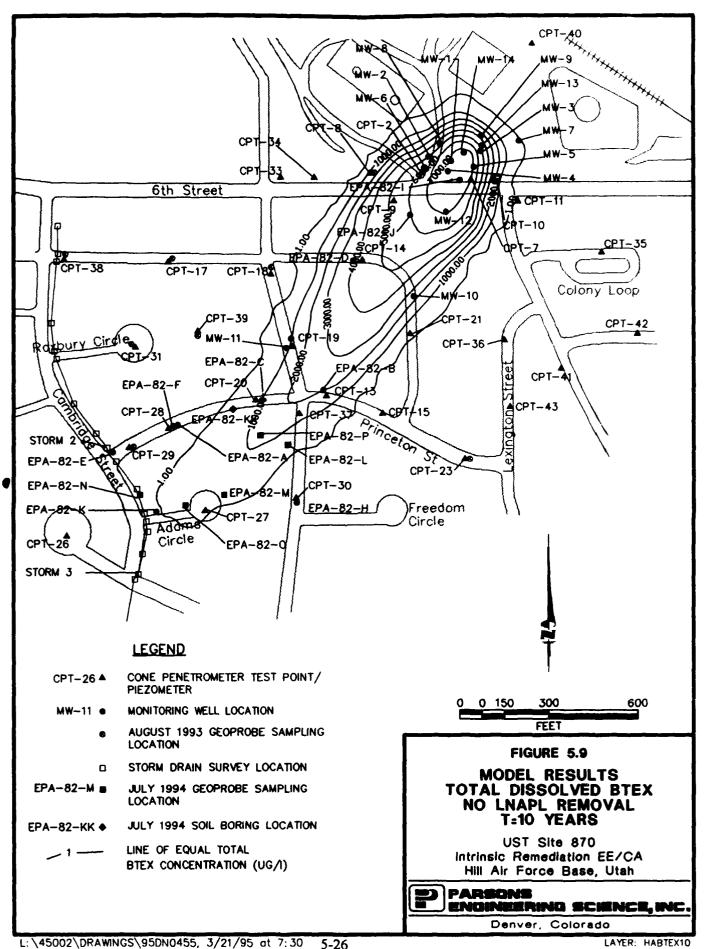
5.7.1 No Source Removal (Model Hill-A)

Model Hill-A simulated the migration and biodegradation of the BTEX plume assuming no LNAPL weathering or removal. Approximately 3,900 gm (39,000 mg or 390,000 µg) of dissolved-phase BTEX contamination existed at the start of modeling (T=0, based on data This estimate was calculated by Bioplume II, which summed all from August 1993). dissolved BTEX contamination over the Hill AFB model domain at time zero. Contaminant migration was rapid because of the high hydraulic conductivity and steep hydraulic gradient present at the site. The total BTEX plume thins in shape and stretches just past Cambridge Street after 1 year (Figure 5.8). The Bioplume II model predicted that the plume would reach steady-state equilibrium within 4 years. Figures 5.8 and 5.9 show the predicted total BTEX concentrations at years 1 and 10. The plume migrates in the expected southwest direction, and by 1 year, levels of greater than 1 µg/L of dissolved-phase BTEX are predicted to reach the vicinity of Cambridge Street in the Patriot Hills Housing complex. However, the stabilized plume (> 4 years) has slightly receded and only extends as far as the intersection of Cambridge Street and Adams Circle. The stabilized plume predicted by the model closely resembles the plume observed at the site in July 1994. Differences in modeled and actual plume shape are caused by physical, chemical, and biological variations within the shallow saturated zone that result from natural aquifer heterogeneity.

5.7.2 Five-Percent Annual Source Removal (Model Hill-B)

Model Hill-B simulated the migration and biodegradation of the BTEX plume assuming a 5-percent annual reduction in source BTEX concentrations caused by natural weathering processes and limited source removal by LNAPL skimming and bioventing. Model Hill-B is



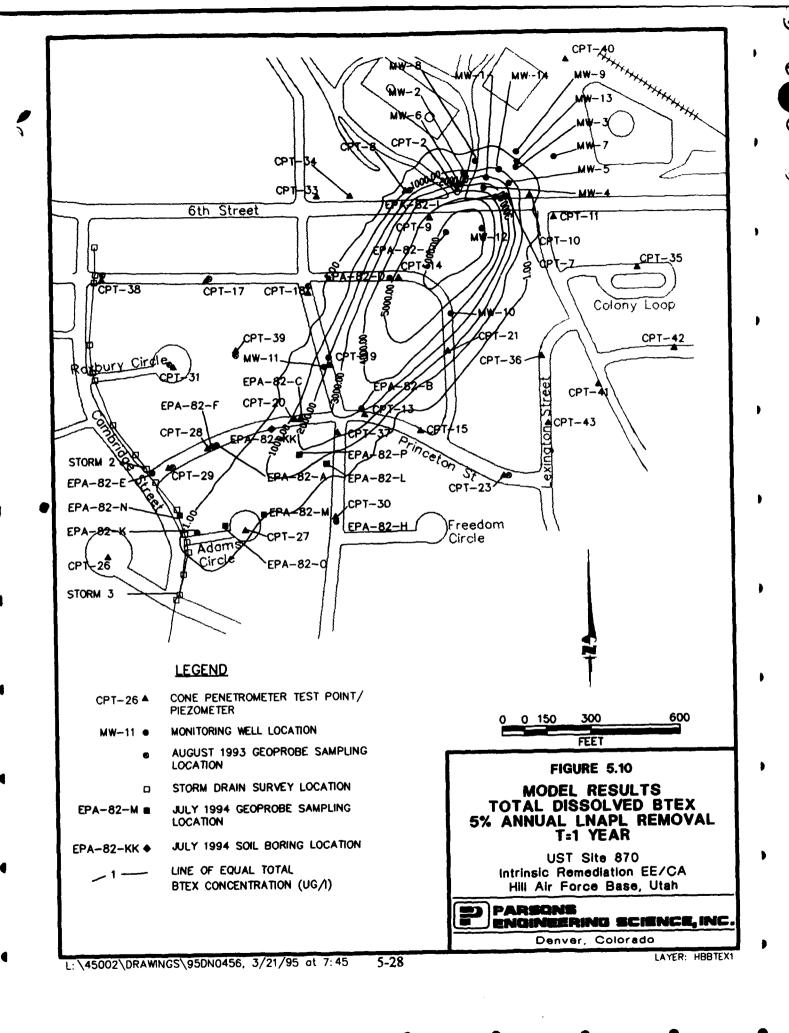


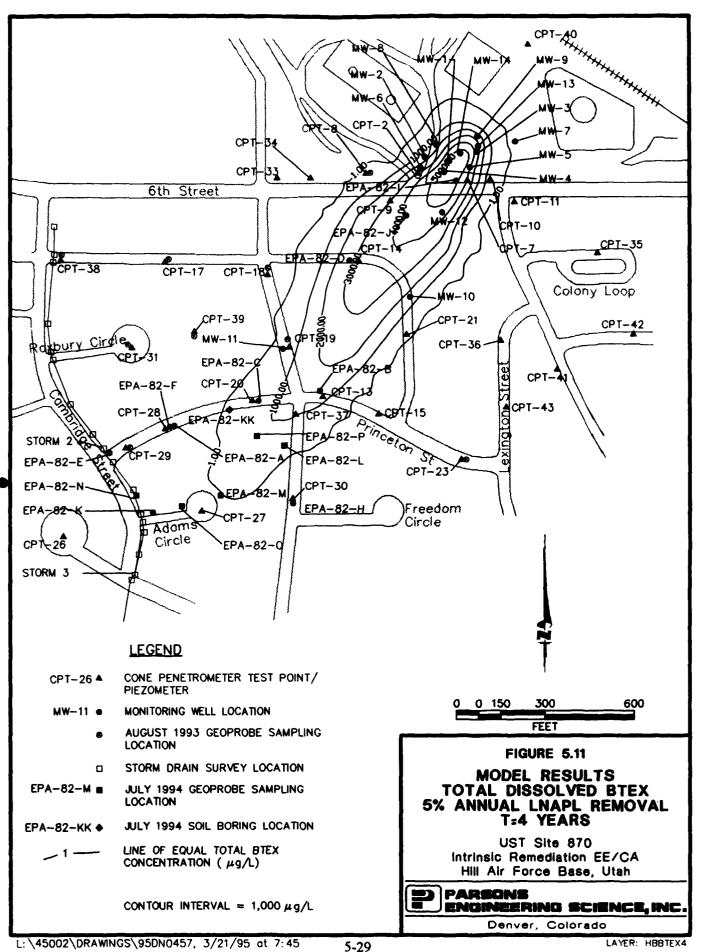
identical to model Hill-A with the exception of the 5-percent annual source removal term. Figures 5.10, 5.11, and 5.12 show the results of this model. The simulation time of the model was 25 years because 20 years were required before the LNAPL was theoretically reduced to 0 percent of its original partitioning strength. Despite the lengthy estimated period required to remove all the LNAPL contamination, BTEX disappeared in model simulations long before free-phase partitioning of BTEX from the LNAPL into the ground water ceased. The initial extent and concentration of BTEX contamination in years 1 and 2 were nearly identical to those predicted in model Hill-A. However, after 4 years the plume had noticeably receded at the periphery and the internal concentrations of BTEX were reduced by as much as 2 mg/L (2,000 µg/L). By year 7, the plume was approximately 10 percent of its original area, and the maximum concentration of BTEX was predicted to be only 300 µg/L in the source area. The reach of contamination at this point extends roughly 100 feet northwest of the intersection at Princeton Street and Liberty Road. Although BTEX partitioning was simulated for the first 19 years of the pumping period, dissolved-phase BTEX contamination was estimated to be completely degraded after 7 years. This situation is caused by the influx of electron acceptors by upgradient replenishment and reaeration that exceed the levels required to biodegraded the BTEX contamination injected into the 20 injection cells of the model grid.

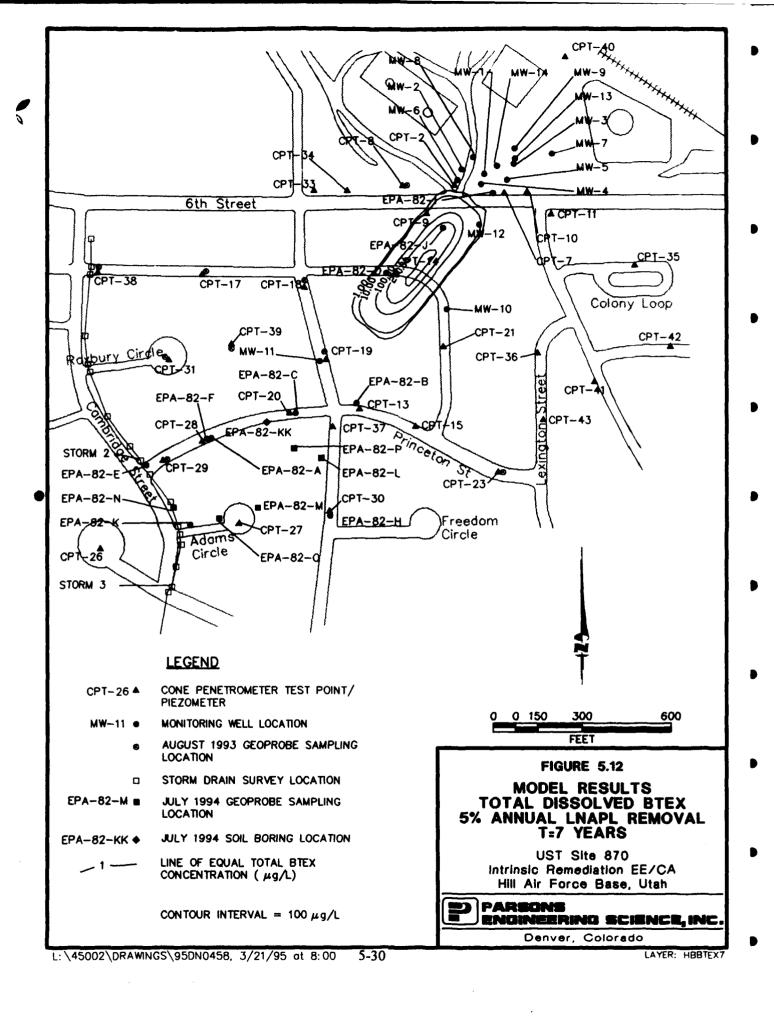
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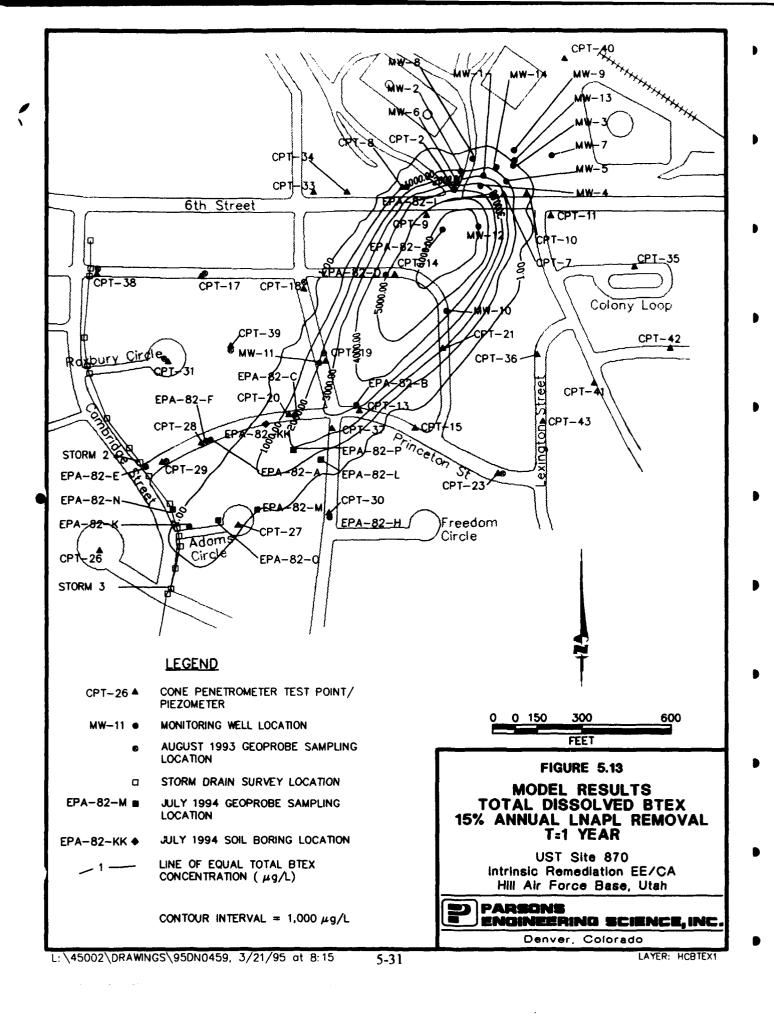
5.7.3 Fifteen-Percent Annual Source Removal (Model Hill-C)

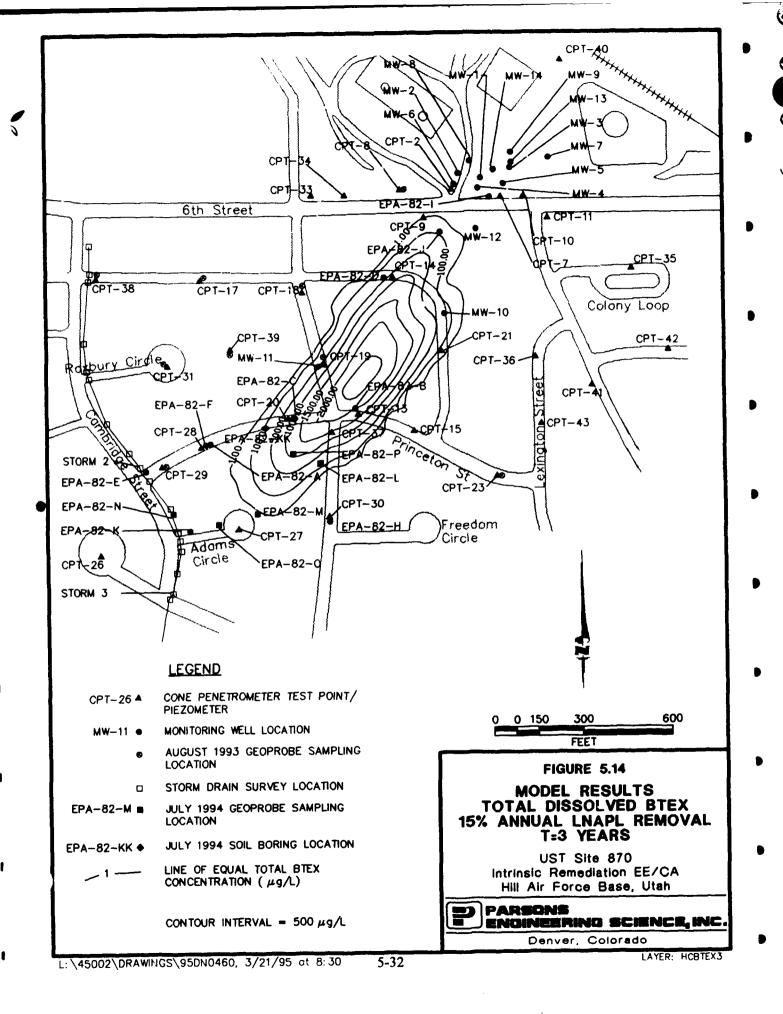
Model Hill-C simulated the migration and biodegradation of the BTEX plume assuming a 15-percent annual reduction in source BTEX concentrations caused by natural weathering processes and more active source removal by expanded LNAPL pumping and expanded bioventing. Model Hill-C is identical to model Hill-A with the exception of the 15-percent annual source removal term. Figures 5.13 and 5.14 show the results of this model for 1 and 3 years after the implementation of a 15-percent annual source removal technology. The initial 1 year prediction of plume migration suggests that the plume would extend as far as Cambridge Street at concentrations of 1 µg/L. By year 3 (Figure 5.14), the BTEX plume had undergone significant loss, including a complete reduction of BTEX contamination in the source area. By year 4, the plume had entirely disappeared. This complete plume disappearance at year 4 was caused by the injection loading rates of modeled BTEX to be reduced to 55 percent of the original loading rate, which was below the biodegradation capacity of the upgradient, influent electron acceptors and aquifer reaeration.











5.9 CONCLUSIONS

Contaminant fate and transport at UST Site 870 was simulated using the finite-difference ground water model Bioplume II. Model results suggest that BTEX contamination may possibly migrate to Cambridge Street and the stormwater sewer running parallel to this street in all models. However, model simulations conducted during this project are extremely conservative for several reasons, including:

- Aerobic respiration, denitrification, iron reduction, sulfanogenesis, and methanogenesis are all occurring at this site; however, only DO and nitrate are considered as electron acceptors during model simulations;
- 2) The stoichiometry used to determine the ratio between DO and nitrate-equivalent DO assumed that no microbial cell mass was produced during the reaction. As discussed in Section 4.3.2.1, this approach may be too conservative by a factor of three.
- 3) The highest DO concentration observed at the site was 6.3 mg/L. The highest DO concentration assumed during model simulations was 5.0 mg/L. In addition, the highest observed nitrate concentration observed at the site was 17 mg/L. The highest nitrate concentration assumed during model simulations was 10 mg/L. This nitrate concentration came only from upgradient, constant head cells; the majority of the area outside the plume was assumed to have nitrate concentrations of only 5 mg/L.
- 4) The lowest coefficient of retardation for benzene (1.29) was used for model simulations. Coefficient of retardation values for the other BTEX compounds range from 1.7 to 3.35. The use of the low coefficient of retardation tends to increase the distance traveled by the simulated BTEX plume, but provides a more accurate estimate of benzene transport.

The results of the Bioplume II modeling effort were used to help develop and compare ground water remedial options. This comparative analysis of remedial options is presented in Section 6.

SECTION 6

COMPARATIVE ANALYSIS OF REMEDIAL ALTERNATIVES

This section presents the development and comparative analysis of three ground water remedial alternatives for UST Site 870 at Hill AFB. The intent of this evaluation is to determine if intrinsic remediation is an appropriate and cost-effective remedial technology to consider when developing final remedial strategies for UST Site 870, especially when combined with other innovative and conventional remedial technologies.

Section 6.1 presents the evaluation criteria to be used to evaluate ground water remedial alternatives. Section 6.2 discusses the development of remedial alternatives to be considered as part of this demonstration project. Section 6.3 provides a brief description of each of these remedial alternatives. Section 6.4 provides a more detailed analysis of the remedial alternatives using the defined remedial alternative evaluation criteria. The results of this evaluation process are summarized in Section 6.5.

6.1 REMEDIAL ALTERNATIVE EVALUATION CRITERIA

The evaluation criteria used to identify the most appropriate remedial alternative for shallow ground water contamination at UST Site 870 were adapted from those recommended by the USEPA for selecting remedies for Superfund sites (OSWER Directive 9902.3). These criteria included (1) long-term effectiveness and permanence, (2) technical and administrative implementability, and (3) relative cost. The following sections briefly describe the scope and purpose of each evaluation criterion. This report does not include a complete discussion of applicable or relevant and appropriate requirements (ARARs) for the site. Rather, this report focuses on the potential use of intrinsic remediation and source reduction technologies to reduce BTEX concentrations within the shallow ground water to levels that pose an acceptable risk to human health or the environment.

6.1.1 Long-Term Effectiveness and Permanence

Each remedial technology or remedial alternative (which can be a combination of remedial technologies such as intrinsic remediation and institutional controls) is analyzed to determine

how effectively it will minimize ground water plume expansion so that ground water quality standards can be achieved at a downgradient POC. The expected technical effectiveness based on case histories from Hill AFB sites and other sites with similar conditions is also evaluated. The ability to minimize potential impacts to surrounding facilities and operations is considered. The ability of each remedial alternative to protect both current and potential future receptors from potential risks associated with site-related contamination in shallow ground water is qualitatively assessed by conservatively estimating if a potential exposure pathway involving ground water could be completed, either now or in the future. This evaluation criterion also included permanence and the ability to reduce contaminant mass, toxicity, and volume. Time to implement the ability to reduce contaminant mass, toxicity, and volume. Time to implement the ability to reduce contaminant mass, toxicity, and volume. Time to implement the ability to reduce contaminant mass, toxicity, and volume. Time to implement the ability to reduce contaminant mass, toxicity, and volume to implement the ability to reduce contaminant mass, toxicity, and volume to implement the ability to reduce contaminant mass, toxicity, and volume to implement the ability to reduce contaminant mass, toxicity, and volume to implement the ability to reduce contaminant mass, toxicity, and volume to implement the ability to reduce the factor of the technology and the potential threats resulting from such a failure, is also presented.

6.1.2 Implementability

The technical implementation of each remedial technology or remedial alternative was evaluated in terms of technical feasibility and availability. Potential shortcomings and difficulties in construction, operations, and monitoring are presented and weighed against perceived benefits. Requirements for any post-implementation site control, such as long-term monitoring and land use restrictions, are described. Details on administrative feasibility in terms of the likelihood of public acceptance and the ability to obtain necessary approvals is discussed.

6.1.3 Cost

The total cost (present worth) of each remedial alternative was estimated for relative comparison. An estimate of capital costs, and operating and post-implementation costs for site monitoring and land use controls is included. An annual inflation factor of 5 percent was applied in calculating the present value of operation, maintenance, and monitoring costs.

6.2 FACTORS INFLUENCING ALTERNATIVES DEVELOPMENT

Several factors were considered during the identification and screening of remedial technologies for addressing shallow ground water contamination at UST Site 870. Factors considered included the objectives of the natural attenuation demonstration program; contaminant, ground water and soil properties; present and future land use; and potential

exposure pathways. This section briefly describes each of these factors and how they were used to narrow the list of potentially applicable remedial technologies to the final remedial alternatives considered for UST Site 870.

6.2.1 Program Objectives

The intent of the Natural Attenuation (Intrinsic Remediation) Demonstration Program sponsored by AFCEE is to develop a systematic process for scientifically investigating and documenting naturally occurring subsurface attenuation processes that can be factored into overall site remediation plans. The objective of this program and the specific UST Site 870 study is to provide solid evidence of intrinsic remediation of dissolved-phase fuel hydrocarbon so that this information can be used to develop an effective ground water remediation strategy. A secondary goal of this multi-site initiative is to provide a series of regional case studies which demonstrate that natural processes of contaminant degradation can often reduce contaminant concentrations in ground water to below acceptable cleanup standards before completion of potential exposure pathways.

Because the objective of this program is to study natural processes in the saturated zone rather than in all contaminated media (e.g., unsaturated soil, or soil gas), technologies have been evaluated based on their potential impact on shallow ground water and phreatic soils. Technologies that can reduce vadose zone contamination and partitioning of contaminants into ground water have also been evaluated. Many of the source removal technologies evaluated in this section will also reduce soil and soil gas contamination, but it is important to emphasize that the remedial alternatives developed in this document are not intended to remediate all contaminated media. Additional program objectives set forth by AFCEE include cost-effectiveness and minimization of waste. Technologies that may meet these criteria include institutional controls, soil vapor extraction, bioventing, mobile LNAPL removal, biosparging, ground water extraction and treatment (air stripping), and intrinsic remediation. Soil excavation, slurry walls, sheet piling, carbon adsorption, ex situ biological or chemical treatment, and onsite/offsite disposal are not attractive technology candidates for this site.

6.2.2 Contaminant Properties

The site-related contaminants targeted as part of this demonstration at UST Site 870 are the BTEX compounds. The source of this contamination is weathered JP-4 jet fuel present as residual LNAPL in capillary fringe soil and as mobile LNAPL floating on the ground water surface within the source area of UST Site 870. The physiochemical characteristics of both

JP-4 and the individual BTEX compounds will greatly influence the effectiveness and selection of a remedial technology.

Petroleum hydrocarbon mixtures, such as JP-4 jet fuel, are comprised of over 300 compounds with different physiochemical characteristics. JP-4 is classified as a LNAPL with a liquid density of approximately 0.75 grams per milliliter (g/mL) at 20°C. Many compounds within JP-4 sorb very well to soil and are concentrated in the capillary fringe because the mixture is less dense than water. JP-4 is slightly soluble in water, with a maximum solubility of approximately 300 mg/L. JP-4 is also a primary substrate for biological metabolism. Simultaneous biodegradation of aliphatic, aromatic, and alicyclic hydrocarbons has been observed. In fact, mineralization rates of hydrocarbons in mixtures, such as JP-4, may be faster than mineralization of the individual constituents as a result of co-metabolic pathways (Jamison et al., 1976; Perry, 1984).

The BTEX compounds are generally volatile, highly soluble in water, and adsorb less strongly to soil. These characteristics allow the BTEX compounds to leach more rapidly from contaminated soil into ground water and migrate as dissolved-phase contamination (Lyman et al., 1992). All of the BTEX compounds are highly amenable to in situ degradation by both biotic and abiotic mechanisms.

Benzene is very volatile, with a vapor pressure of 76 millimeters of mercury (mm Hg) at 20°C and a Henry's Law Constant of approximately 0.0054 atmosphere-cubic meter/mole (atm-m³/mole) at 25°C (Hine and Mookerjee, 1975; Jury et al., 1984). The solubility of benzene in water at 20°C has been reported to be 1,780 mg/L (Verschueren, 1983). Benzene is normally biodegraded to carbon dioxide with catechol as a short-lived intermediate (Hopper, 1978; Ribbons and Eaton, 1992).

Toluene is also volatile, with a vapor pressure of 22 mm Hg at 20°C and a Henry's Law Constant of about 0.0067 atm-m³/mole at 25°C (Pankow and Rosen, 1988; Hine and Mookerjee, 1975). Toluene sorbs more readily to soil media relative to benzene, but is still very mobile. The solubility of toluene in water at 20°C is approximately 515 mg/L at 20°C (Verschueren, 1983). Toluene has been shown to degrade to pyruvate, caetal dehyde, and completely to carbon dioxide via the intermediate catechol (Hopper, 1978; Wilson et al., 1986; Ribbons and Eaton, 1992).

Ethylbenzene has a vapor pressure of 7 mm Hg at 20°C and a Henry's Law Constant of 0.0066 atm-m3/mole (Pankow and Rosen, 1988; Valsaraj, 1988). Ethylbenzene sorbs more

strongly to soils than benzene but less strongly than toluene (Abdul et al., 1987). Ethylbenzene is also less soluble than benzene and toluene in water at 152 mg/L at 20°C (Verschueren, 1983; Miller et al., 1985). Ethylbenzene ultimately degrades to carbon dioxide via its intermediate 3-ethylcatechol (Hopper, 1978; Ribbons and Eaton, 1992).

The three xylene isomers have vapor pressures ranging from 7 to 9 mm Hg at 20°C and Henry's Law Constants of between 0.005 and 0.007 atm-m³/mole at 25°C (Mackay and Wolkoff, 1973; Hine and Mookerjee, 1975; Pankow and Rosen, 1988). Of all of the BTEX compounds, xylenes sorb most strongly to soil, but still can leach from soil into the ground water (Abdul et al., 1987). Xylenes have water solubilities of 152 to 160 mg/L at 20°C (Bohon and Claussen, 1951; Mackay and Shiu, 1981; Isnard and Lambert, 1988). Xylenes can degrade to carbon dioxide via pyruvate carbonyl intermediates (Hopper, 1978; Ribbons and Eaton, 1992).

Based on these physiochemical characteristics, intrinsic remediation, soil vapor extraction, bioventing, biosparging, ground water extraction, and air stripping technologies could all be effective at destroying, collecting, and treating BTEX contaminants at UST Site 870.

6.2.3 Site-Specific Conditions

Two general categories of site-specific characteristics were considered in identifying remedial technologies to comparatively evaluate as part of this demonstration project. The first category considered was physical characteristics such as ground water depth, gradient, and flow direction, and soil type, and their influence on the types of remedial technologies most appropriate for the site. The second category involved assumptions about future land use and potential exposure pathways. Each of these site-specific characteristics have influenced the selection of remedial alternatives included in the comparative evaluation.

6.2.3.1 Ground Water and Soil Characteristics

Site geology and hydrogeology will have a profound effect on the transport of contaminants and the effectiveness and scope of required remedial technologies at a site. Hydraulic conductivity is perhaps the most important aquifer parameter governing ground water flow and contaminant transport in the subsurface. The velocity of the ground water and dissolved-phase contamination is directly related to the hydraulic conductivity of the saturated zone. Rising-head slug tests completed at UST Site 870 indicate a relatively high hydraulic conductivity within and downgradient of the source area and dissolved-phase BTEX plume. Estimated values ranged from 1.67×10^{-2} to 8.31×10^{-3} cm/s. These high values are

characteristic of sandy materials (see Sections 4 and 5 of this report). The high hydraulic conductivity of shallow sediments at this site directly influences the fate and transport of contaminants. The shallow ground water plume has migrated rapidly, increasing the areal extent of contamination (i.e., plume expansion) but decreasing the average concentration within the aquifer via dilution and increased biodegradation.

Although high hydraulic conductivity can result in plume expansion and migration, this same characteristic will also enhance the effectiveness of other remedial technologies, such as ground water extraction, biosparging, and intrinsic remediation. For example, it should be less expensive and time-consuming to capture and treat the contaminant plume using a network of extraction wells in areas of high hydraulic conductivity than to implement this technology in aquifers with low hydraulic conductivity. Contaminant recovery may also be maximized when contaminants are not significantly sorbed and retarded by phreatic soil. The relatively low TOC content of Hill AFB aquifer materials (<0.094 percent) should tend to minimize sorption and increase the mobility of all BTEX compounds. The effectiveness of biosparging may also be increased in highly conductive aquifers because of reduced entry pressures and increased sparging well radius of influence. Greater hydraulic conductivity also increases the amount of contaminant mass traveling through the biosparging network. The DO introduced by biosparging can also be utilized effectively to aerobically biodegrade the dissolved contaminant mass.

The rapid movement of contaminants within the subsurface away from the source will also increase the effectiveness of natural biodegradation processes by distributing the contaminant mass into areas enriched with electron acceptors. To satisfy the requirements of indigenous microbial activity and intrinsic remediation, the aquifer must provide an adequate and available carbon or energy source, electron acceptors, essential nutrients, proper ranges of pH, temperature, alkalinity, salinity, and redox potential.

Data collected as part of the field work phase of this demonstration project and described in Sections 3 and 4 of this document, indicate that UST Site 870 is characterized by an adequate and available carbon/energy source, electron acceptors, and essential nutrients to support measurable biodegradation of JP-4 contamination by indigenous microorganisms. Both DO and nitrate represent significant sources of electron acceptor capacity for the biodegradation of BTEX compounds in ground water at the site. Further, because fuel-hydrocarbon-degrading microorganisms have been known to thrive under a wide range of temperature and pH conditions (Freeze and Cherry, 1979), the physical and chemical

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conditions of the ground water and phreatic soil at UST Site 870 are not likely to inhibit microorganism growth.

Fuel hydrocarbon-degrading microorganisms are ubiquitous, and as many as 28 hydrocarbon-degrading isolates (bacteria and fungi) have been discovered in different soil environments (Davies and Westlake, 1977; Jones and Eddington, 1968). Indigenous microorganisms have a distinct advantage over microorganisms injected into the subsurface to enhance biodegradation as indigenous microorganisms are well adapted to the physical and chemical conditions of the subsurface in which they reside (Goldestein et al., 1985). Microbe addition was not considered a viable remedial technology for UST Site 870.

6.2.3.2 Potential Exposure Pathways

An exposure assessment identifies the potential human and ecological receptors that could potentially come into contact with site-related contamination and the pathways through which these receptors might be exposed. To have a complete exposure pathway, there must be a source of contamination, a potential mechanism(s) of release, a pathway of transport to an exposure point, an exposure point, and a receptor. If any of these elements do not exist, the exposure pathway is considered incomplete, and receptors cannot come into contact with site-related contamination. Evaluation of the potential long-term effectiveness of any remedial technology or remedial alternative as part of this demonstration project includes determining if the approach will be sufficient and adequate to minimize plume expansion so that potential exposure pathways involving shallow ground water are incomplete.

Assumptions about current and future land use at a site form the basis for identifying potential receptors, potential exposure pathways, reasonable exposure scenarios, and appropriate remediation goals. USEPA (1991) advises that the land use associated with the highest (most conservative) potential level of exposure and risk that can reasonably be expected to occur should be used to guide the identification of potential exposure pathways and to determine the level to which the site must be remediated. The source area consists of an industrial fuel storage and office facilities associated with mission support services. Warehouses, offices, and other large structures are located to the east and west of UST Site 870. A portion of the Patriot Hills Base Housing Area is located to the south and southwest of the source area. The ground water plume originating from UST Site 870 is migrating to the southwest, and has impacted shallow ground water underlying this residential area. Hill AFB elementary school is located immediately southwest of the housing area on the base's

southwestern property boundary. Thus, the current land use within and downgradient of the contaminant plume is both industrial and residential.

Under reasonable current land use assumptions, potential receptors include both worker and residential populations. It is unlikely that workers could be exposed to site-related contamination in phreatic soils or shallow ground water unless this material was removed during future construction, excavations or remedial activities. Utility workers could be exposed to shallow ground water contamination if the plume migrates to and discharges into the storm drain located along Cambridge Street. Shallow ground water is not currently used to meet industrial demands at Hill AFB. All onbase water demands are met by deep supply wells and/or from water piped in from the nearby Weber Basin Water Conservancy District. Exposure pathways involving other environmental media such as shallow soils and soil gas in the source area were not considered as part of this project, but should be considered in overall site remediation decisions.

Because of the depth of ground water (>5 feet), current residents should not be exposed to site-related contamination in ground water and phreatic soil under normal exposure conditions appropriate for the site. The most conservative exposure assumption involving ground water would involve uncontrolled or domestic use of ground water as a potable water supply. Although this exposure scenario can be an important consideration in deciding whether or not to take action at a site, it is not reasonable under current land use conditions. As noted previously, shallow ground water is not used to meet domestic potable water demands at Hill AFB at this time. Hill ArB officials could apply land use restrictions or institutional controls in the residential area to prevent residential use of ground water. It is possible that residents could be directly exposed to shallow ground water contamination at the storm drain located along Cambridge Street as ground water may surface at this location. Potential current exposure pathways involving other environmental media such as soil gas beneath residential units were not considered as part of this demonstration. Other studies have addressed the potential of soil gas and have determined that pathways to residential areas are incomplete.

Assumptions about hypothetical future land uses must also be made to ensure that the remedial technology or alternative considered for shallow ground water at the site is adequate and sufficient to provide long-term protection. No changes in land use are anticipated in the foreseeable future. Use of the residential land use assumption is the most conservative (health-protective). Thus, potential future receptors include both worker and residential populations. The potential future exposure pathways involving workers are identical to those under current conditions provided shallow ground water is not used to meet industrial water

demands. The potential future exposure pathways involving residents will also be identical to current conditions if Hill AFB can effectively restrict shallow ground water use in all areas potentially affected by contamination from UST Site 870. In summary, the use of the intrinsic remediation technology at this site will require that the source area be maintained as industrial property and that restrictions on ground water use be enforced in areas downgradient of UST Site 870 to the Cambridge Street stormwater drain. If source removal technologies such as soil vapor extraction, bioventing, mobile LNAPL recovery, biosparging, or ground water pump and treat are implemented, or expanded, they will also impact the short- and long-term land use options and will require some level of institutional control during and following remediation.

6.2.3.3 Remediation Goals for Shallow Ground Water

The stormwater drain located along Cambridge Street has been identified as the point of compliance (POC) for ground water remedial activities because this appears to be the most likely point of exposure for migrating contamination to impact human or ecological receptors. Migration to and discharge of contaminated shallow ground water into the stormwater system could complete an exposure pathway to human or ecological receptors via dermal contact or possible ingestion. The stormwater drain outfall into Pond 5 is an accessible and well-defined location for monitoring and for demonstrating compliance with protective ground water quality standards, such as federal MCLs.

This remedial strategy would be consistent with remediation requirements set forth by the State of Utah. The State recognizes that compliance with promulgated, single-point remediation goals is not necessary if site-related contamination does not pose a threat to human health or the environment (i.e., the exposure pathway is incomplete). Thus, the magnitude of required remediation in areas that can and will be placed under institutional control is different from the remediation that is required in areas that may be available for unrestricted use. This means that viable remedial alternatives, which includes long-term restrictions on shallow ground water use, must be able to achieve concentrations that minimize plume migration and expansion and potential human risk associated with ground water contact. The remediation goal for shallow ground water impacting the Cambridge Street stormwater drain is attainment of federal MCLs for each of the BTEX compounds, as listed in Table 6.1. Although it is unlikely that stormwater would be ingested by humans, this level of long-term protection is appropriate for a residential area.

TABLE 6.1

POINT-OF-COMPLIANCE REMEDIATION GOALS
UST SITE 870 INTRINSIC REMEDIATION EE/CA
HILL AFB, UTAH

Compound	Federal MCLs (μg/L)
Benzene	5
Toluene	1,000
Ethylbenzene	700
Total Xylenes	10,000

In summary, available data indicate that no potential exposure pathway involving shallow ground water is complete under current conditions, with the exception of soil gas emanating from the ground water to within 4 feet of the surface. The exposure route for soil gas was identified in a vapor exposure assessment performed in other site characterization studies (Gemperline, written communication, 1995). Although an exposure pathway to the surface is completed from BTEX contamination volatilizing from ground water, human risk was calculated to be inconsequential. Other than soil gas, no potential exposure pathway involving shallow ground water will be complete under future land use assumptions provided use of ground water as a potable or industrial source of water is prohibited by institutional controls within and downgradient of the source area to the Cambridge Street stormwater drain. Thus, institutional controls are likely to be a necessary component of any ground water remediation strategy for this site. The required duration of these institutional controls may vary depending on the effectiveness of any remedial technology at reducing contaminant mass and concentrations in the ground water. If Federal MCLs are exceeded in the Cambridge Street stormwater discharge, remediation of stormwater will be required to prevent pathway completion.

6.2.4 Summary of Remedial Technology Screening

Several remedial technologies were identified and screened for use in reducing the source of BTEX and for treating the shallow ground water at UST Site 870. Table 6.2 identifies the initial remedial technologies considered for this demonstration and those retained for more detailed analysis. Screening was conducted systematically by considering the objectives of the AFCEE intrinsic remediation demonstration, the physiochemical properties of BTEX compounds, and other site-specific characteristics such as hydrology, land use assumptions,

TABLE 6.2

TECHNOLOGIES AND PROCESS OPTIONS FOR GROUND WATER REMEDIATION UST SITE 870 INTRINSIC REMEDIATION EE/CA INITIAL TECHNICAL IMPLEMENTABILITY SCREENING OF HILL AFB, UTAH

Response	recumonogy	Process Option	Implementability	Retain
	Type			
Action				
Long-Term F	Periodic	Confirmation	Many existing wells are available to confirm the progress of	Yes
Monitoring	Ground Water	Wells	remediation.	
	Monitoring	Point-of-	Sufficient distance exists between the plume and point-of-	Yes
		Compliance Wells	compliance to locate several wells.	
Institutional (Ground Water	Land Use	Plume area is currently within the base boundary and land-use	Yes
Controls	Use Control	Control/Regulate	and ground water use are under base jurisdiction.	
		Well Permits		
_		Seal/Abandon	No production wells are known to exist in the existing or	No
		Existing Wells	predicted plume area.	
		Point-of-Use	No ground water is extracted from the plume area for any use.	No
		Treatment		
	Public	Meetings/	Base public relations and environmental management offices	Yes
	Education	Newsletters	have many information avenues to inform workers and residents.	
Containment of I	Hydraulic	Passive Drain	Existing stormwater drain near Cambridge Street partially	Yes
Plume	Controls	Collection	intercepts ground water. Drain could be expanded.	
		Minimum	A line or semicircle of vertical pumping wells could be located	Yes
		Pumping/Gradient	along the leading edge of plume to intercept and halt the	
		Control	advance of the plume.	
1	Physical	Slurry	Requires significant disruption of a residential area.	S.
	Controls	Walls/Grout		
		Curtains		
		Sheet Piling	Requires significant disruption of a residential area	S S
1	Reactive/Semi-	Biologically	Natural biodegradation of BTEX compounds can be stimulated	Yes
	Permeable	Active Zones	by allowing contaminated ground water to flow through an	
	Barriers		aquifer zone which has enhanced oxygen and nutrient	
			conditions.	

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TABLE 6.2 (Continued)

TECHNOLOGIES AND PROCESS OPTIONS FOR GROUND WATER REMEDIATION INITIAL TECHNICAL IMPLEMENTABILITY SCREENING OF UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

General Response Action	Technology Type	Process Option	Implementability	Retain
<i>In Situ</i> Treatment	Biological	Oxygen and Nutrient Enhanced Biodegradation	Differs from biologically active zone in that oxygen and nutrients are injected upgradient of plume and allowed to migrate downgradient. In theory, this method can more rapidly reduce higher BTEX concentrations in and immediately downgradient of the source area.	Yes
	Chemical/ Physical	Intrinsic Remediation	ig ig	Yes
		Air Sparging (Volatilization)	Injection of air into contaminated aquifer creating a mass transfer of BTEX into air bubbles and into vadose zone. Limited radius of influence and short-circuiting are common problems.	No No
Aboveground Ground Water Treatment	Ground Water Extraction	Vertical Pumping Wells	Entire ground water plume is pumped by installing numerous wells with submersible pumps. High cost and major disruption to residential area.	No
		Downgradient Horizontal Drains	See Passive Drain Collection.	Yes
	Biological	Bioreactors	High flow rates require excessive retention times and large reactors. BTEX is often volatilized in these systems.	No No
	Chemical/ Physical	Air Stripping	Cost-effective technology for removing varying concentrations of BTEX at higher flow rates. Potential permitting for air emissions	Yes
		Activated Carbon	Cost prohibitive for more concentrated BTEX. Creates a carbon disposal problem.	No
		UV/Ozone Reactors	High flow rates require excessive retention times and large, expensive reactors.	No

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TABLE 6.7 (Continued)

TECHNOLOGIES AND PROCESS OPTIONS FOR GROUND WATER REMEDIATION UST SITE 870 INTRINSIC REMEDIATION EE/CAHILL AFB, UTAH INITIAL TECHNICAL IMPLEMENTABILITY SCREENING OF

General	Technology Type	Process	Implementability	Retain
Response	3	Option		
Aboveoround	Direct Discharge		Viable ortion when an WWTD is assistable and assistant of the Vi	7.5
Treatment	to Indicate Discussing		Tradic Option when an IV WILL is available and capable of handing	ជ
1 reatment	to industrial		BIEA and nydraulic loading.	
	Waste Water			
	Treatment Plant			
	(IWWTP)			
Treated Ground	Discharge to	IWWTP	Viable option when access to industrial sewer exists and hydraulic	Yes
Water Disposal	IWWTP or		loading is acceptable.	
	Sanitary Sewer	7		
		Sanitary Sewer	Viable option when access to sanitary sewer exists and hydraulic	Yes
			loading is acceptable.	
	Treated Ground	Vertical	Not recommended due to clogging and high maintenance.	No
	Water Reinjection	Injection Wells		
		Injection	Less clogging than wells but still require large trenches and can be	Yes
		Trenches	subject to injection well permitting.	
	Discharge to	Storm Drains	Viable option but generally requires NPDES or other discharge	Yes
	Surface Waters		permit.	
Source	Mobile LNAPL	Dual-Pump	Best suited for sites with >1 foot mobile LNAPL where aboveground	No
Removal/Soil	Recovery	Systems	ground water treatment already exists	
Remediation				
		Skimmer	Best suited for sites with <1 foot mobile LNAPL where ground water	Yes
		Pumps/Bailers/	pumping is undesirable.	
		Wicks		
		Total Fluids	Best suited for sites with thin saturated zones where excessive ground	Yes
		Pumping	water will not be pumped.	
		Bioslurping	Combined vapor extraction, bioventing, and mobile LNAPL recovery	Yes
			system has been operated at the site with limited success.	
	Excavation/	Biological	Deep excavation is not feasible at this site due to surface structures.	ž
	Treatment	Landfarming		

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TABLE 6.2 (Concluded)

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TECHNOLOGIES AND PROCESS OPTIONS FOR GROUND WATER REMEDIATION UST SITE 870 INTRINSIC REMEDIATION EE/CA INITIAL TECHNICAL IMPLEMENTABILITY SCREENING OF

HILL AFB, UTAH

General Response Action	Technology Type	Process Option	Implementability	Retain
	Excavation/	Thermal	Deep excavation is not feasiely at this site due to surface No	No
	Treatment	Desorption	structures.	
	(cont'd)			
	In Situ	Bioventing	Air injection to stimulate biodegradation of fuel residuals. Yes	Yes
			System currently operating in source area.	
		Soil Vapor	Vapor extraction has been successfully implemented at other Hill Yes	Yes
		Extraction	AFB sites. Requires expensive off-gas treatment.	

potential exposure pathways, and appropriate remediation goals. All of these factors will influence the technical effectiveness, implementation, and relative cost of technologies for remediating shallow ground water underlying and migrating from the site.

The general response actions retained for consideration in the development of remedial alternatives include long-term monitoring institutional controls, in situ treatment (intrinsic remediation), plume containment, bioventing, soil vapor extraction, mobile LNAPL removal and ground water collection and aboveground treatment (air stripping) and ground water disposal in the base industrial waste water treatment plant (IWTP).

6.3 BRIEF DESCRIPTION OF REMEDIAL ALTERNATIVES

This section describes how remedial technologies retained from the screening process were combined into three remedial alternatives for UST Site 870. Sufficient information on each remedial alternative has been provided to facilitate a comparative analysis of effectiveness, implementability, and cost in Section 6.4.

6.3.1 Alternative 1 - Continued Mobile LNAPL Removal and Bioventing in Source Area, Intrinsic Remediation, Institutional Controls with Long-Term Monitoring

Mobile LNAPL recovery operations have been underway at UST Site 870 for over 1 year. To date, approximately 700 gallons of JP-4 have been recovered from one skimmer pump and 5 to 7 wells with sorbent wicks located in the source area. Limited bioventing is also underway in the source area. A two-well bioventing system is currently injecting air into the subsurface and providing oxygen to approximately 15,000 cubic yards of the most contaminated vadose soils. Under this alternative, existing mobile LNAPL removal and bioventing activities would be continued, but no additional source removal technologies would be employed. Because the area of remediation under this alternative is limited to soils north of Sixth Street and because LNAPL recovery is a slow process, it is estimated that a 5-percent annual reduction in source BTEX will occur with this alternative.

Intrinsic remediation is achieved when naturally occurring attenuation mechanisms bring about a reduction in the total mass of a contaminant in the soil or dissolved in ground water. Intrinsic remediation results from the integration of several subsurface attenuation mechanisms that are classified as either destructive or nondestructive. Destructive attenuation mechanisms include biodegradation, abiotic oxidation, and hydrolysis. Nondestructive attenuation mechanisms include sorption, dilution (caused by dispersion and infiltration), and volatilization. In some cases, intrinsic remediation will reduce dissolved-phase contaminant

concentrations below numerical concentration goals, thus protecting human health and the environment. Based on the existing evidence of intrinsic remediation described in Sections 4 and 5, these processes are occurring and will continue to reduce contaminant mass as the plume advances. Figures 5.9, 5.10, and 5.11 illustrate the projected BTEX plume migration and concentration reductions that should take place when 5 percent of the BTEX source is removed each year through limited mobile LNAPL recovery and bioventing. Based on model predictions, the BTEX plume will approach the Cambridge Street storm drain in approximately 1 to 4 years at concentrations exceeding 1 µg/L. During years 4 through 7, the Bioplume II model predicts that the combination of source reductions and intrinsic remediation within the BTEX plume will significantly reduce its size and concentration.

A 5-percent annual LNAPL recovery/reduction was selected as a reasonable removal rate of BTEX concentrations emanating from mobile LNAPL at the site. A 5-percent annual BTEX source recovery/reduction could accomplish this. The most important physical processes contributing to BTEX source weathering are volatilization and dissolution. The dissolution of BTEX compounds from LNAPL is accomplished through interfacial dissolution at the fuel/water interface and dissolution into precipitation that is percolating downward."

The 5-percent annual BTEX loss was selected for comparison purposes only, and is not intended to reflect an actual rate of BTEX source reduction. On the basis of previous fuelspill investigations in similar soils at Wurtsmith AFB, BTEX constituents in mobile LNAPL decreased at rates exceeding 70 percent per year through natural weathering (Parsons ES, 1995). Approximately 1,500 gallons of JP-4 released into a shallow, sandy aquifer at Wurtsmith AFB in October 1988 had weathered to low residual-phase concentrations (<150 μg/L) without measurable free-product by June 1991. BTEX compounds in LNAPL are being similarly weathered at UST 870, as seen by a decrease in BTEX concentrations in LNAPL over time (Table 4.1). The LNAPL sample taken from MW-10 exhibited a 70percent loss of BTEX constituents relative to fresh LNAPL (JP-4). Hence, the partitioning strength of BTEX compounds in LNAPL contamination is diminishing not only from engineered removal (bioslurpers), but also from natural weathering. Regardless of the value used to estimate annual BTEX source reductions, the calibrated model predicts that groundwater will not migrate past the base boundary, with the front of the plume stabilizing near Cambridge Street (assuming current conditions are not compromised with further fuel spills). The BTEX plume is expected to disappear from overwhelming natural attenuation mechanisms once BTEX source concentrations are reduced to approximately 50 percent of their current concentration.

Implementation of Alternative 1 would require the use of institutional controls such as land use restrictions and long-term monitoring. Land use restrictions may include placing long-term restrictions on soil excavation within the source area and ground water well installations within and downgradient of the source area. The intent of these restrictions would be to reduce potential receptor exposure to contaminants by legally restricting activities within areas affected by site-related contamination.

As a minimum, ground water monitoring would be conducted twice annually as part of this remedial technology to evaluate the progress of natural attenuation processes. Based on the potential plume migration, the Cambridge Street stormwater drain could be impacted by benzene at concentrations approaching the federal MCL of $5 \mu g/L$. Section 7 discusses the proposed locations of a POC sampling point located at the stormwater drain outfall and three POC wells that would be used to identify the potential migration of contaminated ground water into or beyond the Cambridge Street stormwater sewer. These wells would be screened across the first 5 to 10 feet of the shallow aquifer to provide some early warning of the advance of the plume toward the base boundary. In addition to these wells, the stormwater discharge from the Cambridge Street sewer would also be monitored to verify hydraulic connection between the shallow ground water and this potential pathway. Detection of benzene in excess of $5 \mu g/L$ at the POC wells or stormwater discharge point would trigger a reevaluation of remedial options to ensure that MCLs are not exceeded at the stormwater discharge point.

Public education on the selected alternative will be developed to inform base personnel and residents of the scientific principles underlying source reduction and intrinsic remediation. This education could be accomplished through public meetings, presentations, press releases, and posting of signs where appropriate. Periodic site reviews could also be conducted every year using data collected from the long-term ground water monitoring program. The purpose of these periodic reviews would be to evaluate the extent of contamination, assess contaminant migration and attenuation over time, document the effectiveness of institutional controls at the site, and reevaluate the need for additional remedial actions at the site.

6.3.2 Alternative 2 - Continued Mobile LNAPL Recovery and Bioventing, Intrinsic Remediation, Institutional Controls with Long-term Ground Water Monitoring, Stormwater Treatment

This alternative is identical to Alternative 1 except that it includes a provision for stormwater treatment if MCLs are exceeded at the stormwater discharge point. Construction

of a passive ground water collection trench was considered but deemed unnecessary given the very low concentration of BTEX expected near the storm drain. Aboveground treatment of stormwater using a portable sparging tank will be included to ensure that benzene concentrations in excess of MCLs do not pose a threat to human or ecological receptors at the stormwater discharge pond. Stormwater would be treated using a simple air sparging tank that would strip BTEX compound from the stormwater prior to discharge to the pond. This alternative would supplement intrinsic remediation by ensuring that any ground water with BTEX concentrations exceeding MCLs is treated before it completes a potential exposure pathway. As with Alternative 1, institutional controls and long-term monitoring would be required. The presence of benzene in excess of 5 µg/L at POC wells could also trigger the need for additional ground water remediation downgradient of Cambridge Street to ensure contaminated ground water does not migrate off-base.

A low-flow weir would be constructed at the stormwater discharge point to convey stormwater through the sparge tank at rates the system is capable of handling. In the event that stormwater runoff exceeds the capacity of the weir (and the sparge tank system), the excess stormwater will be discharged directly to collection ponds without treatment. Although excess water would not be treated, the anticipated risk of BTEX contamination would be very low due to dilution of the BTEX compounds.

6.3.3 Alternative 3 - Expanded Mobile LNAPL Removal and Bioventing, Intrinsic Remediation, Institutional Controls and Long-Term Monitoring

This remedial alternative couples several remedial technologies to more aggressively address both mobile LNAPL and residual LNAPL contamination in soil and ground water at UST Site 870. The objective of this alternative would be to more rapidly reduce the partitioning of BTEX from mobile LNAPL and soils and to ensure that no contaminated ground water migrated into or beyond the Cambridge Street stormwater drain. The source removal technologies considered for mobile LNAPL and residual LNAPL contamination in the soil and capillary fringe are mobile LNAPL recovery using LNAPL recovery pumps, soil vapor extraction, and bioventing.

A maximum of 4 feet of apparent floating mobile LNAPL was discovered at UST Site 870 during recent field investigations. Current mobile LNAPL recovery efforts are focused in the spill source area, although the estimated areal extent of mobile LNAPL contamination at the site extends downgradient of this area (Section 4). More intensive mobile LNAPL recovery could be accomplished by installing conventional skimmer pumps in available 4-inch ground

water monitoring wells containing mobile LNAPL. As a supplement to these pumps, it would also be necessary to install additional product recovery wells and total fluid recovery pumps downgradient of current product recovery wells. Any recovered product would be separated in an oil/water separator, and transported offsite for recycling or disposal in a permitted treatment, storage, and disposal facility for waste oil. It was assumed that contaminated water could be transported to the base industrial wastewater sewer system.

The leading edge of the migrating mobile LNAPL area shown in Figure 4.1 would be targeted for mobile LNAPL recovery. For estimating purposes five, 6-inch diameter mobile LNAPL recovery wells would be installed in a line between CPT-14 and MW-10 to more rapidly remove this source of BTEX contamination. A total-fluids recovery system is recommended to remove LNAPL and small quantities of water from this area. It is important to note that even in optimum, coarse-grained soils, a 30- to 50-percent recovery of the spilled fuel is considered excellent.

Much of the remaining 50 to 70 percent of the fuel is more tightly occluded and bound in the micropore structure of the soil. Removal of this residual fuel can be accomplished using either soil vapor extraction or bioventing technologies. Bioventing is an *in situ* process where low-flow air injection is used to enhance the biodegradation of organic contaminants in subsurface soils. Soil vapor extraction focuses on rapidly removing the volatile fraction of fuels through extracting soil vapor at higher rates. Both technologies have been successfully applied at JP-4 contaminated sites on Hill AFB (Hinchee, 1993) Bioventing is generally the technology of choice because unlike soil vapor extraction, bioventing uses a low rate of air injection that does not create vapor emissions to the atmosphere. Utah strictly limits VOC emissions, and the cost of soil vapor extraction is nearly doubled when vapor treatment is required. Although bioventing has been selected for this alternative, special flux monitoring will be required if air injection is proposed for the capillary fringe contamination beneath the residential area.

Extensive pilot- and full-scale testing of the bioventing technology at Hill AFB has resulted in significant reductions in soil BTEX and TPH. At Site 388, JP-4 jet fuel biodegradation rates were estimated at 2,500 milligrams of TPH per kilogram of soil per year (ES, 1994). Based on an estimated 60-foot radius of oxygen influence observed at Site 388, construction of a bioventing system at UST Site 870 could require approximately 11 vertical vent wells to influence the estimated 120,000 square feet of area with BTEX-impacted soils exceeding 50 mg/Kg total BTEX. Four-inch-diameter wells could be used, and screened intervals would be installed over the thin contaminated soil interval just above the water table. A single 20-

horsepower blower system should be capable of supplying air (oxygen) to this soil volume. Operational emphasis would be placed on the destruction of BTEX compounds in the capillary fringe to significantly reduce this source of continuing ground water contamination.

Although bioventing is primarily used to address vadose (unsaturated) soil contamination, field demonstrations have shown an increase in DO concentration levels in phreatic soil and ground water (Barr, 1993). The increase in DO concentrations within the capillary fringe and ground water can facilitate biodegradation of dissolved hydrocarbon contamination.

In order to estimate the potential impact of this more intensive source removal on the downgradient plume expansion, a 15-percent per year reduction in the BTEX source term was factored into the Bioplume II model. This assumes that the more extensive mobile LNAPL removal and bioventing systems will be able to remove BTEX three times faster than the current source removal rates assumed under Alternatives 1 and 2. Figure 5.13 illustrates the predicted BTEX plume migration after 3 years of more intensive source removal. The model predicts that after 3 years, BTEX concentration will approximately one-half of those encountered with Alternative 1 and 2 after the same 3-year period. Based on these model predictions, the combined effect of intensive source removal and intrinsic remediation would reduce the likelihood of benzene migration in excess of its MCL beyond the POC wells and into the Cambridge Street storm drain. Under this scenario, the need for treatment of the stormwater discharge seems unlikely.

Although more intensive source removal would more rapidly decrease dissolved BTEX concentrations and accelerate intrinsic remediation, it would not eliminate the need for short-term institutional controls and long-term monitoring. The required time frame for institutional controls and long-term monitoring could be shortened by approximately 4 to 5 years if this alternative were implemented.

6.4 EVALUATION OF ALTERNATIVES

This section provides a comparative analysis of each of the three remedial alternatives based on the effectiveness, implementability, and cost criteria. A summary of this evaluation is found in Table 6.6 at the end of this section.

6.4.1 Alternative 1 - Continued Mobile LNAPL Removal and Bioventing in Source Area, Intrinsic Remediation, Institutional Controls with Long-Term Monitoring

6.4.1.1 Effectiveness

Section 5 of this document presents the results of the Bioplume II model completed to support the intrinsic remediation alternative at UST Site 870. The potential impacts of remaining mobile LNAPL on ground water contamination over time were incorporated into the model for this remedial alternative. Only the existing product recovery and bioventing systems in the spill area were included in this alternative because of the increasing cost and reduced efficiency of trying to recover a more dispersed mobile LNAPL layer in downgradient areas.

This assessment predicted that natural attenuation mechanisms will significantly limit contaminant migration and reduce contaminant mass and toxicity. However, the model predicted a potential exceedance of the federal MCL for benzene at the POC wells (Figure 7.1) and a potential risk of exposure at the outfall of the Cambridge Street stormwater drain. Because the Bioplume II model is based upon numerous conservative assumptions and does not fully account for the anaerobic biodegradation available due to sulfate and other electron acceptors, it is possible that benzene concentrations in excess of 5 µg/L will never reach the POC wells or storm drain. Semiannual ground water monitoring at the stormwater discharge point and the POC wells and other wells along the leading edge of the existing plume would be critical to ensuring the protectiveness of this alternative. This alternative would cease to be protective if the BTEX plume was intercepted by the storm drain and contaminated ground water was subsequently discharged into the stormwater pond.

The effectiveness of this remedial alternative requires that excavations or drilling within the source area be limited to properly protected site workers. Long-term land use restrictions will be required to ensure that shallow ground water will not be pumped or removed for potable use within, and approximately 500 feet in all directions from, the existing BTEX plume. Existing health and safety plans should be enforced to reduce risks from operating existing source reduction technologies and from installing and monitoring additional POC wells.

Compliance with program goals is one component of the long-term effectiveness evaluation criterion. Alternative 1 will satisfy program objectives designed to promote intrinsic remediation as a component of site remediation and to scientifically document naturally occurring processes.

Alternative 1 is based on the effectiveness of naturally occurring processes that minimize contaminant migration and reduce contaminant mass over time and the effectiveness of institutional controls. As described earlier, an investigation of the potential effectiveness of naturally occurring processes at UST Site 870 using field data and the Bioplume II model has demonstrated that the BTEX plume will be significantly reduced in size and mass in 4 to 7 years. The maximum distance traveled by the plume could be slightly beyond the Cambridge Street stormwater drain, however, the mass of the benzene will be significantly reduced during that time so that the maximum concentration of benzene reaching the stormwater drain is on the order of magnitude of the 5 µg/L MCL. The sensitivity analysis completed on the Bioplume II model for this site (Section 5) suggests that even under the most conservative (i.e., worst-case) conditions, the naturally occurring processes at UST Site 870 should significantly reduce contaminant migration to a potential exposure point (the stormwater drain located along Cambridge Street). Aside from the administrative concerns associated with long-term enforcement of long-term land use restrictions and long-term ground water monitoring programs, this remedial alternative should provide reliable, continued protection.

For cost comparison purposes, and based on Bioplume modeling results, it is assumed that source removal will continue for 8 years and that dissolved benzene concentrations will exceed MCLs throughout the plume for approximately 8 years under Alternative 1. The 8-year time frame is a reasonable source removal goal based on predictions of successful source removal, both engineered and natural, that will approach, or exceed, 5 percent annually (Section 6.3.1). An additional 5 years of semi-annual ground water monitoring will be required to ensure that intrinsic remediation has uniformly reduced all BTEX compounds to levels below federal MCLs, resulting in a total treatment/monitoring time of approximately 13 years.

6.4.1.2 Implementabilty

Alternative 1 is not technically difficult to implement. Continued operation of existing mobile LNAPL recovery and bioventing systems will require minimal new construction. Existing procedures for mobile LNAPL removal and recycling will be followed. Installation of POC ground water monitoring wells is a standard procedure at Hill AFB. Long-term management efforts will be required to ensure proper sampling procedures are followed. Periodic site reviews should be conducted to confirm the adequacy and completeness of long-term monitoring data and verify the effectiveness of this remediation approach. There may also be administrative concerns associated with long-term enforcement of ground water use restrictions. Future land use within the source area may be impacted by leaving contaminated

soil and ground water in place. Regulators and the public will have to be informed of the benefits and limitations of the intrinsic remediation option. Educational programs are not difficult to implement, and the initial regulatory reaction to this alternative has been positive.

6.4.1.3 Cost

The cost of Alternative 1 is summarized in Table 6.3. Capital costs are limited to the construction of three new POC wells. The estimated cost of maintaining existing mobile LNAPL recovery and bioventing systems for 8 years are included in the \$372,000 present-worth cost estimate for Alternative 1. Also included are the costs of maintaining institutional controls and long-term ground water monitoring for a total of 13 years. The total present worth of this alternative is most sensitive to the estimated time requirement for intrinsic remediation to reduce benzene concentrations to less than the 5 μ g/L MCL. Costs could be reduced by changing from semiannual to annual monitoring after the plume begins to recede.

6.4.2 Alternative 2 - Continued Mobile LNAPL Recovery and Bioventing in Source Area, Intrinsic Remediation, Institutional Controls with Long-Term Ground Water Monitoring, Stormwater Treatment

6.4.2.1 Effectiveness

The effectiveness of Alternative 1 is enhanced under Alternative 2 by ensuring that if stormwater becomes contaminated, an air stripping unit will be installed to treat ground water to levels below federal drinking water MCLs before it is discharged to the stormwater pond. As stated in Section 6.3.2, the use of a stormwater air stripper would be contingent on BTEX concentrations exceeding MCLs at the stormwater discharge point. Air stripping technologies, including sparging tanks, are proven and reliable systems for reducing BTEX compound concentrations in water by more than 95 percent. The use of a low-flow diversion weir to treat only more concentrated BTEX-contaminated stormwater will reduce the size and complexity of the air stripping system. This alternative also complies with the program goals because intrinsic remediation remains the predominant decontamination method at the site.

6.4.2.2 Implementability

The addition of a small stormwater treatment system at the stormwater discharge point near the stormwater pond does not present any unique implementation problems. A 230-volt power source and a concrete pad would be required to support the portable sparging tank system. Additional time would be required for base personnel to sample influent and effluent to the sparging tank. The use of a sparging tank will minimize maintenance time. Some

TABLE 6.3

ALTERNATIVE 1 - COST ESTIMATE UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

Capital Costs	Cost
Design/Construct Three POC Wells	\$12,000
Operation, Maintenance and Monitoring Costs (Annual)	Annual Cost
Operate and Maintain Existing Mobile LNAPL Recovery and Bioventing Systems (8 years)	\$18,000
Ground Water Monitoring (12 wells - Semiannually 13 Years)	\$12,000
Maintain Institutional Controls/Public Education (13 years)	\$6,000
Project Management (13 y rs)	\$8,000
Present Worth of Alternative 1"	\$372,000

a/ Based on I=5%

accumulation of iron and manganese sludge and biological sludge will occur in the tank. A properly designed tank will have a conical bottom to draw off sludge without interrupting the treatment process. Waste sludge should be nonhazardous.

The installation of POC wells, the institutional controls and long-term monitoring commitments described in Alternative 1 will also be implemented with this alternative. If benzene exceeds $5 \mu g/L$ at POC wells, additional ground water remediation may be required to ensure that contaminated ground water is not migrating beyond the base boundary.

6.4.2.3 Cost

The cost of Alternative 1 will be increased by the stormwater treatment system and maintenance and monitoring of the system. Based on Bioplume II model predictions, the plume will begin to recede during the fourth year. For cost comparison purposes its is assumed that the stormwater treatment system will operate for 5 years to ensure that contaminated ground water is not discharged to the stormwater pond. As with Alternative 1,

source reduction technologies would continue for 8 years under Alternative 2. Annual long-term monitoring would continue for an ditional 5 years to ensure that intrinsic remediation is reducing contaminant concentrations below MCLs throughout the plume. The estimated capital and operating costs of Alternative 2 are shown in Table 6.4. The total present worth cost of Alternative 2 is \$455,000.

6.4.3 Alternative 3 - Intensive Source Removal, Intrinsic Remediation, Institutional Controls and Long-Term Monitoring

6.4.3.1 Effectiveness

More intensive source removal coupled with intrinsic remediation and long-term monitoring should reduce the dissolved-phase BTEX plume concentrations and significantly reduce potential exposure at the Cambridge Street stormwater discharge. If a greater percentage of the mobile LNAPL could be removed and soil BTEX concentrations could be significantly reduced, the partitioning of BTEX into ground water would be reduced, thereby promoting a more rapid decrease in contaminant mass, mobility, and toxicity. It was assumed that mobile LNAPL removal and bioventing would continue for approximately 4 years. During these 4 years, the site model assumed that the total BTEX mass in the soil would be reduced by 60 percent and that average dissolved benzene concentrations at the center of the plume would be reduced to less than 5 μ g/L as a result of intrinsic remediation.

Conceptually, this 15-percent annual reduction in a BTEX source from mobile LNAPL will be obtained from both natural weathering and increased engineered removal. Natural weathering rates of BTEX compounds in mobile LNAPL under similar conditions can be substantial (Section 6.3.1). Similar weathering losses of JP-4 contamination are occurring at Site UST 870. The assumed 15-percent annual reduction of BTEX constituents in mobile LNAPL does not necessarily represent actual weathering rates, but show potential LNAPL reduction rates as a result of increased LNAPL removal along with natural weathering. More intensive source removal could help achieve protectiveness approximately 4 years sooner than that under Alternative 1. The model predicts that with more intensive source removal, the BTEX plume will be less concentrated approaching the Cambridge Street stormwater drain, and this exposure pathway may not be completed.

Site workers would have to handle and be exposed to larger volumes of extracted mobile LNAPL. Bioventing in the source area and downgradient smear zones would be an effective

TABLE 6.4

ALTERNATIVE 2 - COST ESTIMATE UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

Capital Costs	Cost
Three POC Wells	\$12,000
Stormwater Treatment System	\$24,000
Operation, Maintenance and Monitoring Costs (Annual)	Annual Cost
Operate Existing Mobile LNAPL Recovery/Bioventing Systems (8 years)	\$18,000
Operate and Monitor Stormwater Treatment System (5 years)	\$14,000
Ground Water Monitoring (12 wells - Semiannually 13 Years)	\$12,000
Maintain Institutional Controls/Public Education (13 years)	\$6,000
Project Management (13 years)	\$8,000
Present Worth of Alternative 2"	\$455,000

a/ Based on I=5%.

method of reducing the BTEX which could partition into shallow ground water. The toxicity of the soil would also be more rapidly reduced. Bioventing has been shown to preferentially remove BTEX compounds and reduce toxicity in soils (Miller, 1993). If air injection is used beneath the residential area, additional monitoring will be required to ensure that vapors do not migrate upward into occupied buildings.

The more aggressive source removal component of this remedial alternative satisfies the statutory preference for using treatment to more rapidly reduce contaminant mobility and toxicity. Long-term natural attenuation processes will also reduce contaminant toxicity, mobility, and volume in ground water. Long-term land restrictions should be implemented to ensure that shallow ground water will not be available for use as a potable water source downgradient of the source area. A health and safety plan would be developed to mitigate

risks from installing and operating the expanded mobile LNAPL recovery and bioventing system, and installing and monitoring POC wells. Thus, this remedial alternative should also minimize contaminant migration and provide long-term protection.

Alternative 3 also satisfies the program objectives of demonstrating the potential effectiveness of intrinsic remediation for minimizing plume expansion and reducing BTEX mass and toxicity. However, this remedial alternative will result in the generation of additional mobile LNAPL, ground water, drill cuttings, and other wastes requiring treatment and/or disposal. Alternative 3 (intensive source removal, intrinsic remediation, and long-term monitoring) should provide reliable, continuous protection with little risk from temporary system failures.

6.4.3.2 Implementability

Installing and operating a more intensive mobile LNAPL recovery, and bioventing system to remove the source of BTEX contamination at UST Site 870 will present additional implementability concerns. Installation involves standard drilling practices for wells, and limited excavation for piping and manifold connections. Implementation in and around residential areas would be disruptive to residents and their yards. Mobile LNAPL recovery and bioventing equipment is available, and small systems are already in place in the UST Site 870 spill area. Extraction wells required for product recovery represent a well-developed technology that has been proven at numerous sites. Bioventing is an innovative technology that has been used effectively at other JP-4 contaminated sites at Hill AFB. Implementation of this remedial alternative would also require flux monitoring during bioventing startup to confirm that soil vapors are not transmitted upward into residential buildings. Annual in situ respiration testing is also required to verify that the system is working as expected. The technical and administrative implementability concerns associated with the intrinsic remediation and long-term monitoring component of this remedial alternative are identical to those discussed in Alternative 1, except the time frame is approximately 4 years shorter.

6.4.3.3 Cost

The total present worth of this alternative is estimated at \$782,000. The cost differential between Alternatives 2 and 3 is sensitive to the extent and duration of required LNAPL recovery, bioventing operations, and the accuracy of intrinsic remediation modeling results. Table 6.5 lists the costs for Alternative 3 based on a mobile LNAPL removal period of 4 years and a bioventing period of 4 years. During years 4 through 9, semiannual ground water

TABLE 6.5

ALTERNATIVE 3 - COST ESTIMATE UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

Capital Costs	Cost
Design/Construct 5 Mobile LNAPL Recovery Wells and Collection Systems	\$98,000
Design/Construct 11-Well Bioventing System	\$363,000
Design/Construct Three POC Wells	\$12,000
Operation, Maintenance and Monitoring Costs (Annual)	Annual Cost
Operate New Mobile LNAPL Recovery/ Bioventing Systems (4 years)	\$36,200
Ground Water Monitoring (12 wells - Semiannually Years 1-9)	\$12,000
Maintain - Institutional Controls/Public Education (9 years)	\$6,000
Project Management (9 years)	\$8,000
Present Worth of Alternative 3 ^{2'}	\$782,000

a/ Based on i=5%.

monitoring will be conducted to verify that intrinsic remediation is reducing dissolved BTEX contaminants to levels below MCLs.

6.5 RECOMMENDED REMEDIAL APPROACH

Three multicomponent alternatives have been evaluated for remediation of the shallow ground water at UST Site 870. Alternatives evaluated include two levels of source removal, intrinsic remediation with long-term monitoring, and an alternative which would treat stormwater if it contained benzene or other BTEX compounds in excess of MCLs. Table 6.6 summarizes the results of this evaluation based upon effectiveness, implementability and cost criteria. Based on this evaluation, the Air Force recommends Alternative 2 as the best combination of risk reduction and cost effectiveness to achieve RAOs for dissolved-phase BTEX in UST Site 870 ground water.

Only marginal reductions in plume migration and risk reduction will be achieved if more intensive source removal is applied to the downgradient smear zone. These marginal reductions will come at a significant increase in cost and significant disturbance to a residential area during additional mobile LNAPL recovery well and bioventing system construction. Based on all effectiveness criteria, Alternative 2 will make maximum use of intrinsic remediation to reduce plume migration and toxicity while providing the assurance that if MCLs are exceeded at the stormwater discharge point, an effective treatment system can be rapidly installed to prevent completion of a very conservative exposure pathway.

All of the remedial alternatives are implementable, however, Alternative 2 significantly minimizes potential disruptions to base housing residents and should be acceptable to the public and regulatory agencies because it is protective of human health and the environment. Implementation of Alternative 2 will require land use and ground water use controls to be enforced for approximately 8 to 13 years with semiannual ground water monitoring. The cost of Alternatives 1 and 2 could be reduced if annual ground water monitoring is implemented once the plume began to recede.

The final evaluation criterion used to compare each of the three remedial alternatives was cost. It is the opinion of the Air Force that the additional cost of Alternative 2 over Alternative 1 is justified by the additional protection it provides. In contrast, the additional cost of Alternative 3 can not be justified by the marginal reduction in treatment and monitoring time that is gained from more intensive source removal.

TABLE 6.6 SUMMARY OF REMEDIAL ALTERNATIVE EVALUATION GROUND WATER REMEDIATION UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

Remedial Alternative	Effectiveness	malemontohiltu	Drecent Worth
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			Cost Estimate
Alternative 1			\$372,000
- Limited Source Removal Co	Continued mobile LNAPL removal and	Readily implementable. Long-term	
- Intrinsic Remediation bio	bioventing will gradually remove BTEX	management, ground water use controls and	
- Long-Term Monitoring sou	source. Contaminant mass, volume and	monitoring required for an estimated 13	
tox	toxicity will be significantly reduced over	years. Minimal exposure of site workers if	
nes	next seven years. MCL for benzene could	excavation is carefully controlled in source	
be	be exceeded at POC.	area.	
Alternative 2			\$455,000
- Limited Source Removal Sin	Similar to Alternative 1 except it provides	Readily implementable. Long-term	
- Intrinsic Remediation add	additional protection against benzene	management, ground water controls, and	
- Optional Stormwater dis	discharge into stormwater ponds and	monitoring required for an estimated 13	
Treatment pol	potential completion of exposure	years. Would also require minor construction	
- Long-Term Monitoring pat	pathways to humans or ecological	at stormwater outfall and operation of a	
rec	receptors. Portable sparging tank should	simple sparging tank for approximately 5	
- pe	be very effective in removing low levels of	years.	
BT	BTEX prior to discharge to pond.		
Alternative 3			\$782,000
	Most effective in reducing soil	Difficult to implement in residential area	
ing	contamination and more rapidly reducing	without disruption and potential secondary	
- Intrinsic Remediation sou	source of ground water contamination.	risk to residents. Could reduce long-term	
- Long-Term Monitoring Ma	May prevent BTEX from impacting POC	management, ground water use controls and	
we	wells if implemented immediately (1995).	monitoring by 4-5 years compared to	
<u> </u>	Could result in increased generation of	Alternative 1 and 2. Increased drilling and	
) sec	secondary waste streams that would	system maintenance will increase site worker	
JO	require additional treatment and disposal.	exposure to contaminated soils and mobile LNAPL	

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SECTION 7

ONG-TERM MONITORING PLAN

7.1 OVERVIEW

As discussed in Section 6, the preferred remedial option for the fuel-hydrocarbon contamination present in ground water at UST Site 870 is Alternative 2. This alternative consists of continued mobile LNAPL recovery and bioventing for mobile- and residual-phase LNAPL contamination, and intrinsic remediation with LTM for contaminated ground water. In addition, this alternative has a provision for treatment of stormwater discharge should BTEX compounds in excess of MCLs be detected in stormwater runoff at the stormwater drain outfall. In keeping with the requirements of this remedial alternative, a LTM plan must be developed. The purpose of LTM is sessite conditions over time, confirm the effectiveness of naturally occurring process. The reducing contaminant mass and minimizing contaminant migration, validate/calibrate the Bioplume II model, and evaluate the need for additional remediation.

The LTM plan consists of identifying the location, of two separate ground water monitoring networks and developing a ground water and stormwater discharge point sampling and analysis strategy. The strategy described in this section is designed to monitor plume migration and attenuation over time to verify that intrinsic remediation of dissolved-phase BTEX is occurring at rates sufficient to protect potential receptors.

7.2 MONITORING NETWORKS

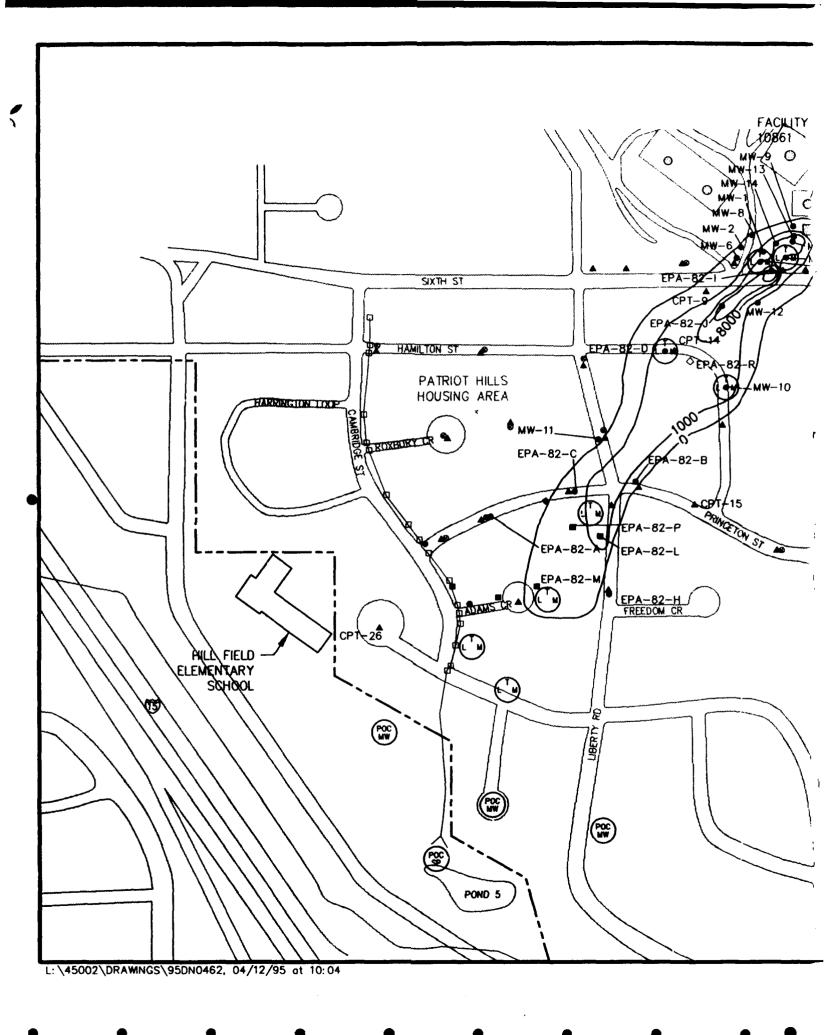
Two separate ground water monitoring networks will be used at UST Site 870 as part of the intrinsic remediation remedial alternative LTM plan. The first network will consist of eight LTM wells located upgradient, within, and downgradient of the observed total BTEX plume. The purpose of the LTM well network is to provide short-term confirmation and verification of intrinsic remediation and to verify the results of the Bioplume II model. The second network of ground water monitoring points will consist of three POC wells and a POC

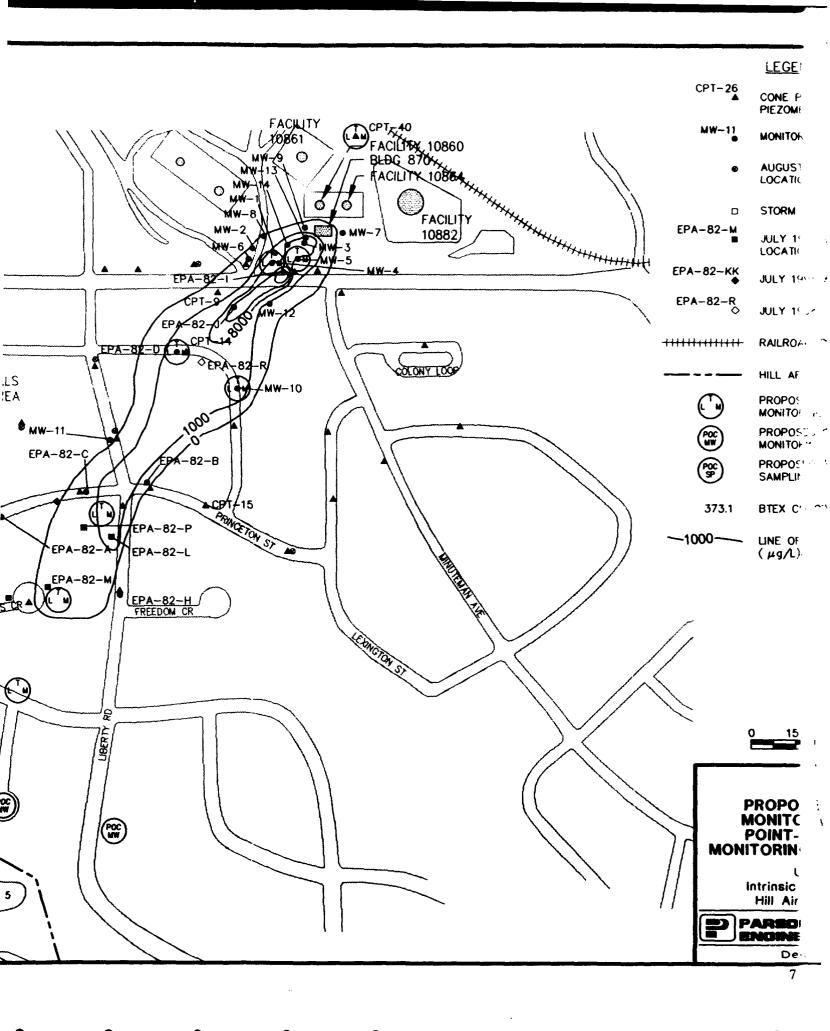
sampling point at the Pond 5 outfall of the stormwater drain located along Cambridge Street. The purpose of the POC monitoring network is to verify that no BTEX compounds in concentrations exceeding MCLs migrate beyond the area under institutional control. Should BTEX compounds be detected in the stormwater drain discharge, installation and operation of the stormwater treatment system discussed in Section 6 will be implemented. Should BTEX compounds be detected in POC wells above MCLs, other remedial options will be evaluated.

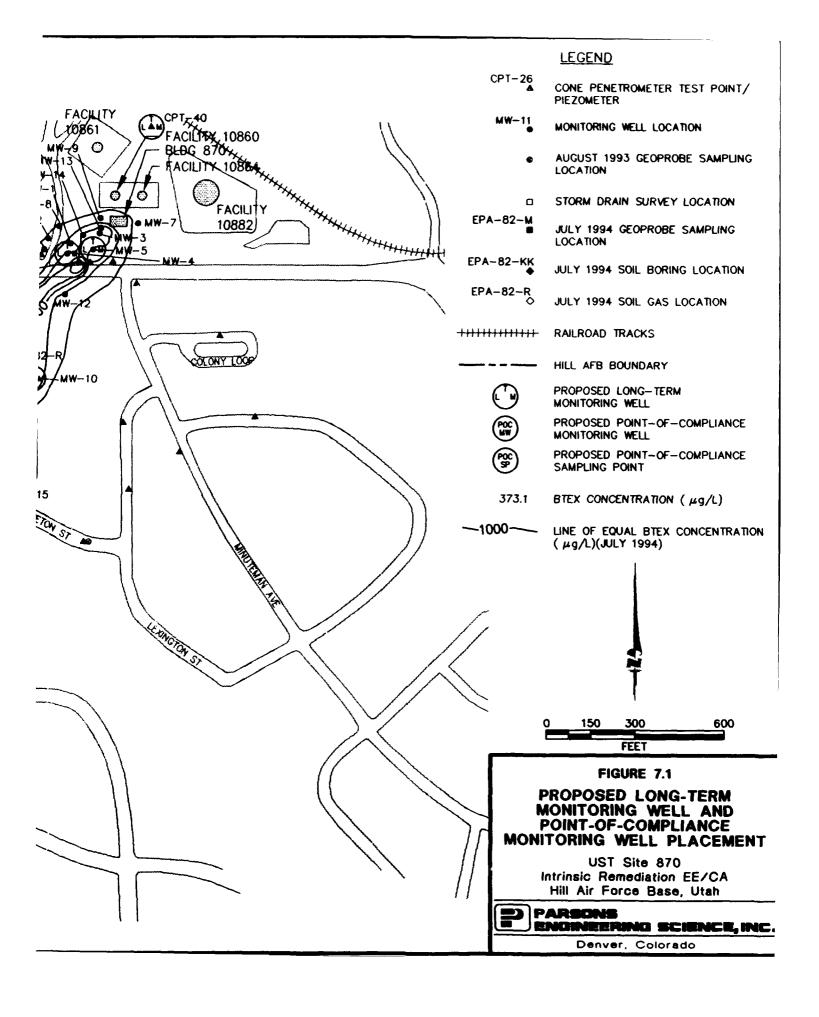
7.2.1 Long-Term Monitoring Network

Eight ground water monitoring wells placed upgradient, within, and immediately downgradient of the existing BTEX contaminant plume will be used to monitor the effectiveness of intrinsic remediation in reducing total contaminant mass and minimizing contaminant migration. Figure 7.1 shows the proposed locations of these wells. One new and four existing monitoring wells (MW-04, MW-05, EPA-82-D and MW-10) will be used as LTM wells to monitor natural attenuation within the anaerobic treatment zone and BTEX concentrations in the source area. In the event that MW-04 is screened to shallow to permit an accurate ground water sample, monitoring wells EPA-82-I, MW-01, or MW-14 should be considered as a substitute LTM location. One new LTM well should be placed within the aerobic treatment zone to monitor natural attenuation within this zone. One new LTM well should be placed downgradient of the BTEX plume. Sampling and analysis of the downgradient LTM well (and the POC wells) will be useful in monitoring changes in ground water chemistry through time and will facilitate early detection of plume migration. Because the velocity of the dissolved-phase BTEX plume is retarded relative to the advective ground water velocity and the velocities of the electron acceptors are not, depleted DO, nitrate, and sulfate concentrations, and elevated ferrous iron and methane concentrations will advance in front of the BTEX plume. Thus, changes in the concentrations of the electron acceptors can be used to provide early warning of BTEX plume encroachment on the LTM and POC wells.

An existing CPT monitoring point (CPT-40) should be used as an upgradient LTM well. CPT-40 was selected as an upgradient LTM point because it has historically been free of ground water contamination and is suited for monitoring background levels of ground water electron acceptors, pH, and oxidation/reduction potential. The different well diameter of CPT-40 compared to the other proposed LTM wells is not a sampling issue because background levels of ground water parameters are presumed to be uniform throughout the







the shallow aquifer. In the case that CPT-40 is destroyed or inaccessible, a new LTM well (described in Section 7) well be installed instead.

The LTM network will supplement the POC monitoring network in monitoring plume migration and will allow model predictions to be validated. Such monitoring of the plume will allow additional response time if BTEX concentrations within the plume are increasing or if the plume begins to migrate further than expected. New LTM wells should be constructed of 2-inch PVC with 5 to 10 feet of 0.010-inch-slotted screen. The screened interval should be within the same stratigraphic horizon as the contaminant plume. The screened interval should be chosen so that the base of the screen coincides with the interface between the sandy saturated zone and the underlying competent clay to silty clay and the top of the screen is above the seasonal high water table.

7.2.2 Point-of-Compliance Monitoring Network

Three new POC monitoring wells should be installed to verify that no contaminated ground water exceeding MCLs migrates beyond the area under institutional control. Figure 7.1 shows the proposed locations for the POC wells and the stormwater drain sampling point. POC sampling points will be used to demonstrate protection of human health and the environment and compliance with site-specific numerical remediation goals (i.e., MCLs for the BTEX constituents).

As described for the LTM wells, the POC wells also should be screened in the same hydrogeologic unit as the contaminant plume. Data presented in this report concerning the nature and extent of contamination at the site suggest that a 5- to 10-foot screen extending from slightly above the ground water table to the interface between the sandy saturated zone and the underlying competent clay to silty clay confining unit should be used to monitor changes in ground water chemistry at these locations. New POC wells should be constructed of 2-inch PVC and a 0.010-inch slotted screen should be used.

7.3 GROUND WATER SAMPLING AND ANALYSIS

To ensure that sufficient contaminant removal is occurring at UST Site 870 to protect human health and the environment and meet site-specific remediation goals, the LTM plan includes a comprehensive sampling and analysis plan. To supplement the LTM sampling and

analysis plan presented herein, a site-specific ground water sampling and analysis plan should be prepared prior to initiating the LTM program.

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7.3.1 Analytical Protocol

7.3.1.1 Long-Term Monitoring Well Analytical Protocol

All LTM wells will be sampled and analyzed to monitor trends in ground water chemistry and to verify the effectiveness of intrinsic remediation at the site. Water level measurements are to be made during each sampling event. All ground water samples from LTM wells will be analyzed according to the analytical protocol presented in Table 7.1. A site-specific ground water sampling and analysis plan should be prepared using this analytical protocol prior to initiating the LTM program.

7.3.1.2 Point-Of-Compliance Monitoring Point Analytical Protocol

All POC sampling points will be sampled and analyzed to monitor trends in ground water chemistry, to verify the effectiveness of intrinsic remediation at the site, and to demonstrate protection of human health and the environment and compliance with site-specific numerical remediation goals. Water level measurements are to be made in POC wells during each sampling event. All ground water samples from POC wells will be analyzed according to the analytical protocol presented in Table 7.2. All water samples from the POC stormwater drain outfall sampling location should be sampled for aromatic hydrocarbons only. A site-specific ground water sampling and analysis plan should be prepared using this analytical protocol prior to initiating the LTM program.

7.3.2 Frequency

Each of the LTM and POC sampling points will be sampled twice each year for 13 years. If the data collected during this time period supports the anticipated effectiveness of the intrinsic remediation alternative at this site, the sampling frequency can be reduced to once every year for all wells in the LTM program, or eliminated. If the data collected at any time during the monitoring period indicate the need for additional remedial activities at the site (i.e., by exceeding MCLs at POC locations) sampling frequency should be adjusted accordingly.

TABLE 7.1

LONG-TERM MONITORING ANALYTICAL PROTOCOL UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

				Recommended	Sample Volume, Sample	Field or
				Frequency of	Container, Sample Preservation	Fixed-Base
Analyte	Method/Reference	Comments	Data Use	Analysis		Laboratory
Ferrous (Fe ²⁺)	Colorimetric	Field only	Elevated ferrous iron	Semiannually	Collect 100 mL of water in a	Field
,	A3500-Fe D		concentrations may be indicative		glass container, acidify with	
			of the anaerobic biodegradation		hydrochloric acid per method	
			process of iron reduction			
Ferrous (Fe ²⁺)	Colorimetric	Alternate method;	Elevated ferrous iron	Semiannually	Collect 100 mL of water in a	Field
,	HACH 25140-25	field only	concentrations may be indicative		glass container	
			of the anaerobic biodegradation		-	
			process of iron reduction			
Temperature	E170.1	Field only	Metabolism rates for	Semiannually	N/A	Field
			microorganisms depend on		· ·	
			temperature			
Dissolved	Dissolved oxygen	Refer to	The oxygen concentration is a	Semiannually	Collect 300 mL of water in	Field
Oxygen	meter	Method A4500	data input to the Bioplume II		biochemical oxygen demand	
}		for a comparable	model; concentrations less than		bottles, analyze immediately,	
		laboratory	1 mg/L generally indicate an		alternately, measure dissolved	
		procedure	anaerobic pathway		oxygen in situ	
Hd	E150 1/SW9040, direct	Protocols/Handbook	Aerobic and anaerobic processes	Semiannually	Collect 106-250 mL of water in a	Field
•	reading meter	methods*	are pH-sensitive		glass or plastic container, analyze	
					ımmediately	
Conductivity	E120.1/SW9050, direct	Protocols/Handbook	General water quality parameter	Semiannually	Collect 100-250 mL of water in a	Field
	reading meter	methods	used as a marker to verify that		glass or plastic container	
			site samples are obtained from the same ground water system			
Nitrate (NO,1)	IC method E300 or	Method E300 is a	Substrate for microbial	Semiannually	Collect up to 40 mL of water in a	Fixed-base
	method SW9056;	Handbook method;	respiration if oxygen is depleted		glass or plastic container, cool to	
	colorimetric,	method SW9056 is			4°C; analyze within 48 hours	
	method E353.2	an equivalent				
		procedure				

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TABLE 7.1 (CONCLUDED)

LONG-TERM MONITORING ANALYTICAL PROTOCOL UST SITE 870 INTRINSIC REMEDIATION EE/CA HILL AFB, UTAH

Sample Volume, Sample Container, Sample Preservation Fixed-Base	Laboratory	Collect up to 40 mL of water in a Fixed-base glass or plastic container, cool to or field (for 4°C.	method)	Collect 100-250 mL of water in a Field	glass container, filling container from bottom: analyze immediately		-				Collect water samples in 40 ml Fixed-base	volatile organic analysis (VOA)	vials with butyl gray/Teflon-lined	caps (zero headspace); cool to 4°C			+	Collect water samples in a 40 int. Fixed-base	VOA vial with zero headspace;	cool to 4°C; add hydrochloric acid		
Sample Vol		Collect up to)	Collect 100-	glass contain from bottom						Collect wate	volatile orga	vials with br	caps (zero h				Collect wate	VOA vial w	cool to 4°C;	to pH 2	
Recommended Frequency of	Analysis	Semiannually		Semiannually							Semiannually							Semiannually				
	Data Use	Substrate for anaerobic microbial respiration		The redox potential of ground	water influences and is influenced by biologically	mediated reactions; the redox	potential of ground water may	range from more than 200 mV	to less than 400 mV		The presence of methane	suggests BTEX degradation via	an anaerobic pathway utilizing	carbon dioxide (carbonate) as	the electron acceptor	(methanogenesis)	e dante.	BIEX is the primary target	analyte for monitoring natural	attenuation; BTEX	concentrations must also be	measured for regulatory
	Comments	Method E300 is a Handbook method; method SW9056 is	an equivalent procedure. HACH method is Photometric	Measurements	are made with electrodes results	are displayed on a	meter, samples	should be protected	from exposure to	atmospheric oxygen	Method published	and used by the US	Environmental	Protection Agency	Robert S. Kerr	Laboratory		Handbook method;	analysis may be	extended to higher	molecular weight	alkylbenzenes
	Method/Reference	IC method E300 or method SW9056 or HACH	Sulfa Ver 4 method	A2580 B							RSKSOP-114 modified	to analyze water	samples for methane by	headspace sampling	with dual thermal	conductivity and flame	ionization detection.	Purge and trap GC	method SW8020			
	Analyte	Sulfate (SO ₄ ²)		Redox potential							Methane							Aromatic	hydrocarbons	(BTEX)		

a/ Protocol methods are presented by Wiedemeier et al., 1994

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TABLE 7.2

POINT-OF COMPLIANCE MONITORING ANALYTICAL PROTOCOL UST SITE 870 INTRINSIC REMEDIATION EE/CA

Fixed-Base Laboratory Fixed-base Field or Field Field Field Field Field Collect 100-250 mL of water in a Container, Sample Preservation Collect 100-250 mL of water in a Collect 100-250 mL of water in a from bottom, analyze immediately cool to 4°C; add hydrochloric acid glass or plastic container, analyze Collect water samples in a 40 mL glass container, filling container VOA vial with zero headspace, alternately, measure dissolved bottles, analyze immediately, biochemical oxygen demand Collect 300 mL of water in Sample Volume, Sample glass or plastic container oxygen in situ immediately ΑX Recommended Frequency of Analysis Semiannually Semiannually Semiannually Semiannually Semiannually Semiannually Aerobic and anaerobic processes General water quality parameter model; concentrations less than site samples are obtained from The oxygen concentration is a used as a marker to verify that The redox potential of ground potential of ground water may range from more than 200 mV the same ground water system analyte for monitoring natural HILL AFB, UTAH 1 mg/L generally indicate an mediated reactions; the redox concentrations must also be BTEX is the primary target data input to the Bioplume influenced by biologically measured for regulatory water influences and is to less than 400 mV attenuation; BTEX anaerobic pathway Well development are pH-sensitive compliance Protocols/Handbook methods* Protocols/Handbook should be protected atmospheric oxygen Handbook method; extended to higher electrodes; results are displayed on a molecular weight alkylbenzenes from exposure to for a comparable analysis may be Comments meter, samples method A4500 Measurements are made with laboratory Field only procedure Refer to methods E120.1/SW9050, direct E150.1/SW9040, direct Method/Reference Purge and trap GC method SW8020 Dissolved oxygen reading meter reading meter A2580 B Redox potential hydrocarbons Analyte Temperature Conductivity Dissolved Aromatic Oxygen (BTEX) 핌

a/ Protocol methods are presented by Wiedemeier et al., 1994

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SECTION 8

CONCLUSIONS AND RECOMMENDATIONS

This report presents the results of an EE/CA conducted by Parsons ES in conjunction with researchers from the USEPA RSKERL to determine the potential for intrinsic remediation of, and to develop an appropriate remedial alternative for, BTEX compounds dissolved in the shallow ground water at UST Site 870, Hill AFB, Utah. Previous investigations determined that JP-4 jet fuel had been released into the soil and shallow ground water at the site through POL operations. Chemical analysis of a sample of mobile LNAPL confirms that residual- and mobile-phase LNAPL contamination at the site is probably dominated by weathered JP-4 jet fuel. The main emphasis of the work described herein was to evaluate the potential for naturally occurring degradation mechanisms to reduce dissolved-phase fuel-hydrocarbon concentrations in ground water to levels that are protective of human health and the environment.

To collect the data necessary for the intrinsic remediation demonstration, Parsons ES and USEPA researchers collected soil and ground water samples from the site. Physical and chemical data collected under this program were supplemented with data collected during previous site characterization events. Site-specific geologic, hydrologic, and laboratory analytical data were then used in the Bioplume II numerical ground water model to simulate the effects of advection, dispersion, sorption, and biodegradation on the fate and transport of the dissolved-phase BTEX plume. Extensive site-specific data were used for model implementation. Model parameters that could not be obtained from existing site data were estimated using widely accepted literature values for sediments similar to those found at the site. Conservative aquifer parameters were used to construct the Bioplume II model for this study, and therefore, the model results presented herein represent a worst-case scenario. Actual dissolved-phase BTEX degradation rates observed during LTM at the site will probably be greater than predicted by this study. This will result in faster removal rates for the BTEX compounds and a shorter plume migration distance than predicted by the Bioplume II model.

The Bioplume II model predicts that the BTEX plume will approach the stormwater drain that runs parallel to Cambridge Street in 1 to 4 years at concentrations of approximately 1 µg/L. After this time, the plume will recede somewhat and reach steady-state equilibrium (continuous source), or will continue to recede until the plume disappears (source reduction). Ground water geochemistry suggests that DO, nitrate, ferric hydroxide, sulfate, and carbon dioxide present in site ground water have the capacity to assimilate at least 31,370 µg/L of total BTEX. The highest plausible total BTEX concentration observed at the site was 26,576 µg/L in August 1992. Based on site observations, ground water at the POL site has enough assimilative capacity to degrade dissolved-phase BTEX that partitions from the LNAPL plume into the ground water before the plume migrates 1,600 feet downgradient from the source area.

The results of the modeling effort and the intrinsic remediation demonstration indicate that dissolved-phase petroleum hydrocarbon contamination present in ground water poses no significant risk to human health or the environment in its present known, or predicted future, concentration and distribution. It is therefore recommended that intrinsic remediation with LTM be implemented for dissolved-phase BTEX contamination found in ground water at this site. To reduce sources of continuing contamination, it is also recommended that mobile LNAPL recovery operations and bioventing activities currently operating at the site be continued.

To verify the predictions made during the Bioplume II modeling effort and to monitor the long-term migration and degradation of the contaminant plume, it is recommended that eight LTM wells, three POC monitoring wells, and a POC sampling location be used at the mouth of the stormwater drain that runs along Cambridge Street and empties into Pond 3. Regular sampling and analysis of ground water from these sampling points will allow sufficient time to implement hydraulic controls to contain the plume if BTEX compounds are detected in the POC wells. These wells should be sampled on a semiannual basis for 13 years. If site conditions indicate that the contaminant plume is receding or gone at this time or sooner, sampling can be discontinued. Ground water samples should be analyzed for the analytes described in Section 7 of this report. If BTEX concentrations in ground water in the Cambridge Street stormwater discharge or POC wells are found to exceed MCLs, additional corrective actions should be implemented to remediate ground water at the site, as described in this report.

SECTION 9

REFERENCES

- Abdul, S.A., Gibson, T.L., and Rai, D.N., 1987, Statistical Correlations for Predicting the Partition Coefficient for Nonpolar Organic Contaminants Between Aquifer Organic Carbon and Water. *Hazardous Waste and Hazardous Materials*, 4(3):211-222.
- Abdul, A.S., Kia, S.F., and Gibson, T.L., 1989, Limitations of monitoring wells for the detection and quantification of petroleum products in soils and aquifers: *Ground Water Monitoring Review*, Spring, 1989, p. 90-99.
- Anderson, M.P., and Woessner, W.W., 1992, Applied Groundwater Modeling Simulation of Flow and Advective Transport: Academic Press, New York, 381 p.
- Ballestero, T.P., Fiedler, F.R., and Kinner, N.E., 1994, An investigation of the relationship between actual and apparent gasoline thickness in a uniform sand aquifer: *Ground Water*, v. 32, no. 5, p. 708-718.
- Barr, K.D., 1993, Enhanced groundwater remediation by bioventing and its simulation by modeling, In Proceedings of the 1993 *Environmental Restoration Technology Transfer Symposium*, January 26-28, Wyndham Hotel, San Antonio, Texas: United States Air Force Center for Environmental Excellence.
- Beller, H.R. Reinhard, M., and Grbic-Galic, D., 1992, Metabolic byproducts of anaerobic toluene degradation by sulfate-reducing enrichment cultures: *Applied Environmental Microbiology*, v. 58, p. 3192-3195.
- Blake, S.B., and Hall., R.A., 1984, Monitoring petroleum spills with wells some problems and solutions: In *Proceedings of the Fourth National Symposium on Aquifer Restoration and Ground Water Monitoring*: May 23-25, 1984, p. 305-310.
- Bohon, R.L., and Claussen, W.F., 1951, The Solubility of Aromatic Hydrocarbons in Water. Journal of American Chemical Society, 73(4):1571-1578.
- Borden, R.C. and P.B. Bedient. 1986. Transport of Dissolved Hydrocarbons Influenced by Oxygen Limited Biodegradation Theoretical Development. Water Resources Research, 22 (13) 1973-1982.
- Bouwer, H., and Rice, R.C., 1976, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells: *Water Resources Research*, v. 12, no. 3, p. 423-428.

- Bouwer, H., 1989, The Bouwer and Rice slug test an update: Ground Water, v. 27, no. 3, p. 304-309.
- Bouwer, E.J., 1992, Bioremediation of Subsurface Contaminants, In R. Mitchell, editor, Environmental Microbiology, Wiley-Liss, New York, New York.
- Concawe, 1979, Protection of groundwater from oil pollution; Den Haag, Report No. 3/79.
- Cozzarelli, I.M., Eganhouse, R.P., and Baedecker, M.J., 1990, Tranformation of Monoaromatic Hydrocarbons to Organic Acids in Anoxic Ground Water Environment. Environmental and Geological Water Science, 16.
- Davies, J.S., and Westlake, D.W.S., 1979, Crude Oil Utilization by Fungi. *Canadian Journal of Microbiology*, 25:146-156.
- de Pastrovich, T.L., Baradat, Y., Barthel, R., Chiarelli, A., and Fussell, D.R., 1979, Protection of groundwater from oil pollution: *CONCAWE*, The Hague, 61 p.
- Domenico, P.A., and Schwartz, F.W., 1990, Physical and Chemical Hydrogeology: *John Wiley and Sons*, New York, 824 p.
- Edwards, E.A., and Grbic-Galic, D., 1992, Complete mineralization of benzene by microorganisms under strictly anaerobic conditions: Applied Environmental Microbiology, v. 58, p. 2663-2666.
- Edwards, E.A., Wells, L.E., Reinhard, M., and Grbic-Galic, D., 1992, Anaerobic degradation of toluene and xylene by aquifer microorganisms under sulfate-reducing conditions: *Applied Environmental Microbiology*, v. 58, p. 794-800.
- Feth, J.H., Barker, D.A., Moore, L.G., and Brown, R.J., and Veirs, C.E., 1966, Lake Bonneville Geology and Hydrogeology of the Weber Delta District, Including Ogden, Utah: US Geological Survey Professional Paper 518, 76 p.
- Freeze, R.A., and Cherry, J.A., 1979, *Ground Water*. Prentice-Hall, Inc., Englewood Cliffs, New Jersey.
- Gemperline, Andrew, 1995, OO-ALC/EMR, personal written communication, Hill Air Force Base, 7276 Wardleigh Road, Utah, 84056-5127.
- Geoprobe Systems[®], 1994, Geoprobe GH-40 Soil Probing Hammer Operating Instructions, Technical Bulletin No. 94-040A.
- Goldstein, R.M., Mallory, L.M., and Alexander, M., 1985, Reasons for Possible Failure of Innoculation to Enhance Biodegradation. *Applied Environmental Microbiology*, 50(4):977-983.
- Grbic'-Galic', D., and Vogel, T.M., 1987, Transformation of toluene and benzene by mixed methanogenic cultures: Applied and Environmental Microbiology, v. 53, p. 254-260.
- Grbic'-Galic', D., 1990, Anaerobic microbial transformation of nonoxygenated aromatic and alicyclic compounds in soil, subsurface, and freshwater sediments: In J.M. Bollag and G. Stotzky, editors, Soil Biochemistry: Marcel Dekker, Inc., New York, p. 117-189.

- Hall, R.A., Blake, S.B., and Champlin, S.C. Jr., 1984, Determination of hydrocarbon thicknesses in sediments using borehole data: In *Proceedings of the Fourth National Symposium on Aquifer Restoration and Ground Water Monitoring*: May 23-25, 1984, p. 300-304.
- Hampton, D.R., and Miller, P.D.G., 1988, Laboratory investigation of the relationship between actual and apparent product thickness in sands:
- Hinchee, R.E., Alleman, B.C., Miller, R.N., and Vogel, C., 1993, Bioventing, In Proceedings of the 1993 Environmental Restoration Technology Transfer Symposium, January 26-28, Wyndham Hotel, San Antonio, Texas: United States Air Force Center for Environmental Excellence.
- Hine, J., and Mookerjee, P.K., 1975, The Intrinsic Hydrophilic Character of Organic Compounds. Correlations in Terms of Structural Contributions. *Journal of Organic Chemistry*, 40(3):292-298.
- Hopper, D.J., 1978, Microbial Degradation of Aromatic Hydrocarbons In R.J. Watkinson (editor), Developments in Biodegradation of Hydrocarbons, I. Applied Science Publishers, Ltd., London.
- Hughes, J.P., Sullivan, C.R., and Zinner, R.E., 1988, Two techniques for determining the true hydrocarbon thickness in an unconfined sandy aquifer: *In Proceedings of the Petroleum Hydrocarbons and Organic Chemicals in Ground Water*: Prevention, Detection, and Restoration Conference: NWWA/API, p. 291-314.
- Hutchins, S.R., 1991, Biodegradation of monoaromatic hydrocarbons by aquifer microorganisms using oxygen, nitrate, or nitrous oxide as the terminal electron acceptor: *Applied Environmental Microbiology*, v. 57, p. 2403-2407.
- Isnard, S., and Lambert, S., 1988, Estimating Bioconcentration Factors from Octanol-Water Partition Coefficient and Aqueous Solubility. *Chemosphere*, 17(1):21-34.
- James M. Montgomery Consulting Engineers, Inc., 1991, External Draft Site Characterization Report for UST Site 870.0 (AGSS), December, 1991.
- James M. Montgomery Consulting Engineers, Inc., 1992a, Free Product Recovery Letter Report, UST Site 870.0 (EGSS), November, 1992.
- James M. Montgomery Consulting Engineers, Inc., 1992b, Pumping Tests and Product Thickness Test Letter Report, UST Site 870.0 (EGSS), November, 1992.
- James M. Montgomery Consulting Engineers, Inc., 1993a, Remedial Options Letter Report, January, 1993.
- James M. Montgomery Consulting Engineers, Inc., 1993b, Draft Investigation Summary Report, UST Site 870, February, 1993.
- Jamison, V.W., Raymond, R.L., and Hudson, J.O. Jr., 1975, Biodegredation of high-octane gasoline in ground water: *Developments in Industrial Microbiology*, v. 16.

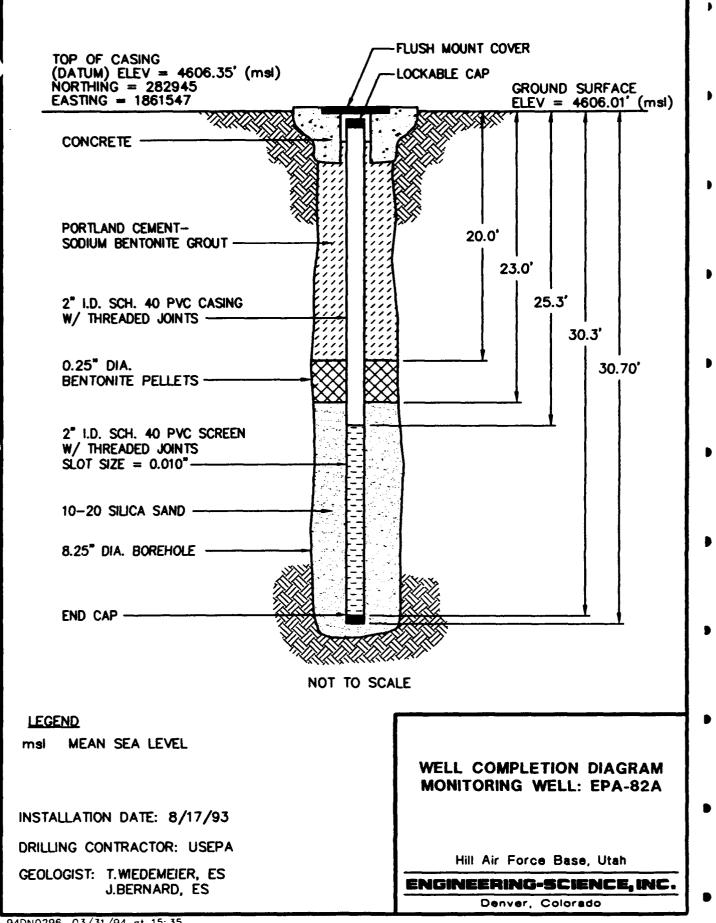
- Jones, J.G., and Eddington, M.A., 1968, An Ecological Survey of Hydrocarbon-Oxidizing Microorganisms. *Journal of General Microbiology*, 52:381-390.
- Jury, W.A., Spencer, W.F., and Farmer, W.J., 1984, Behavior Assessment Model for Trace Organics in Soil: III, Application of Screening Model. *Journal of Environmental Ouality*, 13(4):573-579.
- Kemblowski, M.W., and Chiang, C.Y., 1990, Hydrocarbon thickness fluctuations in monitoring wells: *Ground Water* v. 28, no. 2, p. 244-252.
- Konikow, L.F., and Bredehoeft, J.D., 1978, Computer model of two-dimensional solute transport and dispersion in ground water: *United States Geological Survey, Techniques of Water Resources Investigations of the United States Geological Survey*, Book 7, Chapter C2, 90 p.
- Lenhard, R.J., and Parker, J.C., 1990, Estimation of free hydrocarbon volume from fluid levels in monitoring wells: *Ground Water*, v. 28, no. 1, p. 57-67.
- Lovely, D.R., Baedecker, M.J., Lonergan, D.J., Cozzarelli, I.M., Phillips, E.J.P., and Siegel, D.I., 1989, Oxidation of aromatic contaminants coupled to microbial iron reduction: *Nature*, v. 339, p. 297-299.
- Lyman, W.J., Reidy, P.J., and Levy, B., 1992, Mobility and Degradation of Organic Contaminants in Subsurface Environments. C.K. Smoley, Inc., Chelsea, Michigan.
- Mcckay, D., and Wolkoff, A.W., 1973, Rate of Evaporation of Low-Solubility Contaminants from Water Bodies to Atmosphere. *Environmental Science and Technology*, 7(7):611-614.
- Mackay, D., and Shiu, W.Y., 1981, A Critical Review of Henry's Law Constants for Chemicals of Environmental Interest. *Journal of Physical Chemistry Reference Data*, 10(4):1175-1199.
- Martel, 1987, Military Jet Fuels 1944-1987: AF Wright Aeronautical Laboratories, Wright-Patterson Air Force Base, Ohio.
- Mercer, J.W., and Cohen, R.M., 1990, A review of immiscible fluids in the subsurface properties, models, characterization and remediation: *Journal of Contaminant Hydrology*, v.6, p. 107-163.
- Miller, R.N., Downey, D.C., Carmen, V.A., Hinchee, R.E., and Leeson, A., 1993, A summary of bioventing performance at multiple sites, In Proceedings of the Petroleum Hydrocarbons and Organic Chemicals in Ground Water: *Prevention, Detection, and Restoration Conference*: NWWA/API, p. 397 411.
- Miller, M.M., Wasik, S.P., Huang, G.L., Shiu, W.Y., and Mackay, D., 1985, Relationships Between Octanol-Water Partition Coefficient and Aqueous Solubility. *Environmental Science and Technology*, 19(6):522-529.
- Montgomery Watson, Inc., 1994a, Site Monitoring and Product Recovery Progress Letter Report.

- Montgomery Watson, Inc., 1994b, December 1993/January 1994 Quarterly Ground-Water sampling letter.
- Pankow, J.F., and Rosen, M.E., 1988, Determination of Volatile Compounds in Water by Purging Directly to a Capillary Column with Whole Column Cryotrapping. *Environmental Science and Technology*, 22(4):398-405.
- Perry, J.J., 1984, Microbial Metabolism of Cyclic Alkanes In R.M. Atlas (editor), Petroleum Microbiology. Macmillan Publishing Co., New York, New York.
- Ribbons, D.W., and Eaton, R.W., 1992, Chemical Transformations of Aromatic Hydrocarbons that Support the Growth of Microorganisms In Ralph Mitcheli (editor), Environmental Microbiology. Wiley-Liss, New York, New York.
- Rifai, H.S., Bedient, P.B., Wilson, J.T., Miller, K.M., and Armstrong, J.M., 1988, Biodegredation modeling at aviation fuel spill site: *Journal of Environmental Engineering*, v. 114, no. 5, p. 1007-1029.
- Rifai, H.S., 1995, Procedings of the 3rd Annual Batelle Conference, San Diego, CA, April, 1995. (To be published)
- Smith, J.H., Harper, J.C., and Jaber, H., 1981, Analysis and environmental fate of Air Force distillate and high density fuels: *Engineering & Services Laboratory*, Tyndall Air Force Base, Florida
- Testa, S.M., and Paczkowski, M.T., 1989, Volume determination and recoverability of free hydrocarbon: *Ground Water Monitoring Review*, Winter, 1989, p. 120-128.
- US Environmental Protection Agency, 1991, Role of the Baseline Risk Assessment in Superfund Remedy Selection Decisions. Memorandum from Don R. Clay, Assistant Administrator of the Office of Solid Waste and Emergency Response, OSWER Directive 9355.0-30.
- Valsaraj, K.T., 1988, On the Physio-Chemical Aspects of Partitioning of Non-Polar Hydrophobic Organics at the Air-Water Interface. *Chemosphere*, 17(5):875-887.
- Verschueren, K., 1983, Handbook of Environmental Data on Organic Chemicals. Van Nostrand Reinhold Co., New York, New York.
- von Gunten, U., and Zobrist, J., 1993, Biogeochemical changes in groundwater-infiltration systems Column Studies: Geochem. Cosmochim Acta, v.57, p. 3895-3906.
- Walton, W.C., 1988, Practical Aspects of Ground Water Modeling: National Water Well Association, Dublin, Ohio, 587 p.
- Wilson, B.H., Smith, G.B., and Rees, J.F., 1986, Biotransformations of Selected Alkylbenzenes and Halogenated Aliphatic Hydrocarbons in Methanogenic Aquifer Material: A Microcosm Study. *Environmental Science and Technology*, 20(10):997-1002.

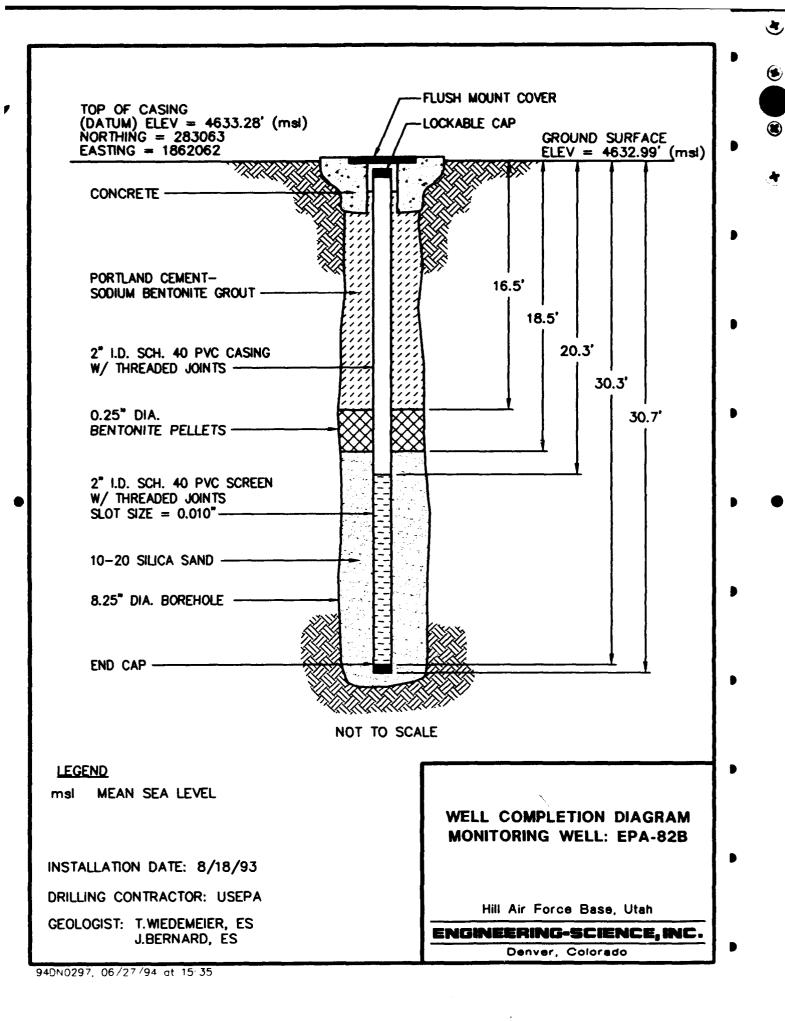
- Wilson, B.H., Wilson, J.T., Kampbell, D.H., Bledsoe, B.E., and Armstrong, J.M., 1990, Biotransformation of Monoaromatic and Chlorinated Hydrocarbons at an Aviation Gasoline Spill Site. *Geomicrobiology Journal*, 8:225-240.
- Wilson, J.T., 1994, Personal Communication, RE: nitrate-BTEX reactions in ground water, USEPA RSKERL.
- Wiedemeier, T.H., Downey, D.C., Wilson, J.T., Kampbell, D.H., Miller, R.N., and Hansen, J.E., 1994, Draft Technical Protocol for Implimenting the Intrinsic Remediation with Long-Term Monitoring Option for Natural Attenuation of Dissolved-Phase Fuel Contamination in Ground Water: Air Force Center for Environmental Excellence, Brooks Air Force Base, Texas.

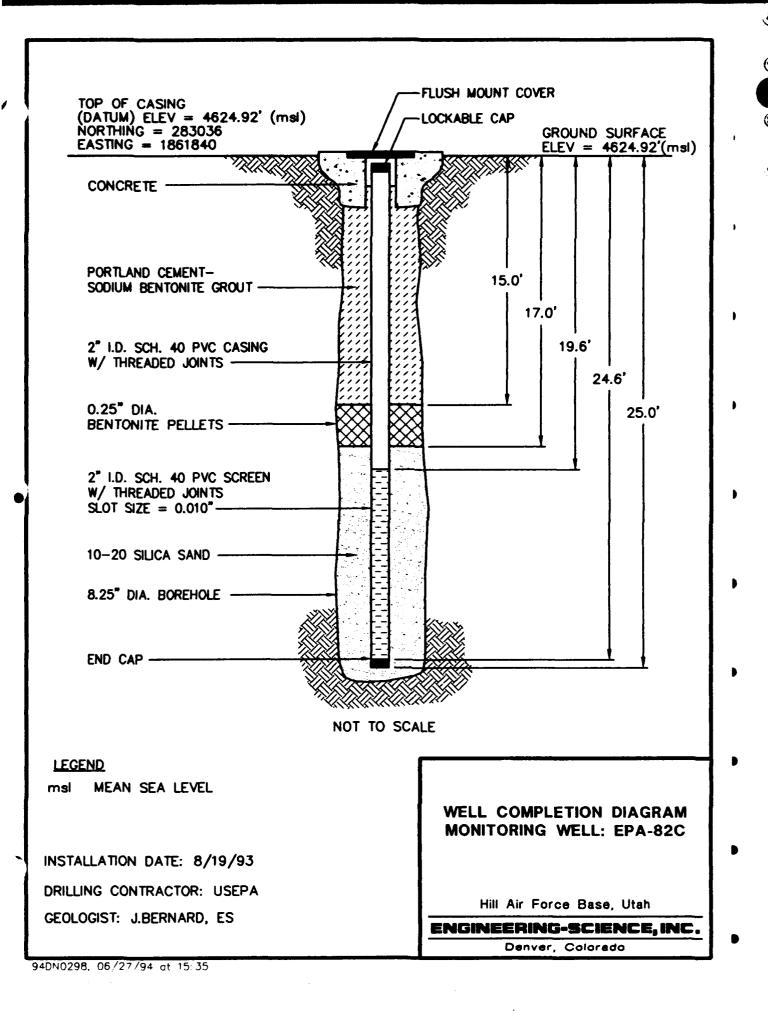
APPENDIX A

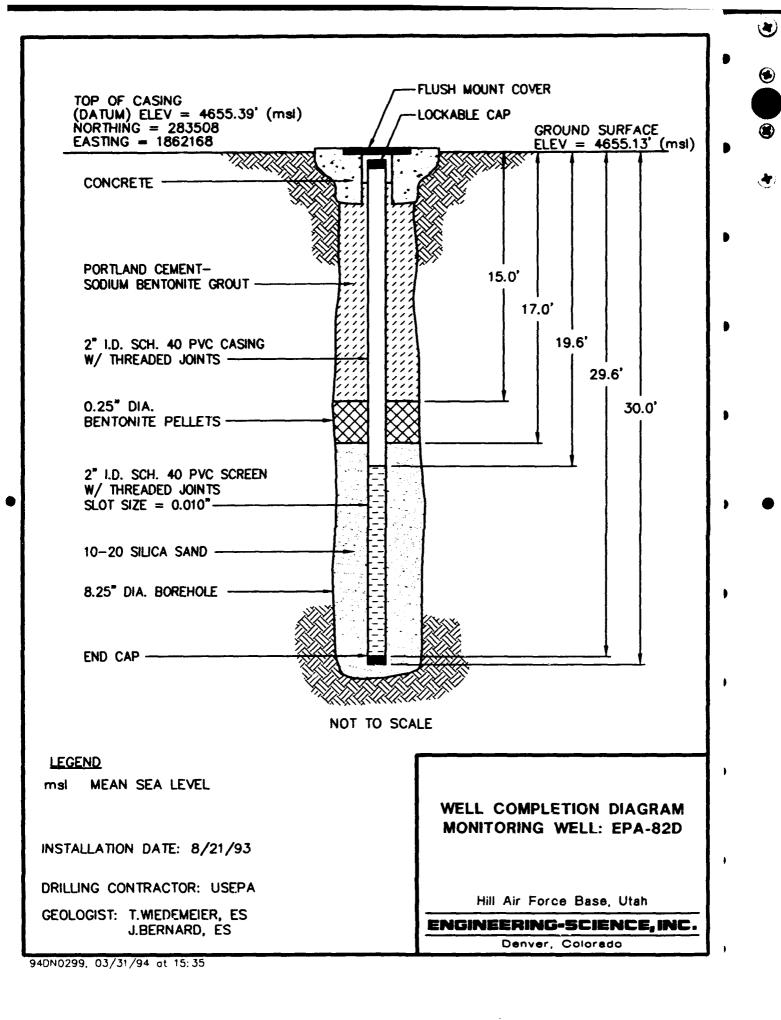
BORING LOGS, WELL COMPLETION DIAGRAMS, AND SLUG TEST RESULTS

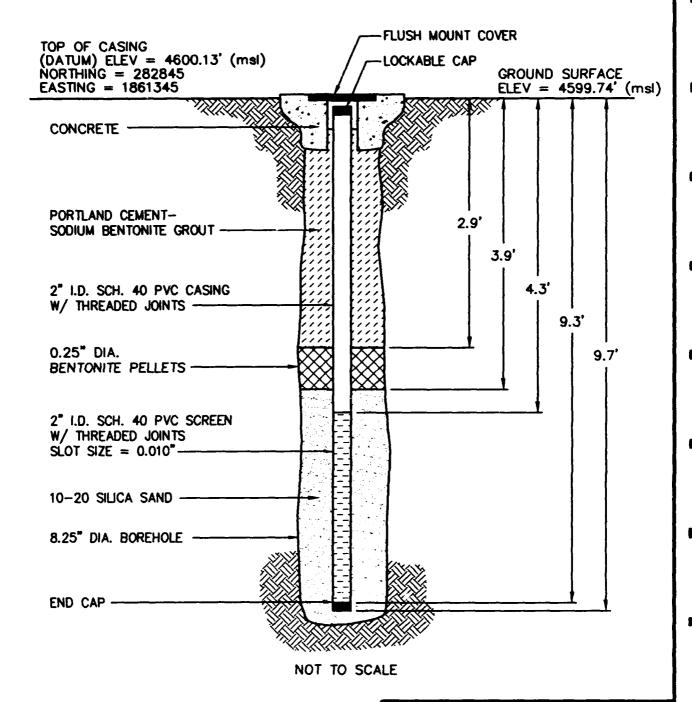


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LEGEND

msi MEAN SEA LEVEL

INSTALLATION DATE: 8/21/93

DRILLING CONTRACTOR: USEPA

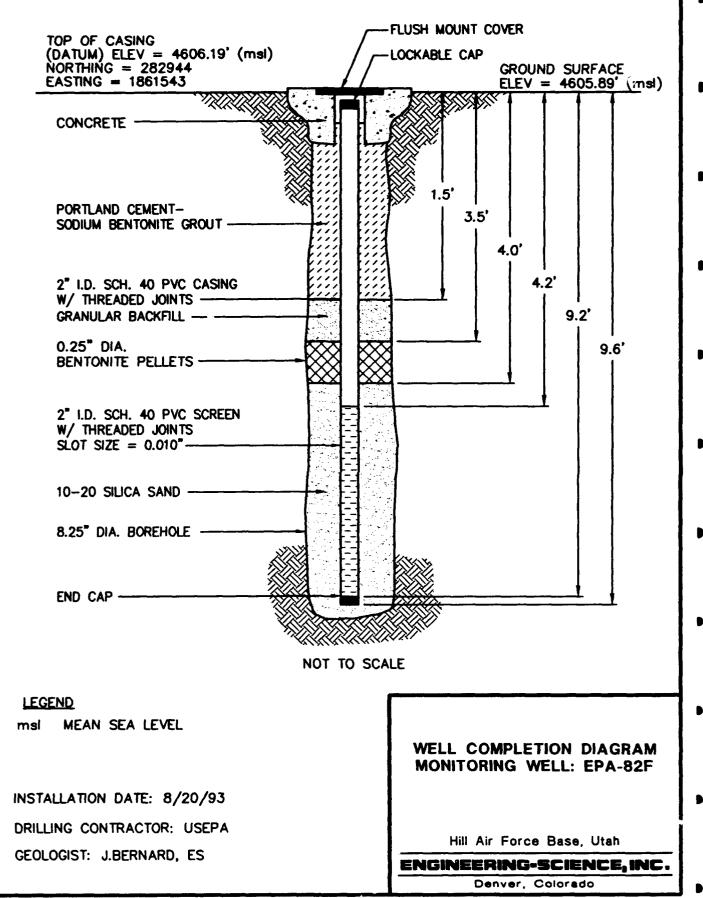
GEOLOGIST: J.BERNARD, ES

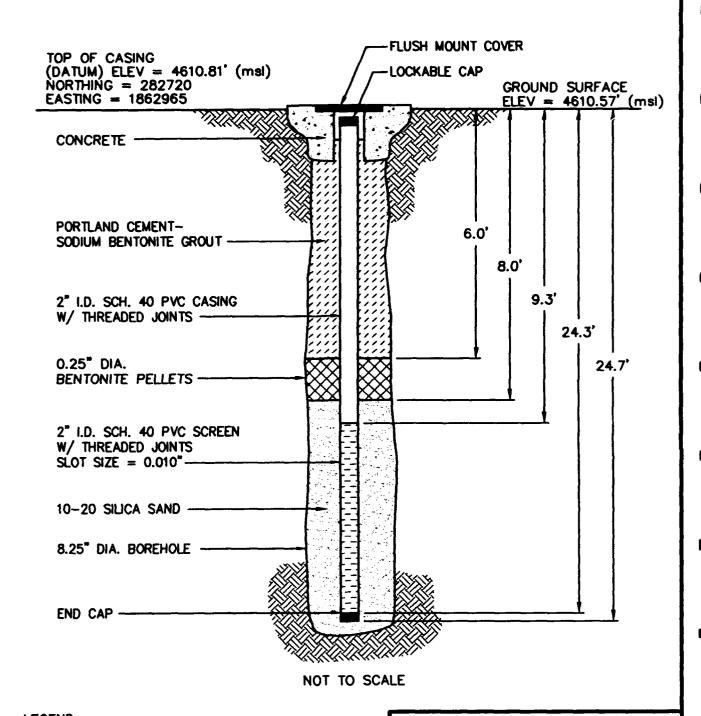
WELL COMPLETION DIAGRAM MONITORING WELL: EPA-82E

Hill Air Force Base, Utah

ENGINEERING-SCIENCE, INC.

Denver, Colorado





LEGEND

msl MEAN SEA LEVEL

INSTALLATION DATE: 8/22/93

DRILLING CONTRACTOR: USEPA

GEOLOGIST: T.WIEDEMEIER, ES

J.BERNARD, ES

WELL COMPLETION DIAGRAM MONITORING WELL: EPA-82H

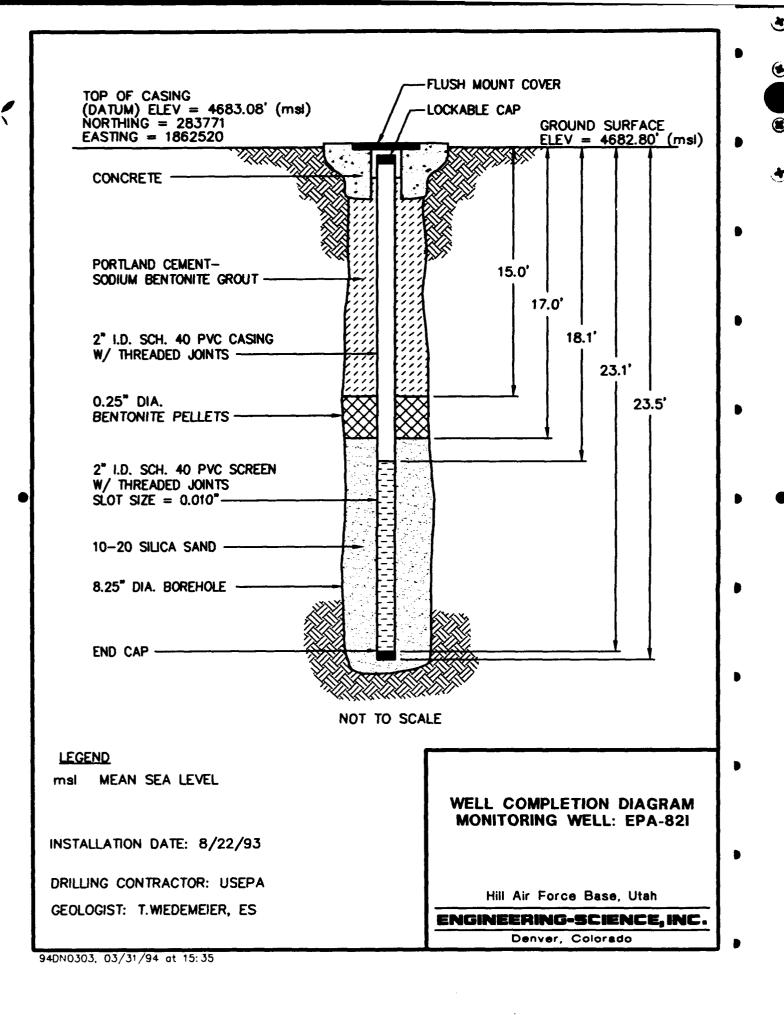
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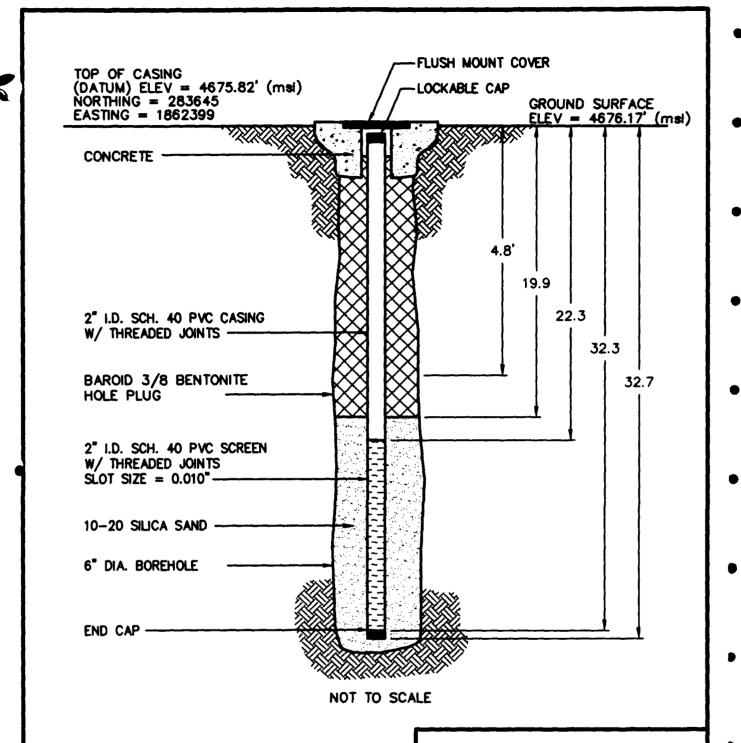
Hill Air Force Base, Utah

ENGINEERING-SCIENCE, INC.

Denver, Colorado

94DN0302, 03/31/94 at 15:35





LEGEND

msi MEAN SEA LEVEL

INSTALLATION DATE: 7/11/94

DRILLING CONTRACTOR: USEPA

GEOLOGIST: T. WEDEMEIER, ES

WELL COMPLETION DIAGRAM MONITORING WELL: EPA-82-J

Hill Air Force Base, Utah

ENGINEERING-SCIENCE, INC.

Denver, Colorado

Sheet 1 of 1

BORING NO.: EPA-82-A CONTRACTOR: USEPA 8/17/93 DATE SPUD: AFCEE CME-55 8/17/93 CLIENT: RIG TYPE: DATE CMPL.: DE311.02/722450.02 DRLG METHOD: HSA GS = 4606.01JOB NO.: **ELEVATION:** 8.25 HILL AFB 74 deg. F LOCATION: BORING DIA .: TEMP: THW/JFB NONE SUNNY DRLG FLUID:

GEOLOGIST: THW/JFB DRLG FLUID: NONE WEATHER: SUNNY

COMENTS: COMPLETED AS MONITORING WELL EPA-82-A, SCREENED FROM 25.3 TO 30.3 ft. bgs.

Elev	Depth	Pro-	US	I	П	Core	Sample	Penet	Γ		TOTAL	ĪРН
(ft)	(ft)	file	CS	Geologic Description	No.	Depth (ft				TLV(ppm)	BTEX(ppm)	(ppm)
	- 1 -	1500	SP	Asphalt to 0.5 ft. Well-sorted fine-grained sand Fill to 1.4 ft.								
			-		1				0_			
	<u> </u>	V/		Light-brown, clavey SILT, 25 to 35% clay, dry			.					
	L	V/	ML	Light-brown, clayey SiLT, 25 to 35% clay, dry semi-cohesive to cohesive, low plasticity, becomes damp ● ~4 ft. bgs.			1			<u> </u>		
	L 5 -			Social de la compact de la com	12	IV			0			
				tiakk aust ton fine to medium remined	_	$I \wedge$		N				
			SP	Light rust—ton, fine—to medium—grained moderately well sorted SAND. Becomes	_	$\langle - \rangle$	\cap	\cap				
				saturated at approx. 7ft. No hydrocarbon odor	3	$I \times$	\cup		0		<u></u>	
	\vdash					\leftarrow	Ν	T				
	10-					NS		'				
							1	١.,	0			
				<u> </u>	1	$I \setminus Z$	1	Μ				
					4	ΙX		lΕ				
	15		ľ		1	$V \setminus$	Ν	_				
	15-		ML	Light-brown, clavey SILT to silty CLAY with	l		'	Α				
			·**-	Light-brown, clayey SILT to silty CLAY with scattered 1/8 to 1 sand stringers, damp (probably saturated but low porosity)	5	$I \vee I$		ŀ	1.2			
				no hydrocarbon odor, cohesive	\cup	$1 \wedge$		S				
					•		\cup	111			<0.01	
	-20-	V/				Λ /	111	U			< 0.01	
		V/			$\overline{}$	$ \setminus / $	$ \cup $	R			< 0.01	
		Y //			0	ΙĂ	S		ļ		< 0.01	
	<u> </u>				ł	// \		E	l		< 0.01	
			SM	Rusty-brown poorly sorted SAND from 22.5 to 23.4ft.	l	$\langle - \rangle$			>1000		<0.01 <0.01	
	-25-	\leftarrow		Clayey SILT	7	IV		D	56		<0.01	
	\vdash			Light gravish-hown claves and sitty sec-	'	$ \wedge $			-		<0.01	
	\vdash		SM	Light grayish-brown, clayey and sitty very poorly-sorted, fine—to very—fine grained SAND, saturated, no hydrocarbon odor		$\langle \cdot \rangle$	\cap		2		< 0.01	
				SAND, aquarated, no hydrocarbon caor		$I \setminus Z$			-		<0.01	
		ازنز		29.5 to 33.5 interhedded clay silt and	8	ΙX	RI		8		< 0.01	
	-30-	\checkmark	ML SM	29.5 to 33.5 interbedded clay, silt and sand, dominated by tan to light rusty gray SILT, no hydrocarban odor. Rusty-brown		$V \setminus$					< 0.01	
		77	- SM	SAND Interbedded from 30.3 to 31.4 ft.	_		E		9		< 0.01	
		V/	ML		9	ΙX					< 0.01	
		1	<u> </u>	Con., bish plastick, CLAM	ľ	$V \setminus$					< 0.01	
	-35-		CL	Gray, high plasticity CLAY, no odor		<u> </u>					< 0.01	
				TD • 35.4 ft.		<u> </u>					< 0.01	

NOTES

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

NS - Not Sampled

SAA - Same As Above

SAMPLE TYPE

D - DRIVE

C - CORE

Sheet 1 of 1

BORING NO .: EPA-82-B

CONTRACTOR: USEPA

DATE SPUD: CME-55 DATE CMPL .: 8/18/93

CLIENT: JOB NO.:

AFCEE RIG TYPE: DE311.02/722450.02 DRLG METHOD: HSA

ELEVATION: 8.25"

8/18/93 GS = 4632.99

LOCATION: GEOLOGIST: HILL AFB BORING DIA.: THW/JFB DRLG_FLUID:

TEMP: NONE

85 deg. F

SUNNY

COMENTS:

WEATHER: COMPLETED AS MONITORING WELL EPA-82-B, SCREENED FROM 20.3 TO 30.3 ft. bgs

ſ	lev	Depth	Pro-	US			Core	Sample	Penet			TOTAL	TPH
L	(ft)	(ft)	file	CS	Geologic Description	No.	Depth (ft)	Туре	Res	PID(ppm)	TLV(ppm)	OTEX(ppm)	(ppm)
46	27.99	- 1 - - 5 -		M to L	Asphalt to 0.5 ft. Light reddish—brown, silty CLAY with laminations of silt. Slightly damp, no hydrocarbon odor	1		•		2			
46	22.99	-10-			Tan to reddish-brown, fine—to medium— grained moderately sorted SAND, no odor, damp	2		コスのい	ZOH	2			
46	17.99	-15-		SP		3	X	-Z	MEAS	2			
45	12.99	-20-			no odor becomes medium grained	5		$O \supset O$	U R	2		<0.01 <0.01 <0.01	
46	07.99	-25-			becomes medium—to coarse—grained becomes saturated ♥ ≈ 25' no odor	6		\circ	E D	2		<0.01 <0.01 <0.01 <0.01	
46	02.99	-30~		CL	Snarp contact light reddish-brown silty CLAY, cohesive		NS) R E		2		<0.01 <0.01	
		-35-			TD 32 feet								

NOTES

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

NS - Not Sampled

SAA - Same As Above

SAMPLE TYPE

D - DRIVE

C - CORE

Sheet 1 of 1

BORING NO.: EPA-82-C CONTRACTOR: USEPA 8/18/93 DATE SPUD: CME-55 8/18/93 AFCEE CLIENT: RIG TYPE: DATE CMPL .: DE311.02/722450.02 DRLG METHOD: HSA GS = 4624.92JOB NO.: ELEVATION: 8.25 HILL AFB 90 deg.F BORING DIA .: LOCATION: TEMP:

GEOLOGIST: THW/JFB DRLG FLUID: NONE WEATHER: SUN TO PARTLY CLDY COMENTS: COMPLETED AS MONITORING WELL EPA-82-C, SCREENED FROM 19.6 TO 24.6 ft. bgs

Elev	Depth	Pro-	US			Core	Sample	Penet			TOTAL	IPΗ
(ft)	(ft)	file	cs	Geologic Description					PID(ppm)	TLV(ppm)	BTEX(ppm)	
	- 1 -		SP	Asphalt to 0.5 ft. bgs Gravelly SAND fill					000			
4619.92	_		ML	Hard, dark gray clayey SILT	1	X			0			
	- 5 -		SM	Light brown, very poorly sorted fine—to very—fine—grained clayey (25%) and silty (20%), SAND, damp		$\langle \cdot \rangle$	С	\tilde{N}	26 31			
45.4.00			.		2	X	N	O	21 11 11			\exists
4614.92	-10-		ML	Light brown, clayey SILT, damp			T	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	14			
					3	X		M E	1 NS			
4609.92	-15-		SP	light reddish-brown fine-to medium- grained moderately sorted SAND, damp,			N_{\perp}	А	1 1			=
			55	no odorbecomes medium—to coarse—grained	4	X	0	S	NS NS			
4604.92	-20-			strong hydrocarbon odor, black hydrocarbon staining becomes saturated			U	UR	26 297 314		0.079 0.055 0.113	
			ML	Light reddish—brown, silty CLAY, cohesive, damp (probably saturated but low porosity) TD ② 24.0'	5	\triangle	S	E	12			<10
4599.95	-25-			10 0 2.10			C	D				
							0			_		
4594.92	-30-						R			-		
	-35-									_		

NOTES

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

NS - Not Sampled

SAA - Same As Above

SAMPLE TYPE

D - DRIVE

C - CORE

Sheet 1 of 1

BORING NO.: EPA-82-D CONTRACTOR: USEPA 8/18/93 DATE SPUD: CME-55 AFCEE 8/18/93 RIG TYPE: DATE CMPL .: CLIENT: DE311.02/722450.02 DRLG METHOD: HSA GS = 4655.13_ ELEVATION: JOB NO.: 8.25" HILL AFB 90 deg. F BORING DIA .: TEMP: LOCATION: THW/JFB NONE PARTLY CLOUDY **GEOLOGIST:** DRLG FLUID: WEATHER:

COMPLETED AS MONITORING WELL EPA-82-D, SCREENED FROM 19.6 TO 29.6 ft. bgs

Elev	Depth	Pro-	US			Core		Penet			TOTAL	ТРH
(ft)	(ft)	file	CS	Geologic Description	Ño.	Depth (ft)	Туре	Res	PID(ppm)	TLV(ppm)	BTEX(ppm)	(ррт)
	- 1 -		SP	Asphalt to 0.5 ft, Well Sorted Fine Sana					0			
				Fill to 1.4 ft		\setminus			0		L	
				Brown, clayey and sandy SILT, interbedded	1	$\mid \vee \mid$		ĺ	0			
				thin red clay layers and thin poorly		$L \wedge I$			0		L	
650.13				sorted very-fine-grained sand layers		I / \			0			
		<i>Y//</i>					C	N	0			
						Λ	(0			
			ML		2	$\Gamma \vee \Gamma$	$ \cup $	\cup	0_			
					_	$ \wedge $	N I	l -	0			
645.13	-10-					\angle			0			
		///			Ì		_		0_			
					l _	$ \setminus / $		1	0			
					13	ΙXΙ	1	M	0			
					~	$I / \setminus I$	l l	lΕ	0			
640.13	-15-				1	/_ \	N	<u> </u>	0			
	L12-				l		1 1	Α	0			
				Reddish-brown, poorly to moderately	<i>A</i>	$ \vee $			0			
				sorted, fine— to medium—grained SAND, no hydrocarbon odor, damp	4	$I \wedge I$		IS.	0			
			SP	no nyarocarbon odor, admp		V. N	()		0			
635.13	20			Black hydrocarbon staining, moderate	ł	NS		\cup	NS			
	-20-			petroleum hydrocarbon odor			U		1		< 0.01	<1
					_ ا	$ \vee $		IR	1		<0.023	<1
				becomes saturated	5	$1 \wedge 1$	S	F	199		0.635	<10
		777		Reddish-brown, clayey SILT to silty CLAY,	_	$V \setminus$					3.022	
630.13	25	<i>Y//</i>		saturated. Contains scattered interbeds of				\Box	282		0.087	
	-25-			clay and very fine-grained sand	۱,	$ \setminus \rangle $		\cup	29		0.237	<10
				, , ,	6	$I \wedge I$			25		0.244	
			ML		i	$V \setminus V$	()		27		0.270	
							~		20			
625.13	7,				_	$ \setminus / $	RI		42			
	-30-				/	X			33			
						$V \setminus V$	E		11			
		 						i '				
		'		TD 9 32 ft								
								1				
	-35-		Ī		ĺ							

NOTES

COMENTS:

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

NS - Not Sampled

SAA - Same As Above

SAMPLE TYPE

D - DRIVE

C - CORE

Sheet 1 of 1

BORING NO.: EPA-82-E CONTRACTOR: USEPA 8/21/93 _ DATE SPUD: AFCEE CME-55 8/21/93 CLIENT: RIG TYPE: DATE CMPL.: DE311.02/722450.02 DRLG METHOD: HSA GS = 4599.74JOB NO.: _ ELEVATION: 8.25 HILL AFB 72 deg. F LOCATION: BORING DIA .: _ TEMP:

GEOLOGIST: THW/JFB DRLG FLUID: NONE WEATHER: PARTLY CLOUDY
COMENTS: COMPLETED AS MONITORING WELL EPA-82-E, SCREENED FROM 4.3 TO 9.3 ft. bgs

Elev	Depth	Pro-	US			Core	Sample				TOTAL	TPH
(ft)	(ft)	file	cs	Geologic Description	No.	Depth (ft)	Туре	Res	PtD(ppm)	TLV(ppm)	BTEX(ppm)	(ppm)
	- 1 -			Asphalt to 0.3 ft		/			3			
1				0.3 to 2.0 ft sandy and gravelly FILL		1\ /			1		<0.01	
)				Light brown,moderately—sorted, fine—to	١.	IV			1		<0.01	
			SP	medium-grained SAND, saturated,	11	$1 \wedge$			1		<0.01	
4594.74	- 5 -			no odor	·	1/\		١	1		< 0.01	
)				becomes coarse—grained		<u> </u>	C	N	1		< 0.01	
		///			15	\mathbb{Z}			1		< 0.01	
			ML	Light-brown, clayey SILT to silty CLAY,	12	IX	\cup	0	3		< 0.01	
			ML	cohesive, saturated, no odor	1		Ν	Τ	2		< 0.01	
4589.74	-10-			,		Λ	1 /	ı	1		<0.01	
	\vdash				13	$I \times I$			<u> </u>			
1	\vdash			TD @ 10.5 feet	1	$1/\lambda$	1.'	M				
1	\vdash			15 & 10.5 1660	ļ	<u> </u>		i				
		1				1	NI	E	 	<u> </u>		{
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NOTES

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

NS - Not Sampled

SAA - Same As Above

SAMPLE TYPE

D - DRIVE

C - CORE

Sheet 1 of 1

BORING NO .: EPA-82-F CONTRACTOR: USEPA 8/21/93 DATE SPUD: 8/21/93 AFCEE CME-55 RIG TYPE: DATE CMPL.: CLIENT: DE311.02/722450.02 DRLG METHOD: HSA GS = 4605.89JOB NO.: **ELEVATION:** 8.25" HILL AFB 90 deg. F LOCATION: BORING DIA .: TEMP: THW/JFB NONE PARTLY CLOUDY GEOLOGIST:

GEOLOGIST: THW/JFB DRLG FLUID: NONE WEATHER: PARTLY CLOUDY
COMENTS: COMPLETED AS MONITORING WELL EPA-82-F, SCREENED FROM 4.2 TO 9.2 ft. bgs

Elev	Depth	Pro-	US			Care	Sample	Penet			TOTAL	ĪРН
(ft)	(ft)	file	cs	Geologic Description	No.	Depth (ft)	Туре	Res	PID(ppm)	TLV(ppm)	BTEX(ppm)	(ррт)
	- 1 <i>-</i>											
												
4600,89	- 5 -											
			1									
4595,89	-10-	L		See Boring Log EPA-82-A TD @ 10'								
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	-13-											
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NOTES

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

NS - Not Sampled

SAA - Same As Above

SAMPLE TYPE

D - DRIVE

C - CORE

Sheet 1 of 1

BORING NO.: EPA-82-H CONTRACTOR: USEPA 8/21/93 DATE SPUD: CME-55 8/21/93 AFCEE RIG TYPE: CLIENT: DATE CMPL .: DE311.02/722450.02 DRLG METHOD: HSA GS=4610.57 JOB NO.: **ELEVATION:** 8.25 HILL AFB 74 deg. F BORING DIA.: LOCATION: TEMP:

NONE THW/JFB SUNNY THW/JFB DRLG FLUID: NONE WEATHER: SUNNY

COMPLETED AS MONITORING WELL EPA-82-H, SCREENED FROM 9.3 TO 24.3 ft. bgs **GEOLOGIST:** COMENTS:

	Depth	Pro-	US				Sample		Γ		TOTAL	TPH
(ft)	(ft)	file	cs	Geologic Description	No.	Depth (ft)	Туре	Res	P10(ppm)	TLV(ppm)	BTEX(ppm)	(ppm)
	- 1 -		SP	Asphalt to 0.6 ft FILL to 2.5 ft	1							
4605.57	- 5 -		ML	Light—brown, dry, crumbly silty clay. No odor present			С	N				
4600.57	-10-			Light reddish-brown, moderately-sorted, fine-to medium-grained SAND, damp, no hydrocarbon odorbecomes saturated	2		0 0 Z F	0 T				
4595.57	-15-		SP	becomes saturated	3	\bigcirc	Z _	M E A				
4590.57	-20-			becomes coarse-grained	4 5	\bigcirc	$O \cup S$	SURL				
4585.57	-25-			Interbedded, light reddish-brown interbedded clay, silt, and sand	6	X	C	E D				
<u>4580.57</u>	-30-			TD @ 31 feet	7	X	R E					
	-35-							!				

NOTES

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

NS - Not Sampled

SAA - Same As Above

SAMPLE TYPE

D - DRIVE

C - CORE

Sheet 1 of 1

BORING NO .: EPA-82-I CONTRACTOR: USEPA 8/22/93 _ DATE SPUD: AFCEE CME-55 8/22/93 CLIENT: RIG TYPE: _ DATE CMPL .: DE311.02/722450.02 DRLG METHOD: HSA GS = 4682.80JOB NO.: _ ELEVATION: 8.25" HILL AFB 82 deg. F LOCATION: BORING DIA.: TEMP: THW/JFB NONE SUNNY **GEOLOGIST:**

GEOLOGIST: THW/JFB DRLG FLUID: NONE WEATHER: SUNNY

COMENTS: COMPLETED AS MONITORING WELL EPA-82-I, SCREENED FROM 18.1 TO 23.1 ft. bgs

Elev	Depth	Pro-	US		Т	Core	Sample	Penet]	Τ	TOTAL	TPH
(ft)	(ft)	file	CS	Geologic Description	No.	Depth (ft)	Туре	Res	PiD(ppm)	TLV(ppm)	BTEX(ppm)	(ppm)
	- 1 -			Clayey and gravelly SAND fill to 2.0 ft Light reddish~brown sandy silt,	1				NS 0 90 1			
4677.80	- 5 -		ML	damp, weak hydrocarbon odor	2		0	<i>Z</i> 0	1 1 31			
4672.80	-10-			Light reddish-brown, poorly sorted, medium to coarse-grained SAND, damp, weak hydrocarbon odor	3		Z	Т М	2 3 2 3 2			
4667.80	-15-		SP	Free—and residual—phase contamination begins at 16.3 feet. Dark hydrocarbon discoloration. Strong odor at 17.0 feet	4		$Z \supset C$	E A S	3 4 81 257		0.005 0.004 105.4 119.4	11500 28300
4662.80	-20-			becomes saturated @ ≈ 18'	5))) S	URE	150 397 176 103 357		551.3 14 7.37 26.2 20.2	<10 276 643 340
4657.80	-25-		ML	Light brown, clayey SILT to silty CLAY	6		CO	D	239 311 239 252		16.1 27.11 4.163	<10 <10 410 <10
4652.80	-30 -			TD @ 27 feet			R E					
	-35-											

NOTES

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

NS - Not Sampled

SAA - Same As Above

SAMPLE TYPE

D - DRIVE

C - CORE

GEOLOGIC BORING LOG Sheet 1 of 1 BORING NO.: EPA-82-J CONTRACTOR: USEPA RSKERL DATE SPUD: 7/9/94 7/11/94 AFCEE **GIDDINGS** RIG TYPE: CLIENT: _ DATE CMPL.: DE311.02/722450.02 DRLG METHOD: HSA _ ELEVATION: JOB NO.: HILL AFB 97 deg. F LOCATION: BORING DIA.: TEMP: TODD MEDEMEIER DRLG FLUID: NONE

COMPLETED AS EPA-82J (MONITORING WELL)

3

CLEAR & HOT

. WEATHER:

	Depth	Pro-	US				Sample				TOTAL	TPH
(ft)	(ft,	file	cs	Geologic Description	No.	Depth (ft)	Туре	Res	PID(ppm)	TLV(ppm)	BTEX(ppm)	(ppm)
	- 1 -		ML	Dark reddish brown, very poorly sorted clay and silty. Very fine grained SAND to clayey & sandy silt. Damp. No hydrocaron odor	1 2 3	NS	HZOO	Z O T Z	0			
·	-15-		SP ML	fine-grained SAND. Damp. No hydrocaron odor Clay-rich fine-grained sand • 13.5-16.5'. No hydrocarbon odor. Damp.	4	$\langle \rangle$	_ Z =	N E A	0000			
!	-20-		SP	Lighter reddish brown to brown, moderately well sorted, fine— to medium—grained SAND. Damp. No hydrocarbon. becomes medium grained.	5 6	\bigvee	$\mathcal{O} \subset \mathcal{O} \subset$	SUR	0 0 0 0		<0.01 <0.01 <0.01 <0.01	
	-25-		SP to SM	becomes saturated © 25' bgs becomes fine grained with minor clay & some silt, saturated.	7) ()	ED	0 0 0 0 2153 1897		<0.01 <0.01	
	-30-		CL	strong hydrocarbon odor. Sharp contact into brown, clayey SILT to silty CLAY. Cohesive. Faint hydrocaron odor. Saturated. TD @32.3 feet	8	X) R E		1594 1555 175			

NOTES

GEOLOGIST:

COMENTS:

bgs - Below Ground Surface

GS - Ground Surface

TOC - Top of Casing

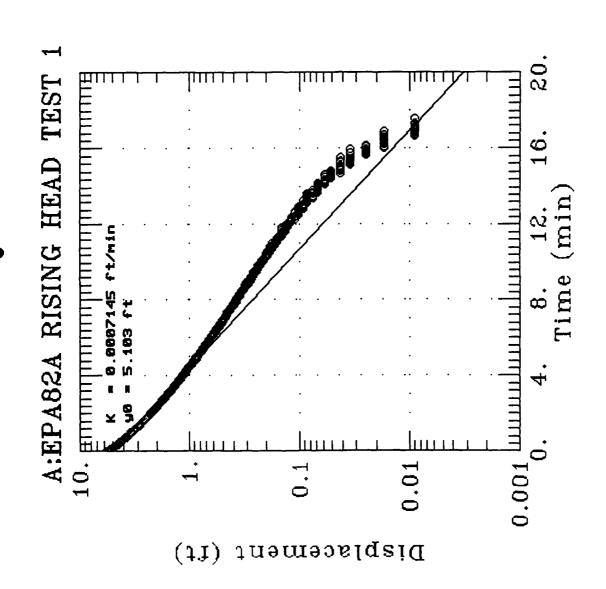
NS - Not Sampled

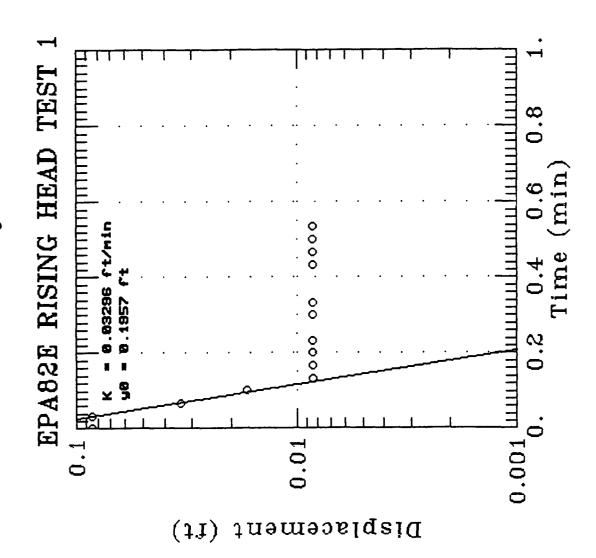
SAA - Same As Above

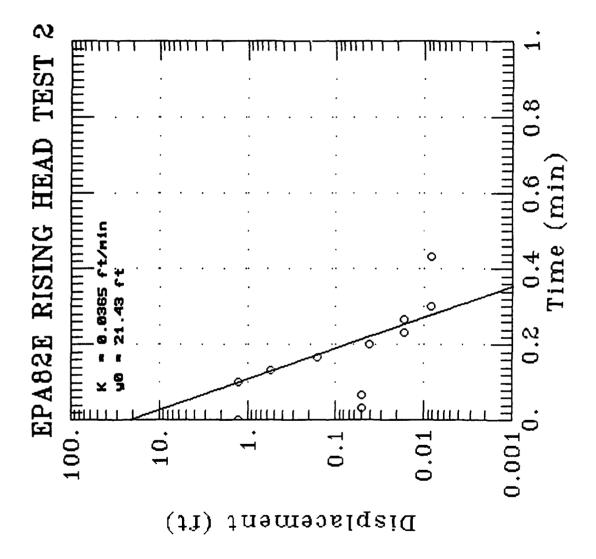
SAMPLE TYPE

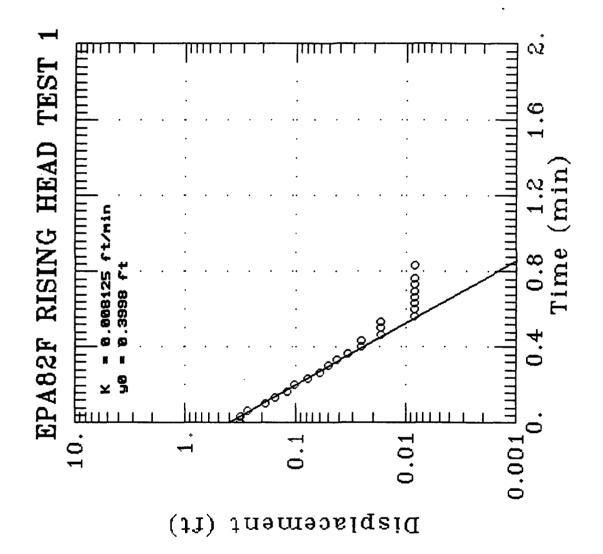
D - DRIVE

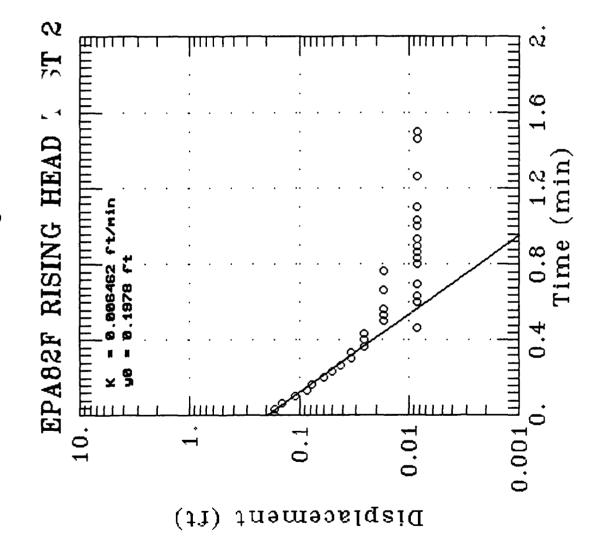
C - CORE

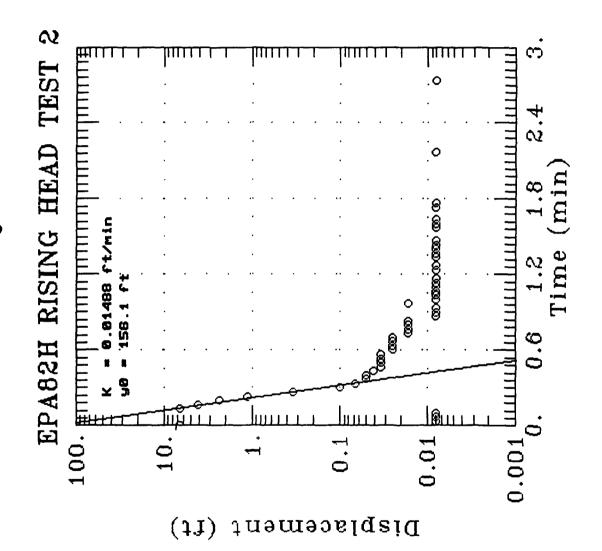


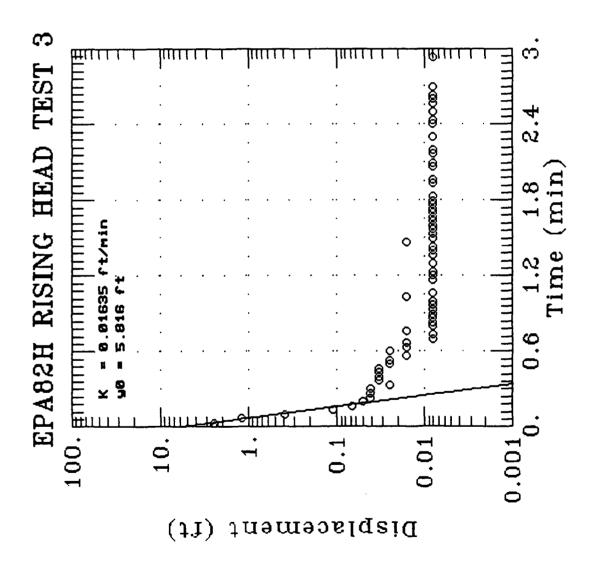


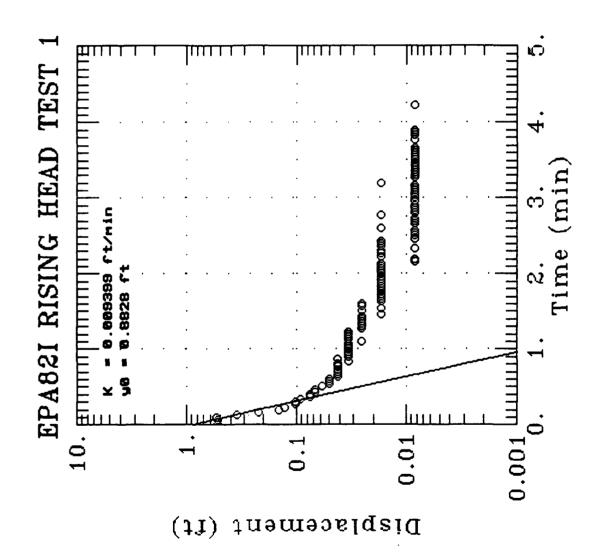


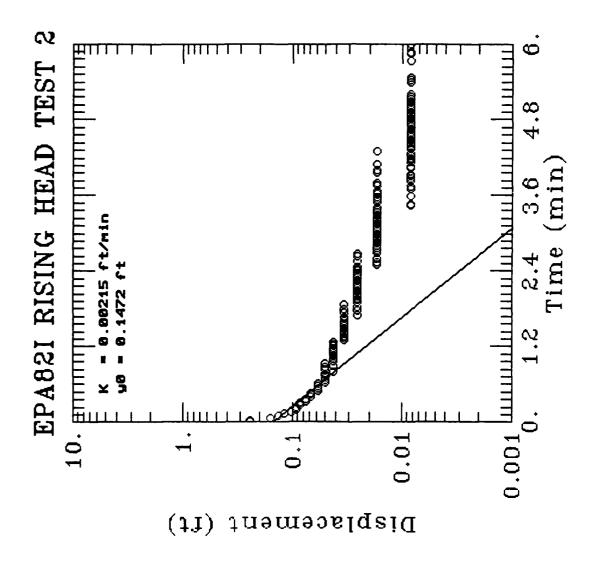












HILL AIR FORCE BASE SLUG TEST ANALYSES DE311.02.02

EPA82IR2	0.0833	0.3438	4.7	*	4.7	
EPA82IR1	0.0833	0.3438	4.7	~	4.7	
EPA82HR3	0.0833	0.3438	13.35	15	13.35	
EPA82HR2	0.0833	0.3438	13.35	15	13.35	
EPA82HR1	0.0833	0.3438	13.35	15	13.35	
EPA82FR2	0.0833	0.3438	3.17	\$	3.17	
EPA82FR1	0.0833	0.3438	3.17	8	3.17	
EPA82ER2	0.0833	0.3438	7.	80	7.	
EPA82ER1	0.0833	0.3438	4.4	8	4.4	
EPA82AR1 E	0.0833	0.3438	25.55	~	25.55	
PARAMETER	Int. displace. Casing radius	Well radius	Sat. Thickness	Screen length	Height of water	in well

(3)

GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(fi msl)	(ft BTOC)	(# BTOC)	(feet)	(ft BTOC)	(fl mst)
CPT-2	12/28/93	SDNA	SDNA	SDNA	26.98	18.58	8.40	20.68	NA
	1/20/94	SDNA	SDNA	SDNA	26.50	20.82	5.68	22.24	AN
	2/3/94	SDNA	SDNA	SDNA	26.95	21.16	5.79	22.61	A'N
	2/17/94	SDNA	SDNA	SDNA	26.83	21.23	9.60	22.63	A'N
	3/3/94	SDNA	SDNA	SDNA	76.99	21.59	5.40	22.94	AN
	3/17/94	SDNA	SDNA	SDNA	26.78	21.55	5.23	22.86	٧X
	3/31/94	SDNA	SDNA	SDNA	26.79	21.79	5.00	23.04	NA AN
	4/14/94	SDNA	SDNA	SDNA	26.80	21.78	5.02	23.04	A'N
CPT-3	12/28/93	SDNA	SDNA	SDNA	21.41		00:00	21.41	AN
	1/20/94	SDNA	SDNA	SDNA	21.45	21.00	0.45	21.11	Ϋ́
	2/3/94	SDNA	SDNA	SDNA	21.34	21.19	0.15	21.23	AN
	2/17/94	SDNA	SDNA	SDNA	21.27	21.12	0.15	21.16	YZ V
	3/3/94	SDNA	SDNA	SDNA	21.72	21.71	0:01	21.71	A'N
	3/17/94	SDNA	SDNA	SDNA	21.74	•	00:0	21.74	Ϋ́
	3/31/94	SDNA	SDNA	SDNA	21.80	•	00:00	21.80	AZ
	4/14/94	SDNA	SDNA	SDNA	21.91	•	00:00	21.91	NA
CPT-4	12/28/93	SDNA	SDNA	SDNA	22.83		0.00	22.83	NA
	1/20/94	SDNA	SDNA	SDNA	22.97	•	0.00	22.97	NA
	2/3/94	SDNA	SDNA	SDNA	22.90	•	0.00	22.90	NA
	2/17/94	SDNA	SDNA	SDNA	22.83	•	00:00	22.83	ΑX
	3/3/94	SDNA	SDNA	SDNA	23.26		00:00	23.26	¥Z.
	3/17/94	SDNA	SDNA	SDNA	23.26	•	00'0	23.26	A'N
	3/31/94	SDNA	SDNA	SDNA	23.36	•	0.00	23.36	Y.
	4/14/94	SDNA	SDNA	SDNA	23.51	•	0.00	23.51	A'A
CPT-6	12/28/93	SDNA	SDNA	SDNA	20.58	•	00'0	20.58	Ϋ́Α
	1/20/94	SDNA	SDNA	SDNA	20.76	•	00'0	20.76	Ϋ́
	2/3/94	SDNA	SDNA	SDNA	20.87	•	00.00	20.87	٧X
	3/3/94	SDNA	SDNA	SDNA	21.27	•	00.0	21.12	Ϋ́
	3/17/94	SDNA	SDNA	SDNA	21.00	•	00.0	21.00	YZ.
	3/31/94	SDNA	SDNA	SDNA	21.32	•	0.00	21.32	٧X
	4/14/94	SDNA	SDNA	SDNA	21.21	•	00.00	21.21	ΥN
CPT-7	8/18/92	2547.88	3772.45	4684.21	21.69	•	0.00	21.69	4662.52
	4/21/93	2547.88	3772.45	4684.21	19.74	•	00:0	19.74	4664.47

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9/20/94

GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(ft msl)	(ft BTOC)	(ft BTOC)	(feet)	(# BTOC)	(fi msl)
	4/29/93	2547.88	3772.45	4684.21	19.45	•	0.00	19.45	4664.76
	8/9/3	2547.88	3772.45	4684.21	19.33	•	00.00	19.33	4664.88
	5/20/93	2547.88	3772.45	4684.21	18.69	•	0.00	69'81	4665.52
	6/11/93	2547.88	3772.45	4684.21	19.96		0.00	96.61	4664.25
	6/23/93	2547.88	3772.45	4684.21	20.00	17.10	2.90	17.83	4666.39
	7/1/93	2547.88	3772.45	4684.21	20.44	17.54	2.90	18.27	4665.95
	7/8/93	2547.88	3772.45	4684.21	20.51	16.51	4.00	17.51	4666.70
	1/20/94	2547.88	3772.45	4684.21	23.48	19.00	4.48	20.12	4664.09
	2/3/94	2547.88	3772.45	4684.21	23.85	19.70	4.15	20.74	4663.47
	2/17/94	2547.88	3772.45	4684.21	23.70	19.99	3.71	20.92	4663.29
	3/3/94	2547.88	3772.45	4684.21	23.85	19.90	3.95	20.89	4663.32
	3/17/94	2547.88	3772.45	4684.21	23.85	19.85	4.00	20.85	4663.36
	3/31/94	2547.88	3772.45	4684.21	23.45	19.45	4.00	20.45	4663.76
	4/14/94	2547.88	3772.45	4684.21	23.35	20.32	3.03	21.08	4663.13
CPT-9	1/20/94	SDNA	SDNA	SDNA	DRY	•	0.00	DRY	NA
	3/17/94	SDNA	SDNA	SDNA	DRY	•	00:00	DRY	AN
	3/31/94	SDNA	SDNA	SDNA	DRY	•	0.00	DRY	NA
CPT-10	8/18/92	2602.28	3772.04	4686.54	22.10	•	00:00	22.10	4664.44
	4/21/93	2602.28	3772.04	4686.54	19.50	•	0.00	19.50	4667.04
	4/29/93	2602.28	3772.04	4686.54	19.50	•	0.00	19.50	4667.04
	5/6/93	2602.28	3772.04	4686.54	19.35	•	0.00	19.35	4667.19
	5/20/93	2602.28	3772.04	4686.54	19.06	18.16	06:0	18.39	4668.16
	6/11/93	2602.28	3772.04	4686.54	19.10	•	0.00	19.10	4667.44
	6/23/93	2602.28	3772.04	4686.54	19.00	17.70	1.30	18.03	4668.52
	7/1/93	2602.28	3772.04	4686.54	18.94	17.34	1.60	17.74	4668.80
	7/8/93	2602.28	3772.04	4686.54	19.10	16.60	2.50	17.23	4669.32
	1/20/94	2602.28	3772.04	4686.54	21.43	18.35	3.08	19.12	4667.42
	2/3/94	2602.28	3772.04	4686.54	21.51	21.36	0.15	21.40	4665.14
	2/17/94	2602.28	3772.04	4686.54	21.48	21.31	0.17	21.35	4665.19
	3/3/94	2602.28	3772.04	4686.54	21.73	21.02	0.71	21.20	4665.34
	3/17/94	2602.28	3772.04	4686.54	21.58	21.00	0.58	21.15	4665.40
	3/31/94	2602.28	3772.04	4686.54	21.60	20.00	1.60	20.40	4666.14
	4/14/94	2602.28	3772.04	4686.54	21.50	16.50	5.00	17.75	4668 79

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9/20/94

GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
cocation	Date	Easting	Northing	(fl msl)	(# BTOC)	(A BTOC)	(feet)	(ft BTOC)	(fl msl)
CPT-11	12/28/93	SDNA	SDNA	SDNA	25.57	•	0.00	25.57	NA
	1/20/94	SDNA	SDNA	SDNA	25.82		0.00	28.82	NA
	2/3/94	SDNA	SDNA	SDNA	25.91	•	00:0	16'57	ΥN
	2/17/94	SDNA	SDNA	SDNA	27.94		0.00	27.94	AN
	3/3/94	SDNA	SDNA	SDNA	26.40		00:0	26.40	NA AN
	3/17/94	SDNA	SDNA	SDNA	26.47	•	00:0	26.47	ΥN
	3/31/94	SDNA	SDNA	SDNA	26.69		00:0	26.69	AN.
	4/14/94	SDNA	SDNA	SDNA	27.00		00:0	27.00	ΥN
CPT-13	1/20/94	SDNA	SDNA	SDNA	DRY	4	0.00	DRY	A'A
	3/17/94	SDNA	SDNA	SDNA	DRY	1	00:0	DRY	Ϋ́Z
	3/31/94	SDNA	SDNA	SDNA	DRY		00:0	DRY	NA
CPT-14	8/18/92	2182.60	3507.60	4655.88	25.38		0.00	25.38	4630.50
	3/4/93	2182.60	3507.60	4655.88	27.08	24.57	2.51	25.20	4630.68
	3/18/93	2182.60	3507.60	4655.88	27.16	24.66	2.50	25.29	4630.60
	4/2/93	2182.60	3507.60	4655.88	27.34	23.60	3.74	24.54	4631.35
	4/29/93	2182.60	3507.60	4655.88	27.32	23.32	4.00	24.32	4631.56
;	8/9/5	2182.60	3507.60	4655.88	26.98	22.98	4.00	23.98	4631.90
	5/20/93	2182.60	3507.60	4655.88	26.72	23.22	3.50	24.10	4631.79
	6/11/93	2182.60	3507.60	4655.88	27.53	24.03	3.50	16'72	4630.98
	6/23/93	2182.60	3507.60	4655.88	26.00	23.00	3.00	23.75	4632.13
	7/1/93	2182.60	3507.60	4655.88	26.80	23.80	3.00	24.55	4631.33
	7/8/93	2182.60	3507.60	4655.88	25.35	22.85	2.50	23.48	4632.41
	8/23/93	2182.60	3507.60	4655.88	23.50	•	0.00	23.50	4632.38
	12/28/93	2182.60	3507.60	4655.88	24 88	23.00	1.88	23.47	4632.41
	1/20/94	2182.60	3507.60	4655.88	25.40	23.49	16.1	23.97	4631.91
	2/3/94	2182.60	3507.60	4655.88	25.64	23.64	2.00	24.14	4631 74
	2/17/94	2182.60	3507.60	4655.88	25.73	23.58	2.15	24.12	4631.76
	3/3/94	2182.60	3507.60	4655.88	25.66	23.86	1.80	24.31	4631.57
	3/17/94	2182.60	3507.60	4655.88	25.85	24.45	1.40	24.80	4631.08
	3/31/94	2182.60	3507.60	4655.88	25.37	24.87	0.50	25.00	46 189
	4/14/94	2182.60	3507.60	4655.88	26.07	24.27	1.80	24.72	
CPT-15	8/18/92	2262.51	2985.53	4638.74	32.97	•	0.00	32.97	4605.77
	1/4/03	13 6966	2985 53	46 38 74	33.85		000	33.04	00 1071

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GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(fi msl)	(ft BTOC)	(f) BTOC)	(feet)	(it BTOC)	(frmst)
	4/2/93	2262.51	2985.53	4638.74	33.50	•	0.00	33.50	4605.24
	4/29/93	2262.51	2985.53	4638.74	32.67		0.00	32.67	4606.07
	8/9/8	2262.51	2985.53	4638.74	32.50	•	00:00	32.50	4606.24
	5/20/93	2262.51	2985.53	4638.74	32.18	•	0.00	32.18	4606.56
	6/17/93	2262.51	2985.53	4638.74	31.73	•	0.00	31.73	4607.01
	6/23/93	2262.51	2985.53	4638.74	31.66	•	0.00	31.66	4607.08
	7/1/93	2262.51	2985.53	4638.74	31.56		00:00	31.56	4607.18
	7/8/93	2262.51	2985.53	4638.74	31.45	•	00:00	31.45	4607.29
	1/20/94	2262.51	2985.53	4638.74	32.25	•	00:00	32.25	4606.49
	2/3/94	2262.51	2985.53	4638.74	32.55		00'0	32.55	4606.19
	2/17/94	2262.51	2985.53	4638.74	32.85	•	00:00	32.85	4605.89
	3/3/94	2262.51	2985.53	4638.74	33.05	•	00:00	33.05	4603.69
	3/17/94	2262.51	2985.53	4638.74	33.28	•	00:00	33.28	4605.46
	3/31/94	2262.51	2985.53	4638.74	33.44	•	00:0	33.44	4605.30
	4/14/94	2262.51	2985.53	4638.74	33.59	•	00:00	33.59	4605.15
CPT-17	8/18/92	1528.38	3493.12	4635.28	11.82	•	0.00	11.82	4623.46
	3/4/93	1528.38	3493.12	4635.28	11.48	•	0.00	11.48	4623.80
	4/29/93	1528.38	3493.12	4635.28	11.58	•	0.00	11.58	4623.70
	8/6/93	1528.38	3493.12	4635.28	11.72	•	0.00	21.11	4623.56
	5/20/93	1528.38	3493.12	4635.2×	11 67		0.00	19'11	4623.61
CPT-18	8/18/92	1885.05	3457.77	4641.46	13.44	•	0.00	13.44	4628.02
	3/4/93	1885.05	3457.77	4641.46	12.38	•	0.00	12.38	4629.08
	3/18/93	1885.05	3457.77	4641.46	11.80	•	0.00	11.80	4629.66
	4/2/93	1885.05	3457.77	4641.46	11.65		0.00	11.65	4629.81
	4/29/93	1885.05	3457.77	4641.46	11.97	•	0.00	11.97	4629.49
	5/6/93	1885.05	3457.77	4641.46	12.10		00:00	12.10	4629.36
	\$/20/93	1885.05	3457.77	4641.46	12.00		00:00	12.00	4629.46
	6/11/93	1885.05	3457.77	4641.46	12.20		0.00	12.20	4629.26
	6/23/93	1885.05	3457.77	4641.46	12.20	•	0.00	12.20	4629.26
	1/1/93	1885.05	3457.77	4641.46	12.55	•	0.00	12.55	4628.91
	7/8/93	1885.05	3457.77	4641.46	12.66	•	0.00	12.66	4628.80
	8/23/93	1885.05	3457.77	4641.46	12.05	•	0.00	12.05	4629.41
	12/28/93	1885.05	3457.77	4641.46	12.75	•	00.00	12.75	4628.71

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9/20/94

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				Datum	Measured Depth	Depth to	Product	Сотт. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(ft msl)	(ft BTOC)	(ft BTOC)	(feet)	(fl BTOC)	(fi msl)
	1/20/94	1885.05	3457.77	4641.46	13.11		00:00	13.11	4628.35
	2/3/94	1885.05	3457.77	4641.46	13.35		00:00	13.35	4628.11
	3/3/94	1885.05	3457.77	4641.46	13.72	,	00:00	13.72	4627.74
	3/17/94	1885.05	3457.77	4641.46	13.85	 	00:00	13.85	4627.61
	3/31/94	1885.05	3457.77	4641.46	12.88		0:00	12.88	4628.58
	4/14/94	1885.05	3457.77	4641.46	13.29		00:00	13.29	4628.17
CPT-19	8/18/92	1948.46	3215.91	4636.98	30.73		00:0	30.73	4606.25
	3/4/93	1948.46	3215.91	4636.98	30.52		0.00	30.52	4606.46
	4/2/93	1948.46	3215.91	4636.98	29.50		0.00	29.50	4607.48
	4/29/93	1948.46	3215.91	4636.98	28.95		00:00	28.95	4608.03
	\$/9/\$	1948.46	3215.91	4636.98	28.85		00:00	28.85	4608.13
	\$/20/93	1948.46	3215.91	4636.98	28.67		0.00	28.67	4608.31
	6/11/93	1948.46	3215.91	4636.98	28.32	•	00:00	28.32	4608.66
	6/23/93	1948.46	3215.91	4636.98	28.29		0.00	28.29	4608.69
	2/1//93	1948.46	3215.91	4636.98	28.30		00:00	28.30	4608.68
	7/8/93	1948.46	3215.91	4636.98	28.28	•	0.00	28.28	4608.70
	8/23/93	1948.46	3215.91	4636.98	28.02		00:00	28.02	4608.96
	12/28/93	1948.46	3215.91	4636.98	28.74	•	0.00	28.74	4608.24
	1/20/94	1948.46	3215.91	4636.98	23.07	•	00:00	23.07	4613.91
	2/3/94	1948.46	3215.91	4636.98	29.31	•	0.00	29.31	4607.67
	2/17/94	1948.46	3215.91	4636.98	29.45	•	0.00	29.45	4607.53
	3/3/94	1948.46	3215.91	4636.98	29.70	•	0.00	29.70	4607.28
	3/17/94	1948.46	3215.91	4636.98	29.81		00:00	29.81	4607.17
	3/31/94	1948.46	3215.91	4636.98	30.86		00:0	30.86	4606.12
	4/14/94	1948.46	3215.91	4636.98	30.05	•	0.00	30:08	4606.93
CPT-20	8/18/92	1848.28	3037.59	4625.48	25.12	•	0.00	25.12	4600.36
	3/4/93	1848.28	3037.59	4625.48	25.19	•	0.00	25.19	4600.29
	3/18/93	1848.28	3037.59	4625.48	27.75	•	00:00	27.75	4597.73
	4/2/93	1848.28	3037.59	4625.48	24.22	•	00:0	24.22	4601.26
	4/29/93	1848.28	3037.59	4625.48	23.50	22.50	1.00	22.75	4602.73
	\$/6/93	1848.28	3037.59	4625.48	23.47		00:0	23.47	4602.01
	\$/20/93	1848.28	3037.59	4625.48	23.25	•	00:00	23.25	4602.23
	6/11/93	1848.28	3037.59	4625.48	22.89	•	00'0	22.89	4602.59

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				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample		•	Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(ft msl)	(ft BTOC)	(ft BTOC)	(feet)	(ft BTOC)	(ft msd)
	6/23/93	1848.28	3037.59	4625.48	22.86	•	0.00	22.86	4602.62
	2/1/23	1848.28	3037.59	4625.48	22.79	•	00:0	22.79	4602.69
	7/8/93	1848.28	3037.59	4625.48	22.76	-	00:0	22.76	4602.72
	8/23/93	1848.28	3037.59	4625.48	22.36		00:0	22.36	4603.12
	12/28/93	1848.28	3037.59	4625.48	23.42	•	00:00	23.42	4602.06
	1/20/94	1848.28	3037.59	4625.48	23.75	•	0.00	23.75	4601.73
	2/3/94	1848.28	3037.59	4625.48	23.98	23.97	0.01	23.97	4601.51
	2/17/94	1848.28	3037.59	4625.48	24.06	24.05	0.01	24.05	4601.43
	3/3/94	1848.28	3037.59	4625.48	24.34	24.31	0.03	24.32	4601.16
	3/17/94	1848.28	3037.59	4625.48	24.45	•	00:00	24.45	4601.03
	3/31/94	1848.28	3037.59	4625.48	24.59		00:0	24.59	4600.89
	4/14/94	1848.28	3037.59	4625.48	24.65	•	00'0	24.65	4600.83
CPT-21	8/18/92	2349.56	3244.25	4655.91	30.68	•	00:0	30.68	4625.23
	3/4/93	2349.56	3244.25	4655.91	32.88	•	00'0	32.88	4623.03
	3/18/93	2349.56	3244.25	4655.91	32.70	•	0.00	32.70	4623.21
	4/2/93	2349.56	3244.25	4655.91	32.00	•	00:0	32.00	4623.91
	5/6/93	2349.56	3244.25	4655.91	31.59	•	0.00	31.59	4624.32
	5/20/93	2349.56	3244.25	4655.91	31.44	•	0.00	31.44	4624.47
	6/23/93	2349.56	3244.25	4655.91	31.27	•	00'0	31.27	4624.64
	7/1/93	2349.56	3244.25	4655.91	31.16	•	00:0	31.16	4624.75
	7/8/93	2349.56	3244.25	4655.91	31.11		00'0	31.11	4624.80
	12/28/93	2349.56	3244.25	4655.91	31.93	•	0.00	31.93	4623.98
	1/20/94	2349.56	3244.25	4655.91	22.34	-	0.00	22.34	4633.57
	2/3/94	2349.56	3244.25	4655.91	32.48	-	0.00	32.48	4623.43
	2/17/94	2349.56	3244.25	4655.91	32.66		00:00	32.66	4623.25
	3/3/94	2349.56	3244.25	4655.91	32.42	•	0.00	32.42	4623.49
	3/17/94	2349.56	3244.25	4655.91	32.80		0.00	32.80	4623.11
	3/31/94	2349.56	3244.25	4655.91	32.85		00'0	32.85	4623.06
	4/14/94	2349.56	3244.25	4655.91	32.94	•	0.00	32.94	4622.97
CPT.23	8/18/92	2526.12	2835.21	4642.49	28.25	•	0.00	28.25	4614.24
	3/4/93	2526.12	2835.21	4642.49	27.08	•	0.00	27.08	4615.41
	4/2/93	2526.12	2835.21	4642.49	26.82	•	00:00	26.82	4615.67
	4/29/93	2526.12	2835.21	4642.49	26.31	٠	0.00	26.31	4616.18

APPENDIX B

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				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(fi msl)	(ft BTOC)	(ft BTOC)	(feet)	(fl BTOC)	(fi msl)
	8/6/93	2526.12	2835.21	4642.49	26.18		0.00	26.18	4616.31
	5/20/93	2526.12	2835.21	4642.49	25.75	•	0.00	25.75	4616.74
	6/11/93	2526.12	2835.21	4642.49	25.14		0.00	25.14	4617.35
	6/23/93	2526.12	2835.21	4642.49	25.05	•	0.00	25.05	4617.44
	7/1/93	2526.12	2835.21	4642.49	24.87	•	00:00	24.87	4617.62
	7/8/93	2526.12	2835.21	4642.49	24.84	-	00.0	24.84	4617.65
	8/23/93	2526.12	2835.21	4642.49	24.40	•	0.00	24.40	4618.09
	12/28/93	2526.12	2835.21	4642.49	24.97	•	0.00	24.97	4617.52
	1/20/94	2526.12	2835.21	4642.49	25.06		00.0	25.06	4617.43
	2/3/94	2526.12	2835.21	4642.49	25.07	•	0.00	25.07	4617.42
	2/17/94	2526.12	2835.21	4642.49	25.04		0.00	25.04	4617.45
	3/3/94	2526.12	2835.21	4642.49	25.33		0.00	25.33	4617.16
	3/17/94	2526.12	2835.21	4642.49	25.37	•	0.00	25.37	4617.12
	3/31/94	2526.12	2835.21	4642.49	25.53		0.00	25.53	4616.96
	4/14/94	2526.12	2835.21	4642.49	25.71		00.0	25.71	4616.78
CPT-25	12/28/93	SDNA	SDNA	SDNA	28.74	•	00.00	28.74	AN
	1/20/94	SDNA	SDNA	SDNA	28.57	•	00.0	28.57	AN
	2/3/94	SDNA	SDNA	SDNA	28.37	•	00.00	28.37	AN
	2/17/94	SDNA	SDNA	SDNA	28.15	•	0.00	28.15	AN
	3/3/94	SDNA	SDNA	SDNA	25.82	•	0.00	25.82	AN
	3/17/94	SDNA	SDNA	SDNA	28.45	•	00'0	28.45	AN
	3/31/94	SDNA	SDNA	SDNA	28.62	•	0.00	28.62	AN
	4/14/94	SDNA	SDNA	SDNA	28.60	•	0.00	28.60	NA
CPT-26	8/18/92	1208.02	2573.01	4591.94	12.35	•	0.00	12.35	4579.59
	1/20/94	1208.02	2573.01	4591.94	DRY	•	00:0	DRY	ΑN
	3/17/94	1208.02	2573.01	4591.94	DRY	•	00:0	DRY	AN
	3/31/94	1208.02	2573.01	4591.94	DRY	•	0.00	DRY	Ϋ́Α
CPT-27	8/18/92	1662.55	2660.73	4604.04	8.57	•	0.00	8.57	4595.47
	4/21/93	1662.55	2660.73	4604.04	8.28	•	0.00	8.28	4595.76
	4/29/93	1662.55	2660.73	4604.04	8.42	٠	0.00	8.42	4595.62
	5/6/93	1662.55	2660.73	4604.04	8.35	٠	00:0	8.35	4595.69
	\$/20/93	1662.55	2660.73	4604.04	8.20	•	0.00	8.20	4595.84
	6/11/93	1662.55	2660.73	4604.04	7.85	•	00:00	7.85	4596.19

APPENDIX B

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				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(ft msl)	(ft BTOC)	(ft BTOC)	(feet)	(f) BTOC)	(finst)
	6/23/93	1662.55	2660.73	4604.04	7.56	•	0.00	7.56	4596.48
	7/1/93	1662.55	2660.73	4604.04	7.80	•	0.00	7.80	4596.24
	7/8/93	1662.55	2660.73	4604.04	69'L	-	00:00	7.69	4596.35
	8/23/93	1662.55	2660.73	4604.04	7.00	-	00:00	7.00	4597.04
	12/28/93	1662.55	2660.73	4604.04	8.51		00:00	8.51	4595.53
	1/20/94	1662.55	2660.73	4604.04	8.90		00.0	8.90	4595.14
	2/3/94	1662.55	2660.73	4604.04	80.6		00:0	80.6	4594.96
	2/17/94	1662.55	2660.73	4604.04	9.12		00:00	9.12	4594.92
	3/3/94	1662.55	2660.73	4604.04	8.99		00:0	8.99	4595.05
	3/17/94	1662.55	2660.73	4604.04	9.15	•	00:00	9.15	4594.89
	3/31/94	1662.55	2660.73	4604.04	8.88	•	0.00	98.00	4595.16
	4/14/94	1662.55	2660.73	4604.04	8.92	•	00:00	8.92	4595.12
CPT-28	8/18/92	1538.79	2939.72	4605.62	6.43	•	00:00	6.43	4599.19
	3/4/93	1538.79	2939.72	4605.62	6.18	•	00:00	6.18	4599.44
	4/29/93	1538.79	2939.72	4605.62	5.62	•	0.00	5.62	4600.00
	\$/6/93	1538.79	2939.72	4605.62	5.72	•	0.00	5.72	4599.90
	5/20/93	1538.79	2939.72	4605.62	5.97	•	0.00	5.97	4599.65
	6/11/93	1538.79	2939.72	4605.62	5.88		0.00	5.88	4599.74
	6/23/93	1538.79	2939.72	4605.62	96.9	•	0.00	96.9	4598.66
	7/1/93	1538.79	2939.72	4605.62	5.82	•	00'0	5.82	4599.80
	7/8/93	1538.79	2939.72	4605.62	6.19	•	00:0	61.9	4599.43
	8/23/93	1538.79	2939.72	4605.62	5.07	•	0.00	5.07	4600.55
	12/28/93	1538.79	2939.72	4605.62	DRY	•	0.00	DRY	ΥN
	1/20/94	1538.79	2939.72	4605.62	DRY	•	0.00	DRY	٧N
	2/3/94	1538.79	2939.72	4605.62	DRY		0.00	DRY	٧×
	2/17/94	1538.79	2939.72	4605.62	6.56	•	0.00	98.9	4599.06
	3/3/94	1538.79	2939.72	4605.62	7.39	•	0.00	7.39	4598.23
	3/17/94	1538.79	2939.72	4605.62	7.43	•	00:00	7.43	4598.19
	3/31/94	1538.79	2939.72	4605.62	09:9	•	00:00	99.9	4599.02
	4/14/94	1538.79	2939.72	4605.62	7.04	•	0.00	7.04	4598.58
CPT-29	8/18/92	1400.23	2863.23	4600.67	5.15	•	0.00	5.15	4595.52
CPT-30	8/18/92	1963.38	2711.28	4610.22	12.82	•	0.00	12.82	4597.40
	4/21/93	1963.38	2711.28	4610.22	12.05	•	00:00	12.05	4598.17

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
ocation	Date	Easting	Northing	(fi msl)	(ft BTOC)	(ft BTOC)	(feet)	(A BTOC)	(प्रमा)
	4/29/93	1963.38	2711.28	4610.22	12.16	•	0.00	12.16	4598.06
	5/6/93	1963.38	2711.28	4610.22	12.15		00.0	12.15	4598.07
	5/20/93	1963.38	2711.28	4610.22	11.90	•	00:00	11.90	4598.32
	6/11/93	1963.38	2711.28	4610.22	11.60	•	00'0	11.60	4598.62
	6/23/93	1963.38	2711.28	4610.22	11.54	•	00:00	11.54	4598.68
	7/1/93	1963.38	2711.28	4610.22	11.50	•	00.0	11.50	4598.72
	7/8/93	1963.38	2711.28	4610.22	11.46	•	00.0	11.46	4598.76
	8/23/93	1963.38	2711.28	4610.22	10.70	•	0.00	10.70	4599.52
	12/28/93	1963.38	2711.28	4610.22	12.17	•	00.0	12.17	4598.05
	1/20/94	1963.38	2711.28	4610.22	12.44	•	00.00	12.44	4597.78
	2/3/94	1963.38	2711.28	4610.22	12.59	•	00.00	12.59	4597.63
	2/17/94	1963.38	2711.28	4610.22	12.71	•	00.00	12.71	4597.51
	3/3/94	1963.38	2711.28	4610.22	12.73	•	00.0	12.73	4597.49
	3/17/94	1963.38	2711.28	4610.22	12.81	•	00:00	12.81	4597.41
	3/31/94	1963.38	2711.28	4610.22	12.85	•	00.00	12.85	4597.37
	4/14/94	1963.38	2711.28	4610.22	12.85	•	00:00	12.85	4597.37
CPT-31	8/18/92	1418.19	3205.92	4610.88	7.37	•	0.00	7.37	4603.51
	3/4/93	1418.19	3205.92	4610.88	9.60	•	00.00	5.60	4605.28
	4/29/93	1418.19	3205.92	4610.88	4.50	•	00.00	4.50	4606.38
	8/6/93	1418.19	3205.92	4610.88	4.74	•	00.00	4.74	4606.14
	5/20/93	1418.19	3205.92	4610.88	5.42	•	00.00	5.42	4605.46
	6/11/93	1418.19	3205.92	4610.88	5.58	•	00:00	5.58	4605.30
	6/23/93	1418.19	3205.92	4610.88	5.80	•	0.00	5.80	4605.08
	7/1/93	1418.19	3205.92	4610.88	7.01	•	00.00	7.01	4603.87
	7/8/93	418.19	3205.92	4610.88	5.78	•	00.00	5.78	4605.10
	8/23/93	1418.19	3205.92	4610.88	6.05	•	00.00	6.05	4604.83
	12/28/93	1418.19	3205.92	4610.88	7.80	•	0.00	7.80	4603.08
	1/20/94	1418.19	3205.92	4610.88	7.98	٠	00:00	7.98	4602.90
	2/3/94	1418.19	3205.92	4610.88	8.15	•	00'0	8.15	4602.73
	2/17/94	1418.19	3205.92	4610.88	8.37		00.00	8.37	4602.51
	3/3/94	1418.19	3205.92	4610.88	7.19	•	00.00	7.19	4603.69
	3/17/94	1418.19	3205.92	4610.88	7.31	•	00.00	7.31	4603.57
	3/31/94	1418.19	3205.92	4610.88	7.28	•	00.00	7.28	4603.60

GROUND WATER ELEVATION AND MOBILE LINAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Cocation	Date	Easting	Northing	(ft msf)	(ft BTOC)	(fl BTOC)	(fect)	(ft BTOC)	(ft msl)
					1				
	4/14/94	1418.19	3205.92	4610.88	7.28	•	0.00	7.28	4603.60
CPT-32	1/20/94	SDNA	SDNA	SDNA	DRY	•	00:0	DRY	NA
	3/17/94	SDNA	SDNA	SDNA	DRY		00:00	DRY	Ϋ́Α
	3/31/94	SDNA	SDNA	SDNA	DRY		00:0	DRY	Ϋ́
CPT-33	12/28/93	SDNA	SDNA	SDNA	18.05		00:00	18.05	NA
	1/20/94	SDNA	SDNA	SDNA	18.33	•	00:0	18.33	ΝΑ
	2/3/94	SDNA	SDNA	SDNA	18.29		0.00	18.29	Ϋ́Α
	2/17/94	SDNA	SDNA	SDNA	18.21	•	0.00	18.21	A'N
	3/3/94	SDNA	SDNA	SDNA	18.85	•	0.00	18.85	ΝΑ
	3/17/94	SDNA	SDNA	SDNA	18.70	•	00:00	18.70	NA
	3/31/94	SDNA	SDNA	SDNA	18.97		00:00	18.97	A'A
	4/14/94	SENA	SDNA	SDNA	19.21		00:0	19.21	NA
CPT-34	12/28/93	SDNA	SDNA	SDNA	20.10		00:0	20.10	NA
	1/20/94	SDNA	SDNA	SDNA	20.27	•	00:0	20.27	NA
3	2/3/94	SDNA	SDNA	SDNA	20.32		00:00	20.32	ΝA
	2/17/94	SDNA	SDNA	SDNA	20.32		00:00	20.32	NA
	3/3/94	SDNA	SDNA	SDNA	20.40	•	00:00	20.40	A'N
	3/17/94	SDNA	SDNA	SDNA	20.45		00:00	20.45	ΨZ
	3/31/94	SDNA	SDNA	SDNA	20.55	•	00:00	20.55	ΥN
	4/14/94	SDNA	SDNA	SDNA	26.66		00:00	76.66	AN
CPT-36	8/18/92	2670.91	3231.11	4669.78	34.97		00:0	34.97	4634.81
CPT-37	8/18/92	1970.30	2978.15	4625.35	26.40	•	00:00	26.40	4598.95
	4/21/93	1970.30	2978.15	4625.35	24.00		00.0	24.00	4601.35
	4/29/93	1970.30	2978.15	4625.35	23.75	•	00:00	23.75	4601.60
	5/6/93	1970.30	2978.15	4625.35	23.74	•	00:00	23.74	4601.61
	5/20/93	1970.30	2978.15	4625.35	23.49	•	00:00	23.49	4601.86
	6/11/93	1970.30	2978.15	4625.35	23.15	•	0.00	23.15	4602.20
	6/23/93	1970.30	2978.15	4625.35	23.10	•	00:00	23.10	4602.25
	7/1/93	1970.30	2978.15	4625.35	22.98	•	00.0	86.22	4602.37
	7/8/93	1970.30	2978.15	4625.35	22.94		00:00	22.94	4602.41
	12/28/93	1970.30	2978.15	4625.35	23.58	•	0.00	23.58	4601.77
	1/20/94	1970.30	2978.15	4625.35	24.12	23.72	0.40	23.82	4601.53
	2/3/94	1970.30	2978.15	4625.35	24.30	24.15	\$10	24 19	460116

GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(fim fi)	(ft BTOC)	(ft BTOC)	(feet)	(ft BTOC)	(ft msl)
	2/17/94	1970.30	2978.15	4625.35	24.65	24.34	0.31	24.42	4600.93
	3/3/94	1970.30	2978.15	4625.35	24.78	24.28	0.50	24.41	4600.95
	3/17/94	1970.30	2978.15	4625.35	24.84	23.84	1.00	24.09	4601.26
	3/31/94	1970.30	2978.15	4625.35	24.85	24.60	0.25	24.66	4600.69
	4/14/94	1970.30	2978.15	4625.35	25.05	24.55	0.50	24.68	4600.68
CPT-38	26/81/8	69'LL11	3504.76	4615.66	13.05		00:00	13.05	4602.61
	3/4/93	1177.69	3504.76	4615.66	12.08		0.00	12.08	4603.58
	4/29/93	1177.69	3504.76	4615.66	13.33		00:0	13.33	4602.33
	8/6/93	1177.69	3504.76	4615.66	13.18	•	00:0	13.18	4602.48
	5/20/93	1177.69	3504.76	4615.66	13.09	•	00:0	13.09	4602.57
	6/11/9	1177.69	3504.76	4615.66	9.60	•	00:0	09:\$	4610.06
	6/23/93	1177.69	3504.76	4615.66	11.94		00.0	11.94	4603.72
	7/1/93	1177.69	3504.76	4615.66	12.19	•	00:0	12.19	4603.47
	7/8/93	1177.69	3504.76	4615.66	11.86	•	00'0	11.86	4603.80
	8/23/93	1177.69	3504.76	4615.66	11.13	•	00:00	11.13	4604.53
	12/28/93	1177.69	3504.76	4615.66	10.16	•	00 0	10.16	4605.50
	1/20/94	1177.69	3504.76	4615.66	11.77	•	0.00	11.77	4603.89
	2/3/94	1177.69	3504.76	4615.66	13.04	٠	0.00	13.04	4602.62
	2/17/94	1177.69	3504.76	4615.66	13.92	•	00'0	13.92	4601.74
	3/3/94	1177.69	3504.76	4615.66	14.71	•	00:0	14.71	4600.95
	3/17/94	1177.69	3504.76	4615.66	15.19	•	00:0	15.19	4600.47
	3/31/94	1177.69	3504.76	4615.66	15.42	•	00'0	15.42	4600.24
	4/14/94	1177.69	3504.76	4615.66	15.45	•	0.00	15.45	4600.21
CPT-40	8/18/92	2758.65	4145.21	4715.46	38.89	•	0.00	38.89	4676.57
	4/21/93	2758.65	4145.21	4715.46	52.85	•	00.00	52.85	4662.61
	4/29/93	2758.65	4145.21	4715.46	53.33		0.00	53.33	4662.13
	\$/6/93	2758.65	4145.21	4715.46	53.17	•	00'0	23.17	4662.29
	5/20/93	2758.65	4145.21	4715.46	53.04		00:00	\$3.04	4662.42
	6/11/93	2758.65	4145.21	4715.46	53.20	•	00'0	53.20	4662.26
	6/23/93	2758.65	4145.21	4715.46	53.27		00'0	53.27	4662.19
	7/1/93	2758.65	4145.21	4715.46	53.22	•	0.00	53.22	4662.24
	7/8/93	2758.65	4145.21	4715.46	53.10	•	0.00	53.10	4662.36
	12/28/93	2758.65	4145.21	4715.46	51.20		0.00	51.20	4664.26

GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water	Elevation
Location	Date	Easting	Northing	(ff msl)	(# BTOC)	(# BTOC)	(feet)	(# BTOC)	(A ms)
	1/20/94	2758.65	4145.21	4715.46	\$0.89		0.00	50.89	4664.57
	2/3/94	2758.65	4145.21	4715.46	50.52	•	00.0	50.52	4664.94
	2/17/94	2758.65	4145.21	4715.46	49.34		00:0	49.34	4666.12
	3/3/94	2758.65	4145.21	4715.46	48.83	•	00:0	48.83	4666.63
ļ	3/17/94	2758.65	4145.21	4715.46	46.47		00.0	46.47	4668.99
	3/31/94	2758.65	4145.21	4715.46	45.93		00:0	45.93	4669.53
	4/14/94	2758.65	4145.21	4715.46	44.13		00:0	44.13	4671.33
CPT-41	6/11/93	2857.64	3142.16	4675.19	39.90	•	00:0	39.90	4635.29
	6/23/93	2857.64	3142.16	4675.19	39.28		00:0	39.28	4635.91
	7/1/93	2857.64	3142.16	4675.19	39.15		00.0	39.15	4636.04
	7/8/93	2857.64	3142.16	4675.19	39.30	•	00:0	39.30	4635.89
	12/28/93	2857.64	3142.16	4675.19	31.25	•	000	31.25	4643.94
	1/20/94	2857.64	3142.16	4675.19	31.31		00:0	31.31	4643.88
	2/3/94	2857.64	3142.16	4675.19	31.09		00:0	31.09	4644.10
	2/17/94	2857.64	3142.16	4675.19	30.93	•	00:0	30.93	4644.26
	3/3/94	2857.64	3142.16	4675.19	31.52	•	00:0	31.52	4643.67
	3/17/94	2857.64	3142.16	4675.19	31.35		00:00	31.35	4643.84
	3/31/94	2857.64	3142.16	4675.19	31.74		00:0	31.74	4643.45
	4/14/94	2857.64	3142.16	4675.19	32.38	•	00:0	32.38	4642.81
CPT-42	3/4/93	3067.32	3238.57	4678.34	36.93		0.00	36.93	4641.41
	4/2/93	3067.32	3238.57	4678.34	36.80	•	00:00	36.80	4641.54
	4/29/93	3067.32	3238.57	4678.34	37.00		00:00	37.00	4641.34
	\$/6/93	3067.32	3238.57	4678.34	36.45		00:00	36.45	4641.89
	\$/20/93	3067.32	3238.57	4678.34	36.00		00:00	36.00	4642.34
	6/11/93	3067.32	3238.57	4678	35.37	•	00:00	35.37	4642.97
	6/23/93	3067.32	3238.57	4678.3⊶	35.25	•	00:00	35.25	4643.09
	7/1/93	3067.32	3238.57	4678.34	33.05	•	0.00	33.05	4645.29
	7/8/93	3067.32	3.238.57	4678.34	35.13		0.00	35.13	4643.21
	12/28/93	3067.32	3238.57	4678.34	32.99	•	0.00	32.99	4645.35
j	1 20/94	3067.32	3238.57	4678.34	33.18	•	0.00	33.18	4645.16
	2,3/94	3067.32	3238.57	4678.34	33.31		00:00	33.31	4645.03
	2/17/94	3067.32	3238.57	4678.34	33.22		00:00	33.22	4645.12
	3/3/94	3067.32	3238.57	4678.34	34.00	•	00:00	34.00	4644.34

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APPENDIX B

GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION ELCA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Sor Ca
Samole	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Cation	Date	Easting	Northing	(fi msl)	(# BTOC)	(# BTOC)	(feet)	(ft BTOC)	(firms)
	3/17/94	3067.32	3238.57	4678.34	33.98	•	0.00	33.98	4644.36
	3/31/94	3067.32	3238.57	4678.34	34.44		0.00	34.44	4643.90
	4/14/94	3067.32	3238.57	4678.34	34.89		00'0	34.89	4643.45
CPT-41	3/4/93	2683.44	3014.06	4659.74	29.60		00:00	29.60	4630.14
	4/2/93	2683.44	3014.06	4659.74	29.67		00:00	29.67	4630.07
	4/29/93	2683.44	3014.06	4659.74	29.35		00:00	29.35	4630.39
	\$/6/93	2683.44	3014.06	4659.74	29.42		0.00	29.42	4630.32
	\$/20/93	2683.44	3014.06	4659.74	29.18		0.00	29.18	4630.56
CPT-44	12/28/93	SDNA	SDNA	SDNA	30.83		00:00	30.83	V
	1/20/94	SDNA	SDNA	SDNA	30.69	•	00:0	30.69	Y.
	2/3/94	SDNA	SDNA	SDNA	30.55		0.00	30.55	NA
	2/17/94	SDNA	SDNA	SDNA	30.34	•	0.00	30.14	Y _N
	3/3/94	SDNA	SDNA	SDNA	30.76		0.00	30.70	NA.
	3/17/94	SDNA	SDNA	SDNA	30.63		00:0	30.63	VA
	3/31/94	SDNA	SDNA	SDNA	30.79		00:0	30.79	NA
	4/14/94	SDNA	SDNA	SDNA	30.63		00:0	30.63	Y.
EPA-82-A	8/23/93	1546.62	2945.10	4606.35	4.85		0.00	4.85	4601.50
	12/28/93	1546.62	2945.10	4606.35	6.22	•	00:00	6.22	4600.13
	1/20/94	1546.62	2945.10	4606.35	6.27	•	0.00	6.27	4600.08
	2/3/94	1546.62	2945.10	4606.35	6.33	•	00:0	6.33	4600.02
	2/17/94	1546.62	2945.10	4606.35	6.28	•	00:00	6.28	4600.07
	3/3/94	1546.62	2945.10	4606.35	8.94	•	00:00	8.94	4597.41
	3/17/94	1546.62	2945.10	4606.35	5.95		00:00	5.95	4600.40
	3/31/94	1546.62	2945.10	4606.35	8.82	•	00:00	8.82	4597.53
	4/14/94	1546.62	2945.10	4606.35	\$.60	•	00.00	5.60	4600.75
EPA-82-B	8/23/93	2062.23	3063.44	4633.28	25.00	•	00:00	25.00	4608.28
	12/28/93	2062.23	3063.44	4633.28	25.49		00.00	25.49	4607.79
	1/20/94	2062.23	3063.44	4633.28	25.35		00:00	25.35	4607.93
	2/3/94	2062.23	3063.44	4633.28	25.43	•	00:00	25.43	4607.85
	2/17/94	2062.23	3063.44	4633.28	23.54		00:00	23.54	4609.74
	3/3/94	2062.23	3063.44	4633.28	25.69		00.00	25.69	4607.59
	3/17/94	2062.23	3063.44	4633.28	25.50		0.00	25.50	4607.78
	221.04	2062 23	1063 44	4633.28	25.79		000	25.79	4607 49

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APPENDIX B

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GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr
Sample	Sample		-	Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(fi msl)	(ft BTOC)	(ft BTOC)	(feet)	(ft BTOC)	(fi msl)
	4/14/94	2062.23	3063.44	4633.28	26.02	•	0.00	26.02	4607.26
EPA-82-C	8/23/93	1840.49	3035.78	4625.17	21.80	•	0.00	21.80	4603.37
	12/28/93	1840.49	3035.78	4625.17	22.82		00:00	22.82	4602.35
	1/20/94	1840.49	3035.78	4625.17	23.13		00:00	23.13	4602.04
	2/3/94	1840.49	3035.78	4625.17	23.35	•	00:00	23.35	4601.82
	2/17/94	1840.49	3035.78	4625.17	23.54	•	00:00	23.54	4601.63
	3/3/94	1840.49	3035.78	4625.17	23.69		0.00	23.69	4601.48
	3/17/94	1840.49	3035.78	4625.17	23.76	•	00:00	23.76	4601.41
	3/31/94	1840.49	3035.78	4625.17	23.87	•	00'0	23.87	4601.30
	4/14/94	1840.49	3035.78	4625.17	23.94		00.00	23.94	4601.23
EPA-82-D	8/23/93	2167.57	3507.69	4655.39	23.69		00.00	23.69	4631.70
	12/28/93	2167.57	3507.69	4655.39	24.45	24.37	80.0	24.39	4631.00
	1/20/94	2167.57	3507.69	4655.39	24.60	24.53	0.07	24.55	4630.84
	2/3/94	2167.57	3507.69	4655.39	24.69	24.42	0.27	24.49	4630.90
	2/17/94	2167.57	3507.69	4655.39	24.51	24.36	0.15	24.40	4630.99
	3/3/94	2167.57	3507.69	4655.39	24.93	24.92	0.01	24.92	4630.47
	3/17/94	2167.57	3507.69	4655.39	24.88	24.80	80.0	24.82	4630.57
	3/31/94	2167.57	3507.69	4655.39	25.09	24.99	0.10	25.02	4630.38
	4/14/94	2167.57	3507.69	4655.39	25.17	•	00:00	25.17	4630.22
EPA-82-E	8/23/93	1345.36	2845.36	4600.13	4.92	•	00:00	4.92	4595.21
	12/28/93	1345.36	2845.36	4600.13	7.32	•	00:00	7.32	4592.81
	1/20/94	1345.36	2845.36	4600.13	7.58	•	00:00	7.58	4592.55
	2/3/94	1345.36	2845.36	4600.13	7.75	•	00:00	7.75	4592.38
	2/17/94	1345.36	2845.36	4600.13	7.81	•	00:00	7.81	4592.32
	3/3/94	1345.36	2845.36	4600.13	7.21		00.00	7.21	4592.92
	3/17/94	1345.36	2845.36	4600.13	7.14	•	00:00	7.14	4592.99
	3/31/94	1345.36	2845.36	4600.13	6.92		00:00	6.92	4593.21
	4/14/94	1345.36	2845.36	4600.13	6.70		00:00	6.70	4593.43
FPA-82-F	8/23/93	1543.19	2943.57	4606.19	6.13	•	00:00	6.13	4600.06
	12/28/93	1543.19	2943.57	4606.19	8.28		0.00	8.28	4597.91
	1/20/94	1543.19	2943.57	4606.19	8.43	•	00:00	8.43	4597.76
	2/3/94	1543.19	2943.57	4606.19	8.54	•	00:00	8.54	4597.65
	2/17/94	1543.19	2943.57	4606.19	8.63	•	00:0	8.63	4597.56

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APPENDIX B

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GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(ft msl)	(ft BTOC)	(fl BTOC)	(feet)	(ft BTOC)	(fi msl)
	3/3/94	1543.19	2943.57	4606.19	7.97	•	0.00	76.7	4598.22
	3/17/94	1543.19	2943.57	4606.19	21.75	•	00:0	7.75	4598.44
	3/31/94	1543.19	2943.57	4606.19	7.53		00:0	7.53	4598.66
	4/14/94	1543.19	2943.57	4606.19	75.7	•	00:0	7.37	4598.82
EPA-82-H	8/23/93	1964.51	17.6172	4610.81	51.11	0.00	00:0	11.15	4599.66
	12/28/93	1964.51	17.6172	4610.81	12.34		00:0	12.34	4598.47
	1/20/94	1964.51	2719.71	4610.81	12.58	•	0.00	12.58	4598.23
	2/3/94	1964.51	2719.71	4610.81	12.74	•	0.00	12.74	4598.07
	2/17/94	1964.51	2719.71	4610.81	12.92	•	0.00	12.92	4597.89
	3/3/94	1964.51	2719.71	4610.81	12.91	•	00:0	12.91	4597.90
	3/17/94	1964.51	2719.71	4610.81	13.00		00:0	13.00	4597.81
	3/31/94	1964.51	2719.71	4610.81	13.03	•	0.00	13.03	4597.78
	4/14/94	1964.51	17.6172	4610.81	13.03		0.00	13.03	4597.78
EPA-82-1	8/23/93	2520.42	3771.26	4683.08	18.55		0.00	18.55	4664.53
	12/28/93	2520.42	3771.26	4683.08	20.29	•	00:00	20.29	4662.79
	1/20/94	2520.42	3771.26	4683.08	22.51		0.00	22.51	4660.57
	2/3/94	2520.42	3771.26	4683.08	20.46	•	0.00	20.46	4662.62
	2/17/94	2520.42	3771.26	4683.08	20.41	•	00:0	20.41	4662.67
	3/3/94	2520.42	3771.26	4683.08	20.84		00:00	20.84	4662.24
	3/17/94	2520.42	3771.26	4683.08	20.61	•	0.00	20.61	4662.47
	3/31/94	2520.42	3771.26	4683.08	20.59	•	00:00	20.59	4662.49
	4/14/94	2520.42	3771.26	4683.08	20.30	•	0.00	20.30	4662.78
MW-1	3/18/93	2475.32	3841.98	4683.91	22.80	22.75	0.05	22.76	4661.15
	4/21/93	2475.32	3841.98	4683.91	23.10	20.18	2.92	20.91	4663.00
	4/29/93	2475.32	3841.98	4683.91	22.77	19.39	3.38	20.24	4663.68
	\$/6/93	2475.32	3841.98	4683.91	22.00	19.04	2.96	19.78	4664.13
	5/20/93	2475.32	3841.98	4683.91	20.14	19.07	1,07	19.34	4664.57
	6/11/93	2475.32	3841.98	4683.91	18.97	18.69	0.28	18.76	4665.15
	6/23/93	2475.32	3841.98	4683.91	19.02	18.66	0.36	18.75	4665.16
	7/1/93	2475.32	3841.98	4683.91	09'81		00:0	18.60	4665.31
	7/8/93	2475.32	3841.98	4683.91	18.85	18.56	0.29	18.63	4665.28
	12/28/93	2475.32	3841.98	4683.91	19.42	19.42	00.00	19.42	4664.49
	1/20/94	2475.32	3841.98	4683.91	08.61	19.79	10.0	19.79	4664.12

GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(ft msl)	(ft BTOC)	(f) BTOC)	(feet)	(ft BTOC)	(fi msl)
	2/17/94	2475.32	3841.98	4683.91	19.52	19.51	0.01	19.51	4664.40
	3/3/94	2475.32	3841.98	4683.91	20.31	20.30	0.01	20.30	4663.61
	3/17/94	2475.32	3841.98	4683.91	20.40	•	0000	20.40	4663.51
	3/31/94	2475.32	3841.98	4683.91	20.42	,	00.00	20.42	4663.49
	4/14/94	2475.32	3841.98	4683.91	22.01	,	00:0	22.01	4661.90
MW-02	2/12/93	2389.21	3846.24	4684.39	25.20		0.00	25.20	4659.19
	3/18/93	2389.21	3846.24	4684.39	25.11	•	00:00	25.11	4659.28
	4/21/93	2389.21	3846.24	4684.39	23.93	•	00:00	23.93	4660.46
	4/29/93	2389.21	3846.24	4684.39	23.69		00'0	23.69	4660.70
	\$/6/93	2389.21	3846.24	4684.39	23.44	•	00:00	23.44	4660.95
	\$/20/93	2389.21	3846.24	4684.39	23.01	•	00:00	23.01	4661.38
	6/17/93	2389.21	3846.24	4684.39	22.57	22.44	0.13	22.47	4661.92
	6/23/93	2389.21	3846.24	4684.39	22.61	22.40	0.21	22.45	4661.94
	7/1/93	2389.21	3846.24	4684.39	22.54	22.27	0.27	22.34	4662.05
	7/8/93	2389.21	3846.24	4684.39	22.62	22.26	0.36	22.35	4662.04
	12/28/93	2389.21	3846.24	4684.39	23.77	23.74	0.03	23.75	4660.64
	1/20/94	2389.21	3846.24	4684.39	24.04	24.03	0.01	24.03	4660.36
	2/3/94	2389.21	3846.24	4684.39	24.06	24.05	0.01	24.05	4660.34
	2/17/94	2389.21	3846.24	4684.39	24.06	24.05	0.01	24.05	4660.34
	3/3/94	2389.21	3846.24	4684.39	24.24	24.23	0.01	24.23	4660.16
	3/17/94	2389.21	3846.24	4684.39	22.24	•	0.00	22.24	4662.15
	3/31/94	2389.21	3846.24	4684.39	24.24	•	00:00	24.24	4660.15
	4/14/94	2389.21	3846.24	4684.39	24.16	•	00:00	24.16	4660.23
MW-03	2/12/93	2533.09	3882.19	4690.67	28.93	28.91	0.02	28.92	4661.76
	3/18/93	2533.09	3882.19	4690.67	28.08	27.69	0.39	27.79	4662.88
	4/21/93	2533.09	3882.19	4690.67	24.25	23.78	0.97	23.52	4667.15
	4/29/93	2533.09	3882.19	4690.67	23.61	23.57	0.04	23.58	4667.09
	\$/6/93	2533.09	3882.19	4690.67	23.53	23.21	0.32	23.29	4667.38
	5/20/93	2533.09	3882.19	4690.67	23.00	22.60	0.40	22.70	4667.97
	6/11/93	2533.09	3882.19	4690.67	22.91	22.58	0.33	22.66	4668.01
	6/23/93	2533.09	3882.19	4690.67	22.68	22.40	0.28	22.47	4668.20
	7/1/93	2533.09	3882.19	4690.67	22.48	22.29	0.19	22.34	4668.33
	7/8/93	2533.09	3882.19	4690.67	23.04	22.33	0.71	22.51	4668.16

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GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

Sample Location		_	_	Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Location	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
	Date	Easting	Northing	(ft msl)	(ft BTOC)	(ft BTOC)	(feet)	(# BTOC)	(प्रथा)
	12/28/93	2533.09	3882.19	4690.67	23.94	23.88	90:0	23.90	4666.78
	1/20/94	5233.09	3882.19	4690.67	23.89	23.74	0.15	23.78	4666.89
	2/17/94	2533.09	3882.19	4690.67	23.65	23.49	0.16	23.53	4667.14
	3/3/94	2533.09	3882.19	4690.67	24.32	24.05	0.27	24.12	4666.55
	3/17/94	2533.09	3882.19	4690.67	24.27	24.03	0.24	24.09	4666.58
	3/31/94	2533.09	3882.19	4690.67	24.42	24.10	0.32	24.18	4666.49
	4/14/94	2533.09	3882.19	4690.67	24.62	23.89	0.64	24.14	4666.53
MW-04	3/18/93	2446.70	3798.05	4682.13	21.65		00'0	21.65	4660.48
	4/21/93	2446.70	3798.05	4682.13	20.05	19.80	0.25	19.86	4662.27
	4/29/93	2446.70	3798.05	4682.13	19.78	19.32	0.43	19.43	4662.70
	5/6/93	2446.70	3798.05	4682.13	19.40	18.93	0.47	19.05	4663.08
	\$/20/93	2446.70	3798.05	4682.13	18.54	18.21	0.33	18.29	4663.84
	6/11/93	2446.70	3798.05	4682.13	18.55	18.30	0.25	18.36	4663.77
	6/23/93	2446.70	3798.05	4682.13	18.79	18.36	0.43	18.47	4663.66
	7/1/93	2446.70	3798 05	4682.13	18.54	18.41	0.13	18.44	4663.69
	7/8/93	2446.70	3798.05	4682.13	18.57	18.45	0.12	18.48	4663.65
	12/28/93	2446.70	3798.05	4682.13	20.38	20.27	0.11	20.30	4661.83
	1/20/94	2446.70	3798.05	4682.13	20.63	20.48	0.15	20.52	19:1994
	2/17/94	2446.70	3798.05	4682.13	20.52	20.51	0.01	20.51	4661.62
	3/3/94	2446.70	3798.05	4682.13	20.81	20.80	10.0	20.80	4661.33
	3/17/94	2446.70	3798.05	4682.13	20.68	•	00.0	20.68	4661.45
	3/31/94	2446.70	3798.05	4682.13	20.61		00:00	20.61	4661.52
	4/14/94	2446.70	3798.05	4682.13	20.05	•	00:0	20.05	4662.08
MW-5	2/12/93	2536.47	3813.49	4686.76	25.00	•	0.00	25.00	4661.76
	3/18/93	2536.47	3813.49	4686.76	20.95		0.00	20.95	4665.81
	4/21/93	2536.47	3813.49	4686.76	20.03	18.78	1.25	60.61	4667.67
	4/29/93	2536.47	3813.49	4686.76	20.01	18.29	1.72	18.72	4668.04
i	8/6/93	2536.47	3813.49	4686.76	20.03	18.10	1.93	18.58	4668.18
	5/20/93	2536.47	3813.49	4686.76	19.43	17.96	1.47	18.33	4668.43
	6/11/93	2536.47	3813.49	4686.76	18.95	18.17	82.0	18.37	4668.40
	6/23/93	2536.47	3813.49	4686.76	19.36	18.12	1.24	18.43	4668.33
	7/1/93	2536.47	3813.49	4686.76	18.78	18.56	0.22	18.62	4668.15
	7/8/93	2536.47	3813.49	4686.76	18.55	18.41	0.14	18.45	4668.32

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GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

4658.21 4658.45 4657.90 4663.74 4665.98 4657.72 4658.21 4659.13 4659.19 4659.31 4659.34 4665.59 4665.31 4656.97 4657.95 4657.98 4662.19 4662.28 4663.48 4664.57 4664.89 Elevation 4663.24 to Water* (A BTOC) 20.99 19.84 19.84 19.72 20.82 20.58 21.08 30.32 30.06 21.31 20 82 20.33 21.05 31.61 30.56 Product Thickness 8 8 8 8 (ged 00.00 8 8 8 8 8 8 9 8 800 8 8 8 8 0.01 000 8 0.0 0.0 0.0 (A BTOC) Depth to 20.79 20.91 20.58 20.73 21.13 20.78 21.33 21.17 21.47 Measured Depth (A BTOC) to Water 19.90 20.82 19.69 21.10 30.06 29.70 29.23 29.15 28.91 21.10 20.92 20.74 21.14 21.08 31.61 30.56 22.06 20.59 4679.03 4679.03 4679.03 4679.03 4679.03 4679.03 4693.80 4693.80 4693.80 4693.80 4693.80 Elevation 4679.03 4679.03 4679.03 4679.03 4693.80 4693.80 4686.76 4685.76 4686.76 4686.76 4686.76 4686.76 4686.76 4679.03 4679.03 (fi msl) 3900.79 3900.79 3900.79 3794.35 3794.35 3794.35 3794.35 3794.35 3794.35 3900.79 3900.79 3900.79 3813.49 3813.49 3794.35 3794.35 3794.35 3794.35 3794.35 3794.35 3794.35 3794.35 3813.49 3794.35 37c4.35 2389.06 2389.06 2389.06 2389.06 2621.27 2621.27 2621.27 2621.27 2621.27 2621.27 2389.06 2389.06 2389.06 2389.06 2621.27 2536.47 2389.06 2389.06 2536.47 2536.47 2536.47 2536.47 2389.06 2389.06 2389.06 2389.06 2536.47 2389.06 2389.06 Easting 3/17/94 3/31/94 4/14/94 2/12/93 3/18/93 7/8/93 12/28/93 1/20/94 2/3/94 4/21/93 6/23/93 2/17/94 1/20/94 3/3/94 3/17/94 3/31/94 4/14/94 3/18/93 4/29/93 \$/20/93 6/11/93 3/3/94 \$/6/93 8/9/9 Sample Date MW-7 (TWP-3) Location Sample 9-MW

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GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(ft msl)	(# BTOC)	(fl BTOC)	(feet)	(fl BTOC)	(fi msl)
	7/8/93	2621.27	3900.79	4693.80	28.79	•	00.0	28.79	4665.01
	12/28/93	2621.27	3900.79	4693.80	25.87	•	00.00	25.87	4667.93
	1/20/94	2621.27	3900.79	4693.80	25.96	1	00.0	25.96	4667.84
	2/3/94	2621.27	3900.79	4693.80	25.82	٠	00.00	25.82	4067.98
	2/17/94	2621.27	3900.79	4693.80	25.68	•	00.0	25.68	4668.12
	3/3/94	2621.27	3900.79	4693.80	29.22	•	00'0	29.22	4664.58
	3/17/94	2621.27	3900.79	4693.80	26.21	•	00.00	26.21	4667.59
	3/31/94	2621.27	3900.79	4693.80	26.32	•	00.00	26.32	4667.48
	4/14/94	2621.27	3900.79	4693.80	26.37	•	00.0	26.37	4667.43
MW-8 (TWP-1)	3/18/93	2449.70	3893.96	4688.02	24.92	24.72	0.20	24.77	4663.25
	4/21/93	2449.70	3893.96	4688.02	23.47	23.42	0.05	23.43	4664.59
	4/29/93	2449 70	3893.96	4688.02	23.21	22.90	0.31	22.98	4665.04
	8/9/5	2449.70	3893.96	4688.02	22.85	22.50	0.35	22.59	4665.43
	\$/20/93	2449.70	3893.96	4688.02	22.50	22.08	0.42	22.19	4665.84
	6/17/93	2449.70	3893.96	4688.02	21.72	21.71	0.01	11.71	4666.31
	6/23/93	2449.70	3893.96	4688.02	21.95	21.81	0.14	21.85	4666.18
	7/1/93	2449.70	3893.96	4688.02	21.75	21.60	0.15	21.64	4666.38
	7/8/93	2449.70	3893.96	4688.02	21.82	21 73	0.10	21.75	4666.28
	12/28/93	2449.70	3893.96	4688.02	21.42	21.33	60'0	21.35	4666.67
	1/20/94	2449.70	3893.96	4688.02	21.63	21.55	80.0	21.57	4666.45
	2/17/94	2449.70	3893.96	4688.02	21.17	21.16	10.0	21.16	4666.86
	3/3/94	2449.70	3893.96	4688.02	21.75	21.74	0.01	21.74	4666.28
	3/17/94	2449.70	3893.96	4688.02	21.65	•	0.00	21.65	4666.37
	3/31/94	2449.70	3893.96	4688.02	21.93		00.00	21.53	4666.09
	4/14/94	2449.70	3893.96	4688.02	21.82	21.82	0.00	21.82	4666.20
MW-9 (TWP-2)	3/18/93	2529.21	3930.05	4692.09	27.25	26.90	0.35	56.99	4665.10
	4/21/93	2529.21	3930.05	4692.09	24.64	24.44	0.20	24.49	4667.60
	4/29/93	2529.21	3930.05	4692.09	24.30	23.81	0.49	23.93	4668.16
	5/6/93	2529.21	3930.05	4692.09	23.84	23.44	0.40	23.54	4668.55
	5/20/93	2529.21	3930.05	4692.09	23.24	22.76	0.48	22.88	4669.21
	6/11/93	2529.21	3930.05	4692.09	22.36	22.00	0.36	22.09	4670.00
	6/23/93	2529.21	3930.05	4692.09	22.59	21.91	89.0	22.08	4670.01
	7/1/93	2529.21	3930.05	4692.09	21.94	21.66	0.28	21.73	4670.36

GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
Location	Date	Easting	Northing	(ft msl)	(f) BTOC)	(ft BTOC)	(feet)	(f) BTOC)	(fi msl)
	7/8/93	2529.21	3930.05	4692.09	22.03	21.61	0.42	21.72	4670.38
	12/28/93	2529.21	3930.05	4692.09	21.77	21.51	0.26	21.58	4670.52
	1/20/94	2529.21	3930.05	4692.09	22.63	21.90	0.73	22.08	4670.01
	2/17/94	2529.21	3930.05	4692.09	21.75	21.73	0.02	21.74	4670.36
	3/3/94	2529.21	3930.05	4692.09	22.28	22.27	10.0	22.27	4669.82
	3/17/94	2529.21	3930.05	4692.09	22.43	22.23	0.20	22.28	4669.81
	3/31/94	2529.21	3930.05	4692.09	22.86	22.45	0.41	22.55	4669.54
	4/14/94	2529.21	3930.05	4692.09	22.69	22.39	0.30	22.47	4669.63
MW-10	2/17/93	2354.84	3397.60	4662.67	30.18	29.18	1.00	29.43	4633.24
	3/18/93	2354.84	3397.60	4662.67	29.90	29.02	88.0	29.24	4633.43
	4/2/93	2354.84	3397.60	4662.67	30.10	29.12	0.98	29.37	4633.31
	4/21/93	2354.84	3397.60	4662.67	30.12	29.11	1.01	29.36	4633.31
	4/29/93	2354.84	3397.60	4662.67	30.07	29.03	1.04	29.29	4633.38
	\$/6/93	2354.84	3397.60	4662.67	29.85	28.77	1.08	29.04	4633.63
	\$/20/93	2354.84	3397.60	4662.67	29.73	28.63	1.10	28.91	4633.77
	6/17/93	2354.84	3397.60	4662.67	29.43	28.35	1.08	28.62	4634.05
	6/23/93	2354.84	3397.60	4662.67	29.68	28.48	1.20	28.78	4633.89
	7/1/93	2354.84	3397.60	4662.67	29.50	28.31	1.19	28.61	4634.06
	7/8/93	2354.84	3397.60	4662.67	29.51	28.29	1.22	28.60	4634.08
	8/23/93	2354.84	3397.60	4662.67	28.44	28.26	0.00	28.44	4634.23
	12/28/93	2354.84	3397.60	4662.67	28.47	28.27	0.20	28.32	4634.35
	1/20/94	2354.84	3397.60	4662.67	28.48	28.34	0.14	28.38	4634.30
	2/3/94	2354.84	3397.60	4662.67	28.21	27.99	0.22	28.05	4634.63
	2/17/94	2354.84	3397.60	4662.67	28.10	27.90	0.20	27.95	4634.72
	3/3/94	2354.84	3397.60	4662.67	28.79	28.74	0.05	28.75	4633.92
	3/17/94	2354.84	3397.60	4662.67	28.42	28.35	0.07	28.37	4634.30
	3/31/94	2354.84	3397.60	4662.67	28.69	28.60	0.09	28.62	4634.05
	4/14/94	2354.84	3397.60	4662.67	28.97	28.95	0.02	28.96	4633.72
MW-11	2/12/93	1923.08	3213.91	4637.37	26.73		00:0	26.73	4610.64
	3/18/93	1923.08	3213.91	4637.37	26.20		0.00	26.20	4611.17
	4/2/93	1923.08	3213.91	4637.37	26.00	•	0.00	26.00	4611.37
	4/21/93	1923.08	3213.91	4637.37	25.98		0.00	25.98	4611.39
	4/29/93	1923.08	3213.91	4637.37	25.98	•	00:00	86.52	4611.39

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GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample		_	Elevation	to Water	Product	Thickness	to Water*	Elevation
ocation	Date	Easting	Northing	(ft msl)	(ft BTOC)	(ft BTOC)	(feet)	(ft BTOC)	(ft msl)
	8/9/5	1923.08	3213.91	4637.37	25.79	•	0.00	25.79	4611.58
	5/20/93	1923.08	3213.91	4637.37	25.85	•	00'0	25.85	4611.52
	6/11/93	1923.08	3213.91	4637.37	25.62	•	00.00	29:52	4611.75
	6/23/93	1923.08	3213.91	4637.37	25.75	•	00.00	25.75	4611.62
	7/1/93	1923.08	3213.91	4637.37	25.74	•	00.00	25.74	4611.63
	7/8/93	1923.08	3213.91	4637.37	26.70		00.00	26.70	4610.67
	8/23/93	1923.08	3213.91	4637.37	26.37	•	00.0	26.37	4611.00
	12/28/93	1923.08	3213.91	4637.37	26.67		00'0	26.67	4610.70
	1/20/94	1923.08	3213.91	4637.37	26.49		00.00	26.49	4610.88
	2/3/94	1923.08	3213,91	4637.37	26.55		00.00	26.55	4610.82
	2/17/94	1923.08	3213.91	4637.37	26.41		00.00	26.41	4610.96
	3/3/94	1923.08	3213.91	4637.37	26.78		00.00	26.78	4610.59
	3/17/94	1923.08	3213.91	4637.37	26.45		00.00	26.45	4610.92
	3/31/94	1923.08	3213.91	4637.37	26.85		00'0	26.85	4610.52
	4/14/94	1923.08	3213.91	4637.37	26.82	•	00.00	26.82	4610.55
MW-12	2/12/93	2457.72	3650.34	4676.87	25.84	25.75	60'0	25.77	4651.10
	3/18/93	2457.72	3650.34	4676.87	25.80	25.70	0.10	25.73	4651.15
	4/2/93	2457.72	3650.34	4676.87	25.71	25.62	0.09	25.64	4651.23
	4/21/93	2457.72	3650.34	4676.87	25.35	25.31	0.04	25.32	4651.55
	4/29/93	2457.72	3650.34	4676.87	25.29	25.27	0.02	25.28	4651.60
	\$/6/93	2457.72	3650.34	4676.87	25.16	•	0.00	25.16	4651.71
	5/20/93	2457.72	3650.34	4676.87	24.83	•	0.00	24.83	4652.04
	6/11/93	2457.72	3650.34	4676.87	24.02	24.01	0.01	24.01	4652.86
	6/23/93	2457.72	3650.34	4676.87	24.00	23.99	0.01	23.99	4652.88
	7/1/93	2457.72	3650.34	4676.87	23.77	23.75	0.02	23.76	4653.12
	7/8/93	2457.72	3650.34	4676.87	23.87	23.84	0.03	23.85	4653.02
	8/23/93	2457.72	3650.34	4676.87	23.14	23.13	0.00	23.14	4653.73
	12/28/93	2457.72	3650.34	4676.87	23.21	23.20	0.01	23.20	4653.67
	1/20/94	2457.72	3650.34	4676.87	23.28	23.27	0.01	23.27	4653.60
	2/3/94	2457.72	3650.34	4676.87	23.16	23.15	0.01	23.15	4653.72
	2/17/94	2457.72	3650.34	4676.87	23.02	22.87	0.15	22.91	4653.96
	3/3/94	2457.72	3650.34	4676.87	23.75	23.74	0.01	23.74	4653.13
	3/17/94	2457.72	3650.34	4676.87	23.44	٠	0.00	23.44	4653.43

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GROUND WATER ELEVATION AND MOBILE LNAPL THICKNESS DATA UST SITE 870 INTRINSIC REMEDATION EE/CA HILL AFB, UTAH

				Datum	Measured Depth	Depth to	Product	Corr. Depth	Corr. GW
Sample	Sample			Elevation	to Water	Product	Thickness	to Water*	Elevation
ocation	Date	Easting	Northing	(ft msl)	(ft BTOC)	(ft BTOC)	(feet)	(ft BTOC)	(ft msl)
	3/31/94	2457.72	3650.34	4676.87	23.80	•	0.00	23.80	4653.07
	4/14/94	2457.72	3650.34	4676.87	24.11	•	0.00	24.11	4652.76
VIW-13	12/28/93	2573.50	3896.74	4689.21	25.93	19.75	6.18	21.30	4667.92
	1/20/94	2573.50	3896.74	4689.21	23.67	21.74	1.93	22.22	4666.99
	2/3/94	2573.50	3896.74	4689.21	23.86	21.48	2.38	22.08	4667.14
	2/17/94	2573.50	3896.74	4689.21	23.88	21.30	2.58	21.95	4667.27
	3/3/94	2573.50	3896.74	4689.21	24.29	21.92	2.37	22.51	4666.70
	3/17/94	2573.50	3896.74	4689.21	24.43	21.82	2.61	22.47	4666.74
	3/31/94	2573.50	3896.74	4689.21	23.21	22.71	0.50	22.84	4666.38
	4/14/94	2573.50	3896.74	4689.21	22.95	22.70	0.25	22.76	4666.45
MW-14	12/28/93	2548.14	3861.96	4686.21	26.21	21.25	4.96	22.49	4663.72
	1/20/94	2548.14	3861.96	4686.21	23.40	21.01	2.39	21.61	4664.60
	2/3/94	2548.14	3861.96	4686.21	23.09	20.59	3.31	20.61	4665.60
	2/17/94	2548.14	3861.96	4686.21	24.50	20.18	4.32	21.26	4664.95
	3/3/94	2548.14	3861.96	4686.21	25.78	20.63	5.15	21.92	4664.29
	3/17/94	2548.14	3861.96	4686.21	28.42	24.44	3.98	25.44	4660.78
	3/31/94	2548.14	3861.96	4686.21	23.05	22.43	0.62	22.59	4663.63
	4/14/94	2548.14	3861.96	4686.21	22.50	22.12	0.38	22.22	4664.00

SDNA = Surveyor's Data Not Available

* Corrected Depth to Water = Measured Depth to Water - (0.75 x Product Thickness)

NA = Not Available

ft msl = Feet Above Mean Sea Level

ft BTOC = Feet Below Top of Casing

APPENDIX C

SOIL AND GROUND WATER ANALYTICAL DATA



Ref: 93-BN4/vg

August 16, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

ATTENTION OF: Roger L. Cosby

Dear Don:

Please find attached test results for methane, carbon dioxide, and oxygen on Hill AFB samples as per Service Request #SF-0-1. Samples were received on August 5 and 9, 1993, and analyzed on August 9-10, 1993. Samples were prepared as described in the paper "Dissolved Oxygen and Methane in Water by a GC Headspace Equilibrium Technique", by Kampbell et al., in <u>International Journal of Environmental Chemistry</u>, Vol. 36, pp. 249-257. Analysis and calculations of carbon dioxide and oxygen were performed as per RSKSOP-114(TCD). Analysis and calculations of methane were performed as per RSKSOP-147(FID).

If you have any questions, please feel free to see me.

Sincerely,

Bryan Newell

xc: J.L. Seeley S.A. Vandegrift

J.T. Wilson

M. Cook

ANALYZED 8/9-10/93			
SAMPLE	METHANE	CARBON DIOXIDE	OXYGEN
71-CPT-GEO DEPTH1	0.0192	838	6.09
71-8CPT-GEO DEPTH1	0.0212	1224	0.93 ×
71-17CPT-GEO DEPTH1	0.0044	518	8.68 🗶
71-17CPT-GE0 DEPTH2	0.0064	607	2.58 2
71-18CPT-GEO DEPTH1	0.0007	398	6.80 🔓
71-18CPT-GEO DEPTH2	0.0017	479	2.78 4
71-19CPT-GEO DEPTH1	0.0564	708	2.50 🗡
71-19CPT-GEO DEPTH1 DUP	0.0552	707	0.81 😽
71-23CPT-GEO DEPTH1	9.0001	433	6.91 ት
71-29CPT-GEO DEPTH1	0.0007	380	4.67
71-29CPT-GEO DEPTH2	0.0541	364	2.52
71-31CPT-GEO DEPTH1	0.0032	511	7.21 4
71-31CPT-GEO DEPTH2	0.0111	603	7.17
71-38CPT-GEO DEPTH1	0.0350	897	4.19
71-39CPT-GEO DEPTH1	0.0141	761	1.70
71-39CPT-GEO DEPTH1 DUP	0.0219	1183	1.42 <
LOWER LIMIT OF QUANTITATION	0.0009	0.17	0.29
UPPER LIMIT OF QUANTITATION	0.9445	1521	52.37

UNITS ARE mg/L.

Missing dota m EPA wells.



Ref: 93-TH9/vg

93-PR9/vg

93-LP5/vg

August 17, 1993

Dr Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

ATTENTION OF: Roger L. Cosby

Dear Don:

Attached are the results of 14 Hill AFB samples submitted to ManTech Environmental as part of Service Request #SF-0-1. samples were received on August 6 and 9, 1993, and analyzed August 6, 9, 10, and 11, 1993. The methods used for analysis were EPA 350.1, 353.1, Water's capillary and 365.1 and Blanks, spikes, duplicates, and electrophoresis method N-601. known AQC samples were analyzed along with the samples for quality

If you have any questions concerning these results, please feel free to contact us.

Sincerely,

Tim Hensley

Priscilla Rhynes

Lynda Pennington

xc: S.A. Vandegrift SAV J.L. Seeley

mg/1 T-P(P)	6.21	6.23	8.40	•	13.0	٠ د	•	.10	<.05	<.05	9.42	5.94	4.33		44	•	•		•	•	3.29		102\$	*66
$\frac{mg/1}{NH_3(N)}$.30	.21	.26	.T.	11.	66.	.30	< .05	.19		<.05	<.05	<.05		14	•	70.	, , ,)) ;	9.68	9.66	9.80	106%	103%
mg/1 NO ₂ +NO ₃ (N)	3.78	2.13	T.83	7.7.7 00 °C		.19	1.40	3.90	1.59		9	4.69	. 7		2.70		4.17	4.13		0	7.12	~	1048	σ
mg/1 so_	74.4	8.C2	54.8	0 . Q.C	8.66	5.68	1 4 1	52.6	! !		46.9	47.4	58.0		51.2		9	31,5		!		1 1	101%	928
mg/l cl	71.5	ה פר ר	60T	90.2	90.3	50.5	1 1 1	107	!!!!		•	91.7	^		118		161	114	116	:		1 1	103%	0 ት
			2	r S	Dup	1				Dap						dng	ı		Dup					
	Depth 1				Depth	Depth	Depth	Depth	Depth	Depth	Depth				Depth 1			Depth 2					>-	
8/5/93 <u>Sample</u>	71-17CPT-GEO	1-18CPT-GEO	-18CPT-GEO	1-18CPT-GEO	-18CPT-GEO	1-19CPT-GEO	1-29CPT-GEO	1-29CPT-GEO	1-29CPT-GEO	1-29CFT-GEO	1-31CPT-GEO	1-31CPT-GEO	/1-38CPT-GEO	8/6/8	71-23CPT-GEO	71-23CPT-GEO	71-39CPT-GEO	71-39CPT-GEO	71-39CPT-GEO	AQCWP030		rue.	Spike Recovery	

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Ref: 93-LP8/vg

August 25, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab U.S. Environmental Protection Agency

P.O. Box 1198 Ada, OK 74820

THRU: S.A. Vandegrift St.

Dear Don:

Below are TOC results for a set of nine aqueous samples submitted to ManTech Environmental August 24, 1993 as a part of Service Request #SF-0-5. The samples were analyzed on the day of receipt using RSKSOP-102. Blanks, duplicates, and known PE samples were analyzed along with your samples for quality control.

Please note that sample "82-MW-10" exhibited an immiscible phase floating on the surface of the sample. An aliquot of sample was taken from below this phase for analysis of TOC.

If you have any further questions concerning this data, please feel free to contact me.

Sincerely,

Lynda Pennington
Lynda Pennington

xc: R.L. Cosby J.L. Seeley

J.T. Wilson

<u>Sample</u>	mg/L TOC	
82A 82B 82C 82C Dup 82D 82E 82F 82H	4.2 \ 2.1 \ 9.4 \ 9.5 \ 8.1 ' 1.7 ' 2.2 \ 2.2 \	
82-MW-10 82-MW-11	27.8 8.0	
17 TH T	8.0	
82-M2-11 Dup WP030 II		
WP030 II T.V.	14.0 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	

ManTech Environmental Technology, Inc.

<u>Sample</u> mq/L TOC 71-CPT-GEO Depth 1 2.3 3.6 / 71-17CPT-GEO Depth 1 2.1 71-17CPT-GEO Depth 2 1.6 71-18CPT-GEO Depth 2 5.4/ 71-19CPT-GEO Depth 1 2.7 71-29CPT-GEO Depth 1 1.9/ 71-29CPT-GEO Depth 2 2.0 71-29CPT-GEO Depth 2 Dup 8.7 WP030 I 2.7 71-31CPT-GEO Depth 1 1.9 71-31CPT-GEO Depth 2 71-38CPT-GEO Depth 1 3.3 / 71-38CPT-GEO Depth 1 Dup 3.3 / WP030 I 8.5 8.0 71-8CPT-GEO Depth 1 2.1 / 71-23CPT-GEO Depth 1 2.8 / 71-39CPT-GEO Depth 1 2.9 / 71-39CPT-GEO Depth 1 Dup 8.7 🗸 WP030 I

True Value of WP030 I = 8.6



Ref: 93-PR12/vg 93-MW13/Vg

August 26, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. BOX 1198 Ada, OK 74820

THRU: S.A. Vandegrift Con

Dear Don:

Attached are the results of 10 microcosm samples submitted to ManTech Environmental as part of Service Request #SF-0-5. The samples were received on August 24, 1993, and analyzed immediately. The methods used for analysis were EPA methods 350.1, 353.1, and 365.1 and Water's capillary electrophoresis method N-601. Blanks, spikes, duplicates, and known AQC samples were analyzed along with the samples for quality assurance.

If you have any questions concerning these results, please feel free to contact us.

xc: R.L. Cosby

J.L. Seeley

J.T. Wilson

Sample	mg/l NO ⁻ 2 + NO ⁻ 3(N)	mg/l NH ₃ (N)	mg/l T-P	mg/l Cl	mg/1 80'2
82-A	.14	<.05	.14	170	66.4
82-B	.25	<.05	. 08	163	76.9
82-C	13	<.05	.24	164	49.9 /
82-C Dup	4		.20	16)	/2 /
82'-D	.53	. 07	.35	198	193 7
82-D Dup	•53	• 05			
82-E	4.40	<.05	<.05	77.1	39.6
82-E Dup				78.3	39.8 4/
82-F	7.41	<.05	<.05	68.5	63.9 //
82-F Rep	7.46	<.05	<.05	71.8	67.9//
82-H	2.12	<.05	<.05	136	59.7
MW-10	9.16	<.05	6.26	44.7	63.2
MW-11	.36	.25	3.77	48.7	97.6/
AQC	7.00	9.85	2.93	176	39.6
True Value	7.10	9.80	3.20	172	42.0
Spike Rec.	102%	103%	97%	928	103%

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MANICATUATIA (TECHIO () () () ()

Ref: 93-DK4/vg

September 1, 1993

Tor. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift SAY

Dear Don:

Please find attached results of GC/MSD analysis of Hill AFB core extracts for quantitation of Benzene, Toluene, Ethylbenzene (EB), p-Xylene, m-Xylene, o-Xylene, 1,3,5-Trimethylbenzene (1,3,5-TMB), 1,2,4-Trimethylbenzene (1,2,4-TMB) and 1,2,3-Trimethylbenzene (1,2,3-TMB) as requested under Service Request #SF-0-5.

The analytical method was a modification of RSKSOP-124. Cool (38°C) on-column injection (0.5 μ l) was used with electronic pressure control (EPC) set for a constant flow of 0.9 ml/min. A 30M X 0.25 mm Restek Stabilwax (Crossbonded Carbowax-PEG, 0.5 μ m film) capillary GC column with 1 foot long X 0.53 mm ID uncoated capillary precolumn was used. Quantification was based on two standard curves: A low level curve was used for extract concentrations in the range 0.01-1.0 μ g/ml (0.01,0.1,1.0 μ g/ml). The second curve was used for quantification of concentrations >1.0 (1,10,100,333 μ g/ml).

If you require further information, please feel free to contact me.

Sincerely,

David A. Kovacs

G. Smith
J.L. Seeley

Sail	Kn-x

Page 1 of 6 Printed: 9/1/93

BLQ < 0.01 µg/ml

Analyst: David A. Kovacs

										22
SR#SF-0-5	.Kampbell		HIIIAFB	B Core Extracts GCISD Analyses	G SD Anal)	808		Units.	Units = mg/kg	• .
AMPLE NAME	BENZENE	TOLUENE	<u>E</u>	P-XYLENE	m-XYLENE	o-XYLENE	1,3,5-TMB	1.2.4-TMB	1,2,3-TMB	
1 µg/ml	9.06E-01	1.00E+00	1.07E+00	1.05E+00	1.06E+00	1.09E+00	1.10E+00	1.09E+00	1.07E+00	
82A-1	2	QN	Q	Q	Q	2	Q	2	Q	
82A-2	QX	Q	Q	Q	QN	Q	QX	Q	Q.	
82A-3	ON.	Q	Q	Q	Q.	2	2	Q	2	
82A-4	Q	2	Q	Q	2	Q	Q	S	9	
82A-5	2	2	Q	Q.	Q.	2	2	2	Q	
82A-6	Q	9	Q	Q	<u>Q</u>	9	Q	Q	9	
82A-7	2	2	Q	0	2	2	Q	2	2	
82A-8	Q	2	Q	Š	9	Q	2	2	2	
82A-9	Q	QN	QN	QX	Q	Q	Q.	2	2	
82A-10	2	QN	Q	Q.	2	S	2	2	9	
10 µg/ml	1.06E+01	1.04E+01	1.04E+01	1.03E+01	1.05E+01	1.05E+01	1.05E+01	1.05E+01	1.05E+01	
1 µg/ml	1.07E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	
82A-11	Q	Q	Q	Q	Q	2	2	Q	2	
82A-12	Q	9	8	Q	Q	Q	Q	Q	Q	
82A-13	2	Q	Q	2	Q	Q	2	2	9	
82A-14	Q	Q	2	Q	2	Q	Q	Q	2	
82A-15	9	2	Q	2	Q	2	2	2	Q	
82A-16	8	Q	Q	2	2	Q	2	2	2	
82A-17	2	Q.	Q	Q	2	Q	2	2	2	
82A-18	QX	Q	Q	QX	2	Q	Š	2	2	
82A-19	QN	Q	Q	Q	Q	2	2	2	Q	
82A-20	Q	S	Q	Q	Q	2	Q	2	Q	<i>(</i>
100µg/ml	1.05E+02	1.06E+02	1.07E+02	1.08E+02	1.06E+02	1.06E+02	1.06E+02	1.07E+02	1.07E+02	
00 µg/ml QC	9.72E+01	9.35E+01	9.28E+01	9.29E+01	9.19E+01	9.19E+01	9.18E+01	9.23E+01	9.20E+01	
82A-21	9	S	Q	2	2	2	2	2	9	
82A-22	2	Q	2	9	2	Q	2	2	2	
82A-23	2	2	Q	Q	2	2	2	2	2	
82A-24	Š	QN	Q	QV	S	QN	Q	Š	2	
82A-25	QX	Q	Q.	Q	Q	9	Q	2	2	
82A-26	2	Š	Q	8	Q	Q	2	Q	2	
82A-27	2	S	2	2	2	2	2	2	2	
82A-28	2	S	9	2	2	2	2	2	2	∑G(
82A-29	Q	Q	Q	Q	Q	Q	9	9	Š	Ĺ
										· K

82A-30 ND	Q	9	NO NO	ND	ND CV	ON ON	ON ON	1.2.3-1MB
BLQ	BLQ	BLQ	Ş	BLQ	BLQ	BLQ	BLQ	2 2
1.08E-01	9.95E-02	1.01E-01	9.94E-02	9.81E-02	1.02E-01	1.01E-01	1.01E-01	1.03E-01
1.11E-02	9.74E-03	1.04E-02	1.02E-02	1.01E-02	1.09E-02	1.28E-02	1.05E-02	1.22E-02
9.62E-01	9.30E-01	9.20E-01	9.10E-01	9.13E-01	9.35E-01	9.33E-01	9.17E-01	9.23E-01
Q.	9	Q	9	9	Q	Q	2	2
2	2	Q	Q	2	Q	2	9	2
<u>Q</u>	2	Q	S	2	QV	2	9	ا چ
Q	2	9	Q.	Q	Q	2	2	Q
2	2	Q	9	Q	9	8	2	Ş
Q	9	Q	Q	2	Q	2	Q	2
2	9	Q	Q	Q	Q	2	2	Q
2	2	Q	Q	Q	Q	2	2	2
2	Q	Q	Q	2	Q	2	2	2
QN	Q	S	Q	9	Ş	S	8	2
1.04E+02	1.06E+02	1.06E+02	1.06E+02	1.06E+02	1.06E+02	1.06E+02	1.06E+02	1.06E+02
9.56E+00	9.35E+00	9.51E+00	9.19E+00	9.39E+00	9.42E+00	9.36E+00	9.41E+00	9.44E+00
2	9	Q	9	Q	<u>Q</u>	Q	2	2
Q.	Q	Q	Q	QN	QN	Q	S	2
Q	9	Q	Q	Q	Q	2	Š	S
2	9	Q	Q	Q	Q	2	2	2
Q	Q	2	Q	2	S	Q	Q	2
Q	Q	S	Q	S	Q	Q	2	Q.
2	Q	Q	Q	Q	8	Q	9	2
Q	2	Q	2	8	Q	2	2	2
Q	Q	2	8	Q	Q	Q	Q	2
Q	2	Q		Q	Q.	9	2	2
1.04E+00	1.04E+00	1.05E+00		1.06E+00	1.04E+00	1.05E+00	1.04E+00	1.04E+00
1.18E-01	1.11E-01	1.10E-01		1.11E-01	1.10E-01	1.12E-01	1.12E-01	1.13E-01
Q	2	Q		2	2	2	Q	2
Q	2	9		Q	Q	2	2	2
9	Q	Q		Q	2	Q	2	2
2	오	Q		2	2	2	S	2
2	Q	Ç		S	2	5	2	2

*

23.

Units = mg/_{hy}

HIII AFB Core Extracts G. MSD Analyses

SR#SF-0-5 ... Kampbell

Ş	2	Q	2	2	1.11E-02	9 34E-02		9.56E-01	9.56E-01 9.34E+00	9.56E-01 9.34E+00 1.04E+00	9.56E-01 9.34E+00 1.04E+00 ND	9.56E-01 9.34E+00 1.04E+00 ND	9.56E-01 9.34E-00 1.04E-00 ND ND	9.56E-01 9.34E-400 1.04E-400 ND ND	9.56E-01 9.34E-400 1.04E-400 ND ND ND	9.56E-01 9.34E-00 1.04E-00 ND ND ND ND	9.56E-01 9.34E-400 1.04E-400 ND ND N	9.56E-01 9.34E-400 1.04E-400 ND ON	9.56E-01 1.04E-400 ND ND N	9.56E-01 1.04E-400 ND ND N	9.56E-01 -0.24E-00 -0.24E-00 -0.25E-	9.56E-01 1.04E-00 1.04E-00 ND ND N	9.56E-01 9.34E-00 1.04E-00 ND ND ND ND ND ND ND ND ND ND	9.56E-01 9.34E-400 1.04E-400 ND ND ND ND ND ND ND ND ND 1.05E-01	9.56E-01 9.34E-400 1.04E-400 ND ND N	9.56E-01 9.34E-00 1.04E-00 ND ND ND ND 1.05E-01 ND	9.56E-01 1.04E-00 1.04E-00 ND ND ND ND 1.05E-01 ND ND ND ND ND ND ND ND ND ND ND ND ND	9.56E-01 9.34E-00 1.04E-00 ND ND ND ND ND ND ND ND ND ND	9.34E-00 1.04E-00 ND ND N	9.346-09 1.046-00 ND ND ND ND ND ND ND ND ND ND	9.56E-01 1.04E-00 ND ND N	9.56E-01 1.04E-00 1.04E-00 ND ND N	9.56E-01 9.56E-01 9.34E-00 1.04E-00 1.04E-00 1.04E-00 ND ND ND ND ND ND ND ND ND ND
2	2	2	2	2	1.35E-02	9.29E-02	9.46E-01	000.100	8.30F+00	4.30E+00 1.03E+00	#.30E+00 1.03E+00 ND	4.30E+00 1.03E+00 ND ND	8.30E+00 1.03E+00 ND ND ND	2.30E+00 1.03E+00 ND ND ND	1.03E+00 1.03E+00 ND ND ND ND	2.30 2.03 2.03 2.03 2.00 3.00 3.00 3.00	2.30 2.03 2.03 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0	2.5.2. 2.0.1. 0.0.0. 0.0.0.0.0.0.0.0.0.0.0.0.0.0	2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	2.30 2.03 2.03 2.03 2.03 2.03 2.03 2.03	2.30 2.03 2.03 2.03 2.03 2.03 2.03 2.03	1.03E+00 1.03E+00 ND ND ND ND ND ND ND ND	1.03E-00 1.03E-00 ND ND ND ND ND ND ND 1.04E-01	8.30E-400 1.03E-400 ND ND ND ND ND ND 1.04E-01 8.43E-01	1.03E-00 1.03E-00 ND ND ND ND ND 1.04E-01 ND	8.30E-400 1.03E-400 ND ND ND ND ND 1.04E-01 ND ND ND	1.03E-00 1.03E-00 ND ND ND ND 1.04E-01 ND ND ND ND	1.03E-00 1.03E-00 ND ND ND ND 1.04E-01 ND ND ND ND ND	8.30 1.03	8.30 1.03 ND ND ND ND 1.04E-01 ND ND ND ND ND ND ND ND ND ND ND ND ND	2.30 2.30 1.03 E-00 ND ND N	2.30 1.03	2.30 1.03 ND ND ND ND ND ND ND ND ND ND ND ND ND
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2	9	Q	Q	2	1.14E-02	9.38E-02	9.38E-01	9.36E+00	40. LOO	1.02E+00	1.02E+00 ND	1.02E+00 ND ND	1.02E+00 ND ND ND	ND ND ND ND	ND N	N N D ON							ND ND ND ND ND ND ND ND ND ND ND ND ND N	ND ND ND ND ND ND ND ND ND ND ND ND ND N	1.02E-500 ND ND ND ND ND ND ND ND 1.05E-01 ND	1.02E-400 ND ND ND ND ND ND 1.05E-01 ND	1.02E-50 ND ND ND ND ND ND 1.05E-01 ND ND ND	1.02E-50 ND ND ND ND ND ND 1.05E-01 ND ND ND	1,02E-50 N N N N N N N N N N N N N N N N N N N	1,02E-50 N N N N N N N N N N N N N N N N N N N	1.02E-50 N N N N N N N N N N N N N N N N N N N	1.02E-30 N N N N N N N N N N N N N N N N N N N	1.02E-50 N N N N N N N N N N N N N N N N N N N
2	2	Q	Q	2	1.13E-02	9.41E-02	9.47E-01	1.00E+01	1.02E+00		2	O Q	222	2222	2222	22222	222222	222222	2222222	22222222	22222222	2 2 2 2 2 2 2 2 2 2 3 2 3 3 3 3 3 3 3 3	N N N N N N N N N N N N N N N N N N N	ND ND ND ND ND ND ND 1.04E-01	ND ND ND ND ND ND 1.04E-01 ND	ND N	ND N	NO N	NO N	ON O	N	ON O	ON O
9	2	2	2	2	1.10E-02	9.36E-02	9.60E-01	9.52E+00	9 97F_01		2	Q Q	222	2 2 2 2						222222222			ND ND ND ND ND ND ND ND ND ND ND ND ND N	ND ND ND ND ND ND ND ND ND ND ND ND ND N	ND ND ND ND ND ND ND ND 1.03E-01 ND	ND ND ND ND ND ND 1.03E-01 ND ND ND ND ND	ND ND ND ND ND 1.03E-01 ND ND ND ND	ND ND ND 1.03E-01	NO N	ND N	NO N	8	8
2	2	9	2	2	1.31E-02	8.94E-02	9.58E-01	9.25E+00	9 17F.D1		NO.	NON	0 Q Q				22222			2 2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2		ND ND ND ND ND ND ND ND ND ND ND ND ND N	ND ND ND ND ND ND ND ND ND ND ND ND ND N	ND ND ND ND ND ND ND 1.02E-01 ND	ND ND ND ND ND ND 1.02E-01 ND ND ND ND ND ND	ND N	ND N	ND N	N N N N N N N N N N N N N N N N N N N	N N N N N N N N N N N N N N N N N N N	8	8
28-1	28-2	328-3	82B-4	82B-5	01 µg/ml	.1 µg/ml	lm/gd l	ng/ml QC	1 /m/		82B-6	828-6 828-7	82B-7 82B-7 82B-8	82B-6 82B-7 82B-8 82B-8	828-6 828-7 828-8 828-8 828-9	828-6 828-7 828-8 828-9 828-10 828-11	828-6 828-7 828-8 828-8 828-10 828-11	828-6 828-7 828-8 828-9 828-10 828-11 828-13	828-6 828-7 828-8 828-9 828-10 828-11 828-13	828-6 828-7 828-8 828-9 828-10 828-11 828-12 828-14	828-6 828-7 828-8 828-9 828-10 828-11 828-12 828-14 828-14	828-6 828-8 828-8 828-8 828-10 828-11 828-14 828-14 828-16	828-6 828-8 828-8 828-9 828-10 828-12 828-14 828-15 828-16 MeCi2	828-6 828-8 828-8 828-9 828-10 828-11 828-14 828-15 828-16 NeCl2	828-6 828-8 828-8 828-9 828-10 828-11 828-14 828-16 NeCi2 1,1 µg/ml	828-6 828-8 828-7 828-8 828-10 828-12 828-14 828-14 828-15 828-15 828-15 828-15 828-15 828-16	828-6 828-8 828-8 828-8 828-10 828-11 828-14 828-14 828-14 11µg/ml 11µg/ml 828-17 828-18	828-6 828-8 828-8 828-9 828-10 828-11 828-12 828-14 828-15 828-15 828-15 828-16 828-17 828-19	828-6 828-8 828-8 828-9 828-10 828-11 828-14 828-15 828-16 MeCi2 1.1 µg/ml 1 µg/ml 828-17 828-18 828-18	828-6 828-8 828-8 828-7 828-10 828-11 828-14 828-15 828-16 1,1µg/ml 1µg/ml 828-17 828-17 828-20 828-21	828-6 828-8 828-8 828-9 828-10 828-11 828-14 828-15 828-15 1,1 µg/ml 1 µg/ml 828-17 828-19 828-20 828-21	828-6 828-8 828-8 828-9 828-10 828-11 828-14 828-14 828-14 828-14 828-17 828-17 828-20 828-21 828-21 828-21	828-6 828-8 828-8 828-1 828-10 828-11 828-15 828-15 828-15 828-17 828-17 828-20 828-21 828-21 828-22

24.

Units = mg/kg

♦ HIII AFB Core Extracts GC/MSD Analyses

SR#SF-0-5 Dr. Kampbell

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Analyst: David A. Kovacs

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1,2,3-TMB	4.91E-03	9.76E+00	1.04E+02	1.08E-01	5.53E-02	2.08E-01	9.05E-01	8.13E-03	3.63E-03	2.29E-02	1.45E-02	BLQ	3.11E-03	6.48E-02	BLQ	BLQ	1.15E-02	9.52E-02	9.83E-01	BLQ	2	BLQ	BLQ (5.18E-03	1.27E-02	2.13E-02	2	2	1.09E+02	9.95E+00	8.21E-03	Q	BLQ	8.17E-01
1,2,4-TMB	1.67E-02	9.54E+00	1.04E+02	1.16E+00	1.03E+00	2.04E+00	4.42E+00	7.41E-02	1.68E-02	5.40E-02	3.71€€	BLQ	8.85E-03	2.25E-01	BLQ	BLQ	1.02E-02	9.66E-02	9.91E-01	4.98E-03	2	4.16E-03	5.72E-03	6.95E-02	3.03E-02	3.99E-02	BLQ	BLQ	1.09E+02	9.86E+00	7.80E-02	3.10E-03	1.11E-02	3.11E+00
1,3,5-TMB	1.39E-02	9.41E+00	1.04E+02	1.65E+00	1.50E+00	2.34E+00	3.70E+00	8.01E-02	1.48E-02	3.88E-02	2.90E-02	4.16E-03	1.74E-02	1.95E-01	ВГО	ВГО	1.11E-02	9.85E-02	9.88E-01	BLQ	2	6.32E-03	8.71E-03	6.37E-02	4.33E-02	3.65E-02	1.47E-02	2.58E-02	1.09E+02	1.00E+01	8.82E-02	4.77E-03	3.04E-02	2.53E+00
O-XYLENE	QN	9.77E+00	1.03E+02	1.51E-02	4.01E-03	BLQ	BLQ	BLQ	BLQ	1.36E-02	7.16E-03	ВГО	ВГО	4.51E-03	ВГО	BLQ	9.83E-03	9.86E-02	9.95E-01	BLQ	2	BLQ	4.76E-03	BLQ	3.23E-02	4.50E-02	BLQ	BLQ	1.08E+02	1.00E+01	5.77E-03	ВГО	ВГО	7.32E-01
m-XYLENE	Q	9.53E+00	1.03E+02	2.57E-02	9.10E-03	9.56E-03	6.62E-02	9.91E-03	1.89E-02	5.21E-02	4.18E-02	BLQ	3.36E-03	3.45E-02	ВГО	ВГО	1.02E-02	9.86E-02	9.98E-01	BLQ	2	1.67E-02	2.75E-02	1.94E-02	1.21E-01	1.81E-01	BLQ	BLQ	1.08E+02	1.00E+01	5.29E-03	3.03E-03	BLQ	3.40E+00
P-XYLENE	Q	9.34E+00	1.05E+02	4.20E-02	2.96E-02	3.65E-02	8.57E-02	1.10E-02	1.05E-02	2.21E-02	1.78E-02	ВГО	BLQ	1.36E-02	BLQ	BLQ	1.02E-02	9.88E-02	1.00E+00	ВГО	2	4.54E-03	7.55E-03	6.62E-02	3.90E-02	5.51E-02	BLQ	BLQ	1.08E+02	9.98E+00	3.88E-02	BLQ	1.30E-02	1.62E+00
8	Q	1.00E+01	1.03E+02	1.80E-02	6.18E-03	5.58E-03	2.86E-02	6.42E-03	7.95E-03	1.24E-02	1.18E-02	1.59E-02	3.35E-03	8.71E-03	BLQ	BLQ	1.00E-02	9.87E-02	1.00E+00	ND	2	1.15E-01	1.41E-01	1.24E-01	8.78E-02	6.13E-02	2.13E-02	3.44E-02	1.08E+02	9.96E+00	6.04E-02	9.49E-02	1.11E-01	1.48E+00
TOLUENE	Q	9.62E+00	1.03E+02	ВГО	1.76E-02	1.92E-02	2.00E-02	ВГО	BLQ	BLQ	ВГО	ВГФ	ВГО	BLQ	BLQ	ВГФ	9.59E-03	9.93E-02	1.01E+00	ВГО	ВГО	BLQ	ВГО	ВГО	BLQ	3.04E-03	ВГО	BLQ .	1.08E+02	9.98E+00	ВГО	ВГО	ВГО	ВГФ
BENZENE	QN	9.52E+00	9.87E+01	6.21E-03	BLQ	3.67E-03	3.27E-03	BLQ	BLQ	BLQ	BLQ	9.59E-03	Ş	BLQ	BLQ	2	1.02E-02	9.87E-02	1.09E+00	ВГО	BLQ	2.03E-02	1.85E-02	2.09E-02	3.43E-02	3.16E-02	6.30E-03	7.92E-03	1.13E+02	1.10E+01	8.29E-03	1.04E-02	6.97E-02	2.71E-01
SAMPLENAME	82C-16	10 µg/ml QC	100 µg/ml	82C-19	82C-20	82C-21	82C-22	82C-23	82C-24	82C-25	82C-26	820-1	820-3	82D-4	MeC12	Method Blank	0.01 µg/ml	0.1 µg/ml	1 µg/ml	820-5	820-6	82D-12	820-13	82D-14	82D-15	82D-16	820-17	82D-18	100 µg/ml	10 µg/ml	820-19	820-21	82D-22	82D-23

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Units = mg/xg

HIII AFB Core Extracts &/MSD Analyses

SR#SF-0-5 or. Kampbell

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1.2.3-TWB	1.35E-01	BLQ	3.84E-02	BLQ	1.63E-02	Q	1.00E+00	9.93E-02	2	2	Ş	9	Q	1.93E+01	BLQ	3.42E+02	2.03E+00	6.72E-01	2.34E+00	1.25E+00	9.23E+00	9.50E+01	1.01E+01	1.01E+00	7.78E-02	7.09E-02	7.83E-02	8.99E-02	1.55E-01	7.49E-02	9.09E-02	9.58E-01	2.72E-01	BLQ
1.2.4-TWB	4.40E-01	7.02E-03	1.07E-02	BLQ	3.73E-02	9	9.89E-01	9.91E-02	<u>Q</u>	2	Q	2	8	6.09E+01	BLQ	3.43E+02	8.45E+00	2.33E+00	8.37E+00	4.72E+00	9.01E+00	9.50E+01	1.02E+01	1.02E+00	2.22E-01	1.91E-01	2.06E-01	2.46E-01	4.02E-01	1.95E-01	2.44E-01	2.54E+00	7.24E-01	6.24E-03
1,3,5-TMB	3.73E-01	7.44E-03	7.33E-02	7.70E-03	4.39E-02	2	1.02E+00	1.00E-01	2	오	2	2	2	2.93E+01	BLQ	3.43E+02	2.94E+00	8.57E-01	3.04E+00	1.62E+00	8.89E+00	9.51E+01	1.03E+01	1.08E+00	8.43E-02	7.47E-02	7.96E-02	9.38E-02	1.57E-01	7.43E-02	1.03E-01	1.24E+00	3.84E-01	ВГФ
O-XYLENE	1.44E-01	3.59E-03	6.92E-02	4.86E-03	2.42E-02	2	9.93E-01	9.99E-02	Q	2	Q	2	Q	1.99E+01	ВГО	3.44E+02	5.58E+00	1.72E+00	6.28E+00	2.31E+00	9.17E+00	9.40E+01	1.00E+01	1.01E+00	3.16E-01	3.03E-01	3.21E-01	3.18E-01	5.67E-01	3.10E-01	4.03E-01	2.04E+00	7.25E-01	BLQ
M-XYLENE	5.55E-01	1.43E-02	1.01E-01	4.04E-03	1.11E-01	2	9.93E-01	1.01E-01	9	2	Q	9	ND	6.31E+01	BLQ	3.45E+02	1.05E+01	1.83E+00	4.89E+00	9.88E-01	9.02E+00	9.39E+01	9.99E+00	1.01E+00	5.17E-01	6.04E-01	6.12E-01	6.21E-01	1.16E+00	6.16E-01	8.02E-01	4.74E+00	1.84E+00	8.84E-03
D-XYLENE	2.76E-01	6.75E-03	1.05E-02	BLQ	3.78E-02	9	9.85E-01	1.01E-01	2	2	2	2	Q	2.34E+01	BLQ	3.56E+02	4.81E+00	1.48E+00	4.69E+00	2.02E+00	8.67E+00	9.08E+01	1.02E+01	1.00E+00	2.43E-01	2.21E-01	2.33E-01	2.33E-01	4.27E-01	2.28E-01	2.81E-01	1.70E+00	6.25E-01	BLQ
8	2.64E-01	1.06E-02	1.28E-01	1.37E-01	1.71E-01	2	9.94E-01	1.02E-01	Q	2	Q	Q	Q	1.12E+01	BLQ	3.44E+02	3.72E+00	1.12E+00	3.39E+00	1.31E+00	9.45E+00	9.40E+01	9.76E+00	1.02E+00	1.60E-01	1.52E-01	1.59E-01	1.50E-01	2.83E-01	1.50E-01	1.87E-01	1.03E+00	3.77E-01	вга
TOLUENE	BLQ	BLQ	8.09E-03	ВГО	ВГО	2	1.02E+00	1.03E-01	9	2	2	2	Q	2.04E-01	BLQ	3.45E+02	1.07E+00	3.04E-01	5.91E-01	1.17E-01	9.15E+00	9.47E+01	9.81E+00	1.02E+00	4.55E-02	4.36E-02	3.50E-02	9.36E-02	2.00E-01	1.59E-01	2.31E-01	3.75E+00	1.73E+00	1.68E-02
BENZENE	1.29E-01	1.03E-02	3.93E-02	3.88E-02	3.14E-02	2	1.05E+00	1.08E-01	2	2	2	2	Q	1.61E+00	BLQ	3.49E+02	5.01E-01	3.33E-01	6.53E-01	6.29E-01	1.03E+01	1.00E+02	9.74E+00	9.89E-01	6.78E-01	5.38E-01	6.65E-01	7.71E-01	1.45E+00	7.87E-01	8.66E-01	7.49E-01	4.90E-01	BLQ
AMPLENAME	82D-24	82D-25	82D-38	82D-39	82D-40	82E-2	1 µg/ml	0.1 µg/ml	82E-3	82E-13	82E-14	82E-15	82E-17	821-6	MeC12	333 µg/ml	821-15	821-16	821-17	821-18	10 µg/ml QC	100 µg/ml	10 µg/ml	1 µg/ml	821-19	821-20	821-21	821-22	821-23	821-24	821-25	821-26	821-27	821-28

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26.

Units = mg...

HIII AFB Core Extracts C. MSD Analyses

SR#SF-0-o ... Kampbell 5 x // "" 1

Analyst: David A. Kovacs

BLQ < 0.01 µg/m1

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Units=mg/kg

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SR#SF-0-5 Dr. Kampbell

BLQ < 0.01 µg/ml

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1.01E+00	9.53E-02	BLQ	BLQ	2.59E-01	3.09E+00	2	2	9	9.37E-03	1.50E+00	3.10E-02	8.23E-01	BLQ	BLQ	1.06E+01	1.04E+02
1.04E+00	9.11E-02	BLQ	BLQ	1.91E-02	7.62E+00	BLQ	2	BLQ	1.72E-02	5.38E+00	1.13E-01	3.30E+00	BLQ	BLQ	1.05E+01	1.04E+02
1.08E+00	9.35E-02	BLQ	BLQ	4.18E-01	1.31E+01	BLQ	2	ВГО	1.21E-02	2.32E+00	3.10E-02	1.27E+00	ВГО	BLQ	1.04E+01	1.04E+02
1.03E+00	9.70E-02	ВГО	BLQ	BLQ	3.76E-02	Q	2	BLQ	8.50E-02	4.79E+00	1.29E-01	1.03E+00	BLQ	ВГО	1.06E+01	1.04E+02
1.01E+00	9.92E-02	ВГО	BLQ	1.28E-02	1.79E+00	Ş	Q	2	8.98E-02	7.86E+00	6.92E-02	2.28E+00	BLQ	BLQ	1.06E+01	1.04E+02
1.01E+00	9.95E-02	BLQ	BLQ	2	1.05E+00	9	2	ВГО	3.64E-02	3.96E+00	1.54E-01	1.75E+00	ВГО	ВГО	1.04E+01	1.03E+02
1.02E+00	9.81E-02	BLQ	ВГО	1.01E-01	1.24E+00	2.71E+01	1.61E+01	BLQ	2.38E-02	2.72E+00	1.21E-01	1.31E+00	ВГО	ВГО	1.08E+01	1.04E+02
1.05E+00	1.03E-01	1.57E-02	1.11E-02	1.14E-02	3.20E-02	1.22E-02	7.30E-03	1.37E-02	1.54E-02	1.82E-01	1.88E-02	6.74E-02	BLQ	BLQ	1.06E+01	1.04E+02
1.01E+00	1.05E-01	BLQ	BLQ	BLQ	1.36E-02	BLQ	ВГО	8.31E-03	8.12E-02	7.12E-01	3.15E-01	4.22E-01	ВГО	9	1.06E+01	1.07E+02
1 µg/ml	0.1 µg/ml	821-29	821-30	821-31	821-32	821-33	821-34	821-35	821-36	821-37	821-38	821-39	MeC12	Method Blank	10 µg/ml QC	100 µg/ml
	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.08E+00 1.04E+00	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.08E+00 1.04E+00 1.05E-01 1.03E-01 9.81E-02 9.95E-02 9.70E-02 9.35E-02 9.11E-02	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.08E+00 1.04E+00 1.05E-01 9.35E-02 9.70E-02 9.70E-02 9.35E-02 9.11E-02 BLQ BLQ BLQ BLQ BLQ	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.04E+00 1.05E-01 1.03E-01 9.81E-02 9.92E-02 9.70E-02 9.35E-02 9.11E-02 BLQ 1.57E-02 BLQ BLQ BLQ BLQ BLQ BLQ	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.04E+00 1.04E+00 1.05E-01 1.03E-01 9.81E-02 9.95E-02 9.70E-02 9.35E-02 9.11E-02 BLQ 1.57E-02 BLQ BLQ BLQ BLQ BLQ BLQ 1.11E-02 BLQ BLQ BLQ BLQ BLQ BLQ 1.14E-02 1.01E-01 ND 1.28E-02 BLQ 4.18E-01 1.91E-02	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.08E+00 1.04E+00 1.05E-01 1.03E-01 9.81E-02 9.95E-02 9.70E-02 9.35E-02 9.11E-02 BLQ 1.57E-02 BLQ BLQ BLQ BLQ BLQ BLQ 1.11E-02 BLQ BLQ BLQ BLQ BLQ BLQ 1.14E-02 1.01E-01 ND 1.28E-02 BLQ 4.18E-01 1.91E-02 1.36E-02 3.20E-02 1.24E+00 1.05E+00 1.79E+00 3.76E-02 1.31E+01 7.62E+00	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.04E+00 1.05E+00 1.05E+00	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.04E+00 1.04E+01 1.04E+01 1.04E+01 1.04E+01 1.05E+00 1.79E+00 3.76E+02 4.18E+01 1.61E+01 1.06E+00 1.06E+00	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.04E+00 1.05E+00 1.05E+00	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.01E+00 1.03E+00 1.02E+00 1.01E+00 9.95E-02 9.92E-02 9.70E-02 9.35E-02 9.11E-02 9.11E-02	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.03E+00 1.02E+00 1.01E+00 1.03E+00 1.04E+00 1.05E+00 1.05E+00	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.03E+00 1.02E+00 1.01E+00 1.03E+00 1.04E+00 1.04E+00 1.05E-01 1.05E-01 9.81E-02 9.95E-02 9.92E-02 9.70E-02 9.35E-02 9.11E-02 BLQ 1.57E-02 BLQ BLQ BLQ BLQ BLQ BLQ BLQ 1.14E-02 1.01E-01 ND 1.28E-02 BLQ 4.18E-01 1.91E-02 1.36E-02 3.20E-02 1.01E-01 ND 1.79E+00 3.76E-02 1.31E-01 1.62E+00 BLQ 1.22E-02 2.71E+01 ND ND ND ND BLQ 7.30E-03 1.61E+01 ND ND ND ND 8.31E-03 1.37E-02 2.38E-02 3.64E-02 8.98E-02 1.71E-02 1.72E-02 8.12E-02 1.58E-01 1.54E-01 1.56E-02 1.29E-02 1.31E-01 1.31E-02	1.01E+00 1.05E+00 1.02E+00 1.01E+00 1.03E+00 1.02E+00 1.01E+00 1.03E+00 1.04E+00 1.04E+00 1.05E+01 1.05E+01 1.05E+02 9.95E-02 9.92E-02 9.70E-02 9.35E-02 9.11E-02 9.11E-02	1.01E+00 1.05E+00 1.01E+00 1.01E+00 1.03E+00 1.02E+00 1.01E+00 1.03E+01 1.03E+02 9.3E-02 9.1E-02 9.1E-02 9.1E-02 9.1E-02 9.1E-02 9.1E-02 9.1E-02 9.1E-02 9.3E-02 9.3E-02 9.3E-02 9.3E-02 9.1E-02 9.1E-02 9.1E-02 9.1E-02 9.1E-02 9.1E-02 9.3E-02 9.1E-02 9.3E-02 9.1E-02 9.1E-02	1.01E+00 1.05E+00 1.07E+00 1.01E+00 1.03E+00 1.02E+00 1.01E+00 1.03E+00 1.04E+00 1.04E+00 1.05E+02 9.92E-02 9.70E-02 9.35E-02 9.11E-02 9.11E-02	1μg/ml 1.01E+00 1.05E+01 1.01E+00 1.05E+01 1.05E+02 9.92E+02 9.70E+02 9.35E+02 9.70E+02 9.35E+02 9.10E+02 9.35E+02 9.10E+02 9.35E+02 9.10E+02 9.35E+02 9.10E+02 9.10E+02 9.35E+02 9.10E+02 9.10E+02 9.35E+02 9.10E+02 9.35E+02 9.35E+02 9.35E+02



Ref: 93-DK8/vg

October 21, 1993

Dr. John T. Wilson

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift APV

Dear John:

Please find attached results of GC/MSD analysis of Hill AFB core extracts for quantitation of Benzene, Toluene, Ethylbenzene (EB), p-Xylene, m-Xylene, o-Xylene, 1,3,5-Trimethylbenzene (1,3,5-TMB), 1,2,4-Trimethylbenzene (1,2,4-TMB) and 1,2,3-Trimethylbenzene (1,2,3-TMB) as requested under Service Request #SF-0-26.

The analytical method was a modification of RSKSOP-124. Cool (38°C) on-column injection (0.5 μ l) was used with electronic pressure control (EPC) set for a constant flow of 0.9 ml/min. A 30M X 0.25 mm Restek Stabilwax (Crossbonded Carbowax-PEG, 0.5 μ m film) capillary GC column with 1 foot long X 0.53 mm ID uncoated capillary precolumn was used. Quantification was based on two standard curves: A low level curve was used for extract concentrations in the range 0.01-1.0 μ g/ml (0.01, 0.1, 1.0 μ g/ml). The second curve was used for quantification of concentrations >1.0 (1, 10, 100 μ g/ml).

If you require further information, please feel free to contact me.

Sincerely,

David A. Kovačs

xc: R.L. Cosby J.L. Seeley G. Smith

Servic. . (equest SF-0-26 Dr. Wilson

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1.2.3-TMB	0 15()	1 07 11	4 74 11 400	2 626 404	6.33E+01	3.82E+01	1.246.401	1.85E+01	9,0	C	2) C	y C	4 075400	1.07 F		y (ر ع	٢	Č	1 a	1.07E+00
1,2,4-TMB	9.19F+01	1 03E+00	4 435+00	A DRITAD4	4 87E-02	1.07.1.02	4.275401	4.99E+01	BLO	BIO	0	, E	5 6	4 085400	4 OAE OA	- C	ָץ כ מ	פוני	BLO	0 78		1.03E+00
1,3,6-TMB	9.40E+01	1.06E+00	2 30F+00	3.68E±01	8 88F±01	2.32E404	2.00C+01	Z.61E+U1	9 60	BLO	80	1018		1 OFF+00	1 04E-04	, C	, c	בנ	g B	ВГО	018	1.06E+00
O-XYLENE	9.22E+01	1.03E+00	1.61E+00	3.68F+01	1 00F+02	2 ORE 404	10.11.00.1	1.045401	BLO	BLQ	ВГО	BLO	0	1 05F+00	9 935-02		, c	ָבָּרָ בַּרָ	BLO	BLQ	ВГО	1.03E+00
m-XYLENE	9.22E+01	1.03E+00	3.67E+00	9.93E+01	2.94E+02	8 23E+01	6 27E404	3.27 5.401	<u>0</u>	BLQ	BLQ	BLO	- 4.08E-03	1.05E+00	9.86F-02	810	5 43E-03	201.0	BLO	ВГО	BLO	1.03E+00
P-XYLENE	9.39E+01	1.03E+00	1.22E+00	3.44E+01	1.05E+02	2.23E+01	1 005+01	10.16.1	BLO	BLQ	ВГО	BLQ	BLO	1.06E+00	9.63E-02	BLO	ē	y (BLO	ВГО	BLQ	1.03E+00
£8	9.24E+01	1.03E+00	5.56E-01	1.75E+01	4.77E+01	4.83E+00	1 45F+01		BLG	a Q	BLQ	ВГО	BLQ	1.06E+00	9.74E-02	BLQ	BIO		BLQ	BLQ	BLQ	1.03E+00
TOLUENE	9.29E+01	1.06E+00	1.42E-01	1.26E+01	2.73E+00	2.35E-01	2 86F-02	; ; ;	7	BLQ	BLO	BLQ	BLQ	1.06E+00	1.04E-01	BLQ	ВГО		מנס	a O	BLQ	1.06E+00
BENZENE	9.78E+01	1.05E+00	BLQ	4.01E-01	4.55E+00	5.17E-01	3.26E-02		ָ מרכי	BLQ	BLQ	BLQ	2	9.73E-01	1.04E-01	BLQ	BLO	Ē	ָ פרק	2	2	1.05E+00
SAMPLE	100 µg/ml QC	1 µg/ml	821-1	821-2	821-3	821-4	821-5	9 70	9-179	821-7	871-8	821-9	821-10	1 µg/ml	0.1 µg/ml	821-11	821-12	67:43	C1-170	821-14	Method Blank	1րց/ու

Analyst: David A. Kovacs

BLQ < 0.01 µg/ml

Page 1 of 1 Printed: 10/21/93

Ref: 93-RC16/vg

October 20, 1993

Dr. John Wilson

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

Post Office Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift SW

Dear John:

Attached is a report of the data generated from the analyses of 14 sample core extracts from Hill AFB, UT. The extracts, which were submitted under Service Request #SF-0-26, were analyzed for total fuel content as JP-4 jet fuel only. The reported values for fuel carbon were computed from the JP-4 determinations. I have also attached a report of the quality control analyses that were performed concurrently with the sample analyses.

Data quantification, peak identification, component concentration calculations, and dilution factor corrections were performed by MAXIMA chromatography software. JP-4 data was quantified with a 7-point external standard calibration curve ranging from 50 - 50,000 ng/µl.

The Minimum Detectable Limit (MDL) for JP-4 is determined by the concentration of the lowest calibration standard, which is 50 ng/ μ l. Since the MDL is determined by a calibration standard, it may also be defined as the Minimum Quantifiable Limit (MQL). It is important to note that values less than the MQL are reported in this data set, but cannot be considered quantified since they lie outside the range of the standard curve. All such unquantified data are approximations extrapolated from the JP-4 standard curve.

The samples from Service Request #SF-0-26 had an average mass of 15.23 g, and were extracted with 5.0 ml of methylene chloride. For simplicity's sake, I have assumed complete extraction of the sample's contents into the 5.0 ml of solvent.

In order to compute the MQL of JP-4 in the average sample core, assume the following:

Sample mass = 15.23 g
Extract volume = 5.0 ml
Extraction efficiency = 100%
Determined mass of JP-4 = 50 ng
(in 1.0 µl of extract)

MariTech Environmental Technology, Inc.

1.
$$\left(\frac{50 \text{ pg}}{1.0 \text{ µI}}\right) \left(\frac{1000 \text{ µI}}{2000 \text{ pg}}\right) \left(\frac{1 \text{ µg}}{1000 \text{ pg}}\right) = 250 \text{ µg}$$

Consider that 22.28 g of sample was extracted with the 5.0 ml aliquot of methylene chloride and the original concentration is computed by division of the extracted mass of JP-4 by the sample mass:

2.
$$\frac{250 \ \mu g}{15.23 \ g} = 16.41 \ \mu g/g$$

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Therefore, 16.41 μ g/g (or mg/kg, or ppm if you prefer either of these units) is the Minimum Quantifiable Limit (MQL) of JP-4 determined in these samples.

It should be realized that JP-4 determinations are based on the summation of multiple peak areas detected over a defined period of time rather than the area of a specific peak, which is typical of individual fuel component determinations. When using this method of determination, it is entirely possible for a single peak or a group of peaks not attributable to JP-4 to register enough area to be mistakenly represented as JP-4.

Sample extracts were received from Mark Blankenship on October 15, 1993. Analyses were started on October 18, 1993, and concluded on October 19, 1993. Sample extracts and quality control samples were analyzed according to RSKSOP-72, Rev. No. 1, excepting the modifications listed in the attached outline.

If you have any questions concerning this report, please contact me at your convenience.

Singerely,

Kandy Caylaway

xc: R.L. Cosby J.L. Seeley SR#SF-0-26 / Wilson / Hiy \ \text{VFB} all conc. are ug/g (

	•		•	
Sample I.D.	Dilution Factor	JP~4	Fuel Carbon (JP-4 x 0.85)	13 2 19
				N9 ×
				(y x 102)
82 II	1	398.00	338.00	(34)
82 I2	1	5870.00	4990.00	2
82 I3	10	14800.00	12600.00	
82 I4	1	3770.00	3200.00	
82 I5	1	4330.00	3680.00	
82 I6	1	30.40	25.80	
82 I7	1	2.35	2.00	
82 18	1	0.73	0.62	
82 I9	1	0.84	0.72	
82 I10	1	0.86	0.73	
82 I11	1	0.83	0.71	
82 I12	1	0.88	0.75	
82 I13	1	1.24	1.05	
82 I14	1	0.98	0.83	

all reported values are corrected for dilution factors where applicable

all conc. are ng/ul SR#SF-0-26 / Wilson / QC 1 •

Sample I.D. Date

180CT93 1.70 blk MeCl2 Method blank 2.21 ° 0.00 500 jp4 5000 jp4 50000 jp4 4 3.00 47400.00

blk MeCl2 210CT93 2.96 1000 jp4 10000 jp4 976.00 9130.00

blk MeCl2 - methylene chloride solvent blank jp4 - JP-4 fuel standard (ng/ul)

HP5890 GC / OPERATING CONDITIONS A. Instr. ant Control I.

Analyses: "SH-2-JP4" 1.

Program: "RWC-AS10" 2.

Calibration: "DK-5-BTEX"

B. Temperature Program

> 1. Initial Temp & Time: 10°C for 3.00 min

Level 1: Rate = 4°C/min to 70°C, Final Time = 0.00 2.

Level 2: Rate = 10°C/min to 270°C, Final Time = 3. 2.00

Run Time: 40.00 min

Oven Equilibration Time: 1.00 min 5.

c. Miscellaneous

> 1. Peak Width: 0.02

Attentuation: 2⁵ 2.

3. Chart Speed: 0.50

Threshold = 0

5. Offset = 10%

MAXIMA PEAK ITEGRATION II.

Peak Detection Parameters

Baseline Points: 18

Filter Window (in points): 13 2.

Intg. Sensitivity (coarse): $5.00 \mu V/sec$

Intg. Sensitivity (fine): $5.00 \mu V/sec$

Peak Rejection Criteria В.

Minimum Area: 2000 μV-sec

2. Minimum Height: 300.0 μ V

Minimum Width: 3.00 sec 3.

c. Integration Events

0.00: Disable Peak Skimming
0.00: Disable Peak Detection
5.00: Enable Peak Detection
19.96: Set Baseline 1.

2.

3.

4.

5. 21.74: Set Baseline

23.23: Set Baseline 6.

26.20: Set Baseline 7.

27.58: Set Baseline 8.

9. 28.66: Set Baseline

30.20: Set Baseline 10.

32.81: Set Baseline 11.

IV. MAXIMA DATA ACQUISITION

Preacquisition Delay: 5.00 min

B. Duration: 35.00 min

Rate: 3.00 points/sec C.

D. Run Time: 40.00 min

MAXIMA CALIBRATION CURVES v.

A. JP-4

> 1. Calibration Range = $50 - 50,000 \text{ ng/}\mu\text{l}$

2. Summation of all peaks detected from 5.00 - 40.00 minutes

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Hill AFB Field Data Number 2		
Sample	Depth (ft)	OVM
82 I-14 TO 82 I-8	13.8-16.28	2
82 I-7	16.28-16.64	13
82 I-6	16.64-17.00	81
8a I-5	17.0-17.36	257
82 I-4	17.36-1772	181
82 I-3	17.72-1808	137
82 I-2	1808-18.44	150
82 I-1	18.44-18.80	143
82 I-27	18.8-19.12	397
82 I-26	19.12-19.45	301
82 I-25	19.45-19.77	136
82 I-24	19.77-20.09	176
82 I-23	20.09-20.42	78
82 I-22	20.42-20.74	87
82 I-21 TO 82 I-19	20.74-21.71	92.33
82 I-18	21.71-22.03	298
82 I-17	22.03-22.35	357
82 I-16	22.35-22.68	293
82 I-15	22.68-23.00	270
82 I-39	23.0-23.2	255
82 I-38	23.2-23.4	145
82 I-37	23.4-23.76	330
82 I-36	23.76-24.12	239
82 I-35	24.12-24.48	74
82 1-34	24.48-24.89	68
82 I-33	24.89-25.20	311
82 I-32	25.20-25.56	236
82 I-31	25.56-25.92	249
82 I-30 TO 82 I-28	25.92-27.00	84

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Hill AFB Field Data Number 2		
Sample	Depth (ft)	JP-4 (mg/kg)
82 I-14 TO 82 I-8	13.8-16.28	1.2 to 0.73
82 I-7	16.28-16.64	2.4
82 I-6	16.64-17.00	30.4
8a I-5	17.0-17.36	5330 and 4330
82 I-4	17.36-17.72	3770
82 I-3	17.72-18.08	14800
82 I-2	18.08-18.44	5870
82 I-1	18.44-18.80	398
82 I-27	18.8-19.12	67.30
82 I-26	19.12-19.45	276.00
82 I-25	19.45-19.77	17.60
82 I-24	19.77-20.09	14.30
82 I-23	20.09-20.42	24.00
82 I-22	20.42-20.74	17.90
82 I-21 TO 82 I-19	20.74-21.71	12.96
82 I-18	21.71-22.03	720.00
82 I-17	22.03-22.35	1290.00
82 I-16	22.35-22.68	385.00
82 I-15	22.68-23.00	1190.00
82 I-39	23.0-23.2	485.00
82 I-38	23.2-23.4	8.06
82 I-37	23.4-23.76	1370.00
82 I-36	23.76-24.12	4.20
82 I-35	24.12-24.48	4.96
82 I-34	24.48-24.89	2.87
82 I-33	24.89-25.20	4.43
82 I-32	25.20-25.56	3830.00
82 I-31	25.56-25.92	834.00
82 I-30 TO 82 I-28	25.92-27.00	5.96

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(3)

Hill AFB Field Data Number 2		
Sample	Depth (ft)	TPH (mg/kg)
82 I-14 TO 82 I-8	13.8-16.28	<10
82 I-7	16.28-16.64	138
82 I-6	16.64-17.00	139
8a I-5	17.0-17.36	3530
82 I-4	17.36-17.72	11500
82 I-3	17.72-18.08	28300
82 I-2	18.08-18.44	5160
82 I-1	18.44-18.80	6080
82 I-27	18.8-19.12	<10
82 I-26	19.12-19.45	<10
82 I-25	19.45-19.77	<10
82 I-24	19.77-20.09	<10
82 I-23	20.09-20.42	<10
82 I-22	20.42-20.74	<10
82 I-21 TO 82 I-19	20.74-21.71	<10
82 I-18	21.71-22.03	276
82 I-17	22.03-22.35	856±80
82 I-16	22.35-22.68	<10
82 I-15	22.68-23.00	643
82 I-39	23.0-23.2	<10
82 I-38	23.2-23.4	<10
82 I-37	23.4-23.76	340
82 I-36	23.76-24.12	<10
82 I-35	24.12-24.48	<10
82 I-34	24.48-24.89	<10
82 I-33	24.89-25.20	<10
82 I-32	25.20-25.56	410±256
82 I-31	25.56-25.92	<10
82 I-30 TO 82 I-28	25.92-27.00	<10

(4)

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82 D-40

82 D-39

82 D-38

Hill AFB Field Data Number 2		
Sample	Depth (ft)	OVM
82 D-11	20.0-20.3	1
82 D-10	20.3-20.6	1
82 D-9	20.6-20.9	1
82 D-8	20.9-21.2	1
82 D-7	21.2-21.5	1
82 D-6	21.5-21.8	1
82 D-5	21.8-22.1	3
82 D-4	22.1-22.4	139
82 D-3	22.4-22.8	11
82 D-2	22.8-23.2	0
82 D-1	23.2-23.8	0
NS	23.8-24.0	
82 D-25	24.0-24.1	25
82 D-24	24.1-24.4	50
82 D-23	24.4-24.7	282
82 D-22	24.7-25.0	63
82 D-21	25.0-25.3	30
82 D-20	25.3-25.6	16
82 D-19	25.6-25.9	29
82 D-18	25.9-26.2	11
82 D-17	26.2-26.5	15
82 D-16	26.5-26.8	20
82 D-15	26.8-27.0	27
82 D-14	27.0-27.3	20
82 D-13	27.3-27.6	25
82 D-12	27.6-27.8	15
NS	27.8-28.0	
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28.0-28.2

28.2-28.5

28.5-28.8

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82 D-37	28.8-29.1
82 D-36	29.1-29.4
82 D-35	29.4-29.7
82 D-34	29.7-30.0
82 D-3 3	30.0-30.3
82 D-32	30.3-30.6
82 D-31	30.6-30.9
82 D-30	30.9-31.2
82 D-29	31.2-31.5
82 D-28	31.5-31.8
82 D-27	31.8-32.1
82 D-26	32.1-32.4

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Hill AFB Field Data Number 2		
Sample	Depth (ft)	JP-4 (mg/kg)
82 D-11	20.0-20.3	
82 D-10	20.3-20.6	
82 D-9	20.6-20.9	
82 D-8	20.9-21.2	
82 D-7	21.2-21.5	
82 D-6	21.5-21.8	0.76
82 D-5	21.8-22.1	0.81
82 D-4	22.1-22.4	79.60
82 D-3	22.4-22.8	1.93
82 D-2	22.8-23.2	
82 D-1	23.2-23.8	1.12
NS	23.8-24.0	
82 D-25	24.0-24.1	1.69
82 D-24	24.1-24.4	77.10
82 D-23	24.4-24.7	572.0
82 D-22	24.7-25.0	2.22
82 D-21	25.0-25.3	1.83
82 D-20	25.3-25.6	
82 D-19	25.6-25.9	2.72
82 D-18	25.9-26.2	1.92
82 D-17	26.2-26.5	0.56
82 D-16	26.5-26.8	2.67
82 D-15	26.8-27.0	2.41
82 D-14	27.0-27.3	3.25
82 D-13	27.3-27.6	3.38
82 D-12	27.6-27.8	3.09
NS	27.8-28.0	
82 D-40	28.0-28.2	6.12
82 D-39	28.2-28.5	4.12

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82 D-38	28.5-28.8	3.96
82 D-37	28.8-29.1	
82 D-36	29.1-29.4	
82 D-35	29.4-29.7	
82 D-34	29.7-30.0	
82 D-33	30.0-30.3	
82 D-32	30.3-30.6	
82 D-31	30.6-30.9	
82 D-30	30.9-31.2	
82 D-29	31.2-31.5	
82 D-28	31.5-31.8	
82 D-27	31.8-32.1	
82 D-26	32.1-32.4	

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Hill AFB Field Data Number 2		
Sample	Depth (ft)	TPH (ms/kg)
82 D-11	20.0-20.3	
82 D-10	20.3-20.6	
82 D-9	20.6-20.9	
82 D-8	20.9-21.2	
82 D-7	21.2-21.5	
82 D-6	21.5-21.8	
82 D-5	21.8-22.1	<10
82 D-4	22.1-22.4	<10
82 D-3	22.4-22.8	<10
82 D-2	22.8-23.2	<10
82 D-1	23.2-23.8	<10
NS	23.8-24.0	
82 D-25	24.0-24.1	
82 D-24	24.1-24.4	<10
82 D-23	24.4-24.7	<10
82 D-22	24.7-25.0	<10
82 D-21	25.0-25.3	
82 D-20	25.3-25.6	
82 D-19	25.6-25.9	
32 D-18	25.9-26.2	
82 D-17	26.2-26.5	<10
82 D-16	26.5-26.8	<10
82 D-15	26.8-27.0	<10
82 D-14	27.0-27.3	<10
82 D-13	27.3-27.6	
82 D-12	27.6-27.8	
NS	27.8-28.0	
82 D-40	28.0-28.2	
82 D-39	28.2-28.5	

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82 D-38	28.5-28.8	
82 D-37	28.8-29.1	
82 D-36	29.1-29.4	
82 D-35	29.4-29.7	
82 D-34	29.7-30.0	
82 D-33	30.0-30.3	
82 D-32	30.3-30.6	
82 D-31	30.6-30.9	
82 D-30	30.9-31.2	
82 D-29	31.2-31.5	
82 D-28	31.5-31.8	
82 D-27	31.8-32.1	
82 D-26	32.1-32.4	

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Hill	AFB Field Dat	a Number 2
Sample	Depth (ft)	OVM
82 C-1	14.0	
82 C-2	13.5	
82 C-3	18.1	
82 C-4	17.8	
82 C-5	17.5	
82 C-6	17.2	
82 C-7	16.9	
82 C-8	16.6	
82 C-9	16.3	
82 C-10	16.0	
82 C-11	15.7	
82 C-12	15.4	
82 C-13	22.9	
82 C-14	22.6	
82 C-15	skipped	
82 C-16	22.3	
82 C-17	22.1	
82 C-18	broke	
82 C-19	22.0	
82 C-20	21.7	
82 C-21	21.55	
82 C-22	21.4	
82 C-23	21.1	
82 C-24	20.8	
82 C-25	20.5	
82 C-26	20.2	

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Hill	AFB Field Dat	a Number 2
Sample	Depth (ft)	JP-4 (mg/kg)
82 C-1	14.0	
82 C-2	13.5	
82 C-3	18.1	
82 C-4	17.8	
82 C-5	17.5	
82 C-6	17.2	
82 C-7	16.9	
82 C-8	16.6	
82 C-9	16.3	
82 C-10	16.0	
82 C-11	15.7	
92 C-12	15.4	
82 C-13	22.9	
82 C-14	22.6	0.62
82 C-15	skipped	
82 C-16	22.3	1.01
82 C-17	22.1	
82 C-18	broke	
82 C-19	22.0	638.0
82 C-20	21.7	593.0
82 C-21	21.55	698.0
82 C-22	21.4	820.0
82 C-23	21.1	26.0
82 C-24	20.8	1.02
82 C-25	20.5	2.88
82 C-26	20.2	1.95

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Hill AFB Field Data Number 2				
Sample	Depth (ft)	TPH (mg/kg)		
82 C-1	14.0			
82 C-2	13.5			
82 C-3	18.1			
82 C-4	17.8			
82 C-5	17.5			
82 C-6	17.2			
82 C-7	16.9			
82 C-8	16.6			
82 C-9	16.3			
82 C-10	16.0			
82 C-11	15.7			
82 C-12	15.4			
82 C-13	22.9			
82 C-14	22.6	<10		
82 C-15	skipped			
82 C-16	22.3	<10		
82 C-17	22.1	<10		
82 C-18	broke			
82 C-19	22.0	444		
82 C-20	21.7	580±14		
82 C-21	21.55	173		
82 C-22	21.4	352		
82 C-23	21.1	<10		
82 C-24	20.8	<10		
82 C-25	20.5	<10		
82 C-26	20.2	<10		

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SF-0-5 DATA

ANALYZED 8/25/93			
SAMPLE	METHANE	CARBON DIOXIDE	CXYGEN
82A	0.001	373	1.358
82B	0.001	409	1.911/
82C	0.002	624	1.514
82D	NO	747	2.266
82E	ND	295	6.396 /
82F	0.019	453	2.110
82H	ND ND	424	7.072 🗸
82-MW-10	0.004	640	2.539
82-MW-11 REP1	0.117	726	1.585
82-MW-11 REP2	0.095	822	2.107

LOWER LIMITS OF QUANTITATION:

0.001 0.169 0.275

UNITS ARE mg/L.

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TO

Ref: 93~LP27/vg

November 16, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift SAV

Dear Don:

TOC results follow for nine samples submitted under Service Request #SF-0-27. The samples were received November 10 and stored at 6°C until November 15 when analyses were done using RSKSOP-102. Blanks, duplicates, and known AQC samples were analyzed along with your samples for quality control.

Sample	mg/L Toc
82 A	2.2
82 B	3.1
82 C	6.0
82 D	5.2
82 D Dup	5.3
82 B	1.9
82 F	1.9
82 H	1.6
MW-10	5.3
MW-11	4.0
MW-11 Dup	3.8
WP030	13.6
WP030 T.V.	14.0

Sincerely,

Kynda Pennington

Lynda Pennington

J.L. Seeley ju J. Wilson



Ref: 93-PR48/vg

November 16, 1993

Dr. Don Kampbell/Dr. John Wilson

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift SAV

Dear Don/John:

Attached are the results of 9 Hill AFB samples submitted to ManTech Environmental as part of Service Request #SF-0-27. The samples were received on November 10, 1993, and analyzed November 11, 12, and 15. The methods used for analysis were EPA methods 353.1 and 365.1 along with Water's capillary electrophoresis method N-601. Blanks, spikes, duplicates, and known AQC samples were analyzed along with the samples for quality assurance.

If you have any questions concerning these results, please feel free to contact me.

Sincerely,

Priscilla Rhynes

J.L. Seeley

Sample	mg/l NO'_+ NO'_(N)	mg/1 C1	mg/l 80°,	mg/l T-P
82 A	- 08	159	60.5	.06
82 B	.37	144	72.2	.06
82 C	.08	109	17.2	.95
82 D	.13	151	116	.12
82 E	5.61	76.4	65.8	.10
82 F	5.07	60.2	55.5	.06
82 F Dup	5.06	60.7	55.0	.06
82 H	2.01	104	55.7	.08
MW 10	17.4	33.9	53.1	.86
MW 10 Dup	17.1			
MW 11	.17	29.5	94.1	3.95
MW 11 Dup				3.96
AQCWP030	7.24	176	38.5	1.56
True Value	7.10	178	42.0	1.60
Spike Recove	ry 104 %	97*	98\$	106%

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SF-0-27 DATA

ANALYZED 11/1	0/93	
SAMPLE	METHANE	CARBON DIOXIDE
82A	0.001	530
82B	ND	462
82C	0.002	733
82D	NO	1122
82E	ND	452
82F	0.006	552
82H	ND	513
MW-10	0.001	590
MW-11	0.022	914

LOWER LIMITS OF QUANTITATION

0.001 0.17

UPPER LIMITS OF QUANTITATION

0.940 1519

UNITS ARE mg/L.



Ref: 93-BN27/vg

December 2, 1993

Dr. John Wilson

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

S.A. Vandegrift 500

Dear John:

Below find results for methane on the Hill AFB sample as per Service Request #SF-0-35. The sample was received on Normber 19, 1993 and analyzed on November 23, 1993. The sample was $p_{\rm sup}$ ared as described in the paper "Dissolved Oxygen and Methane in Water by a GC Headspace Equilibration Technique", by Kampbell et.al., in International Journal of Environmental Analytical Chemistry, volume 36, pp. 249-257. Analysis and calculation of methane was performed as per RSKSOP-147.

Sample

Methane Concentration

EPA 82-I

0.68 mg/L

If you have any questions, please feel free to see me.

Sincerely,

Beyon Newell Bryan Newell

xc: R.L. Cosby J.L. Seeley ROBERT S. KERR ENVIRONMENTAL RESEARCH LABORATORY UNITED STATES ENVIRONMENTAL PROTECTION AGENCY SUBSURFACE PROCESSES BRANCH P.O. BOX 1198 ADA, OKLAHOMA 74820

FAX NUMBER: 405/436-8703

FACSIMILE TRANSMITTAL SHEET

DATE: 2-28-94

NUMBER OF PAGES (Including cover sheet): 3

TO: Leigh Benson

No Soil Duter

PHONE: 303/831-8100

82-E

FAX: 303-831-8208

82-F 82-H

FROM: John Wilson

PHONE: 405-436-8532

These numbers are for

COMMENTS/MESSAGE: modeling sorption of BTEX Compounds to squifer solids at bill AFB. Resume that Istal Soil to organic Carbon

is appropriate number for modeling.

Cl: Todd Wideneyer - please.



Ref: 94-LP9/rc

February 22, 1994

Dr. John Wilson

R.S. Kerr Environmental Research Lab U.S. Environmental Protection Agency

Post Office Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift SAV

Dear John:

Attached are TOC results for a set of four soils submitted to ManTech Environmental February 14, 1994 under Service Request # SF-0-46. The method used for these determinations was RSKSOP-120. The soil sample labeled "82E-15" was subsampled in a glove box to maintain anaerobic conditions in the jar.

A Leco standard soil was analyzed along with your samples for quality control.

If you have any questions concerning this data, please feel free to ask me.

Sincerely,

Synda Penrington Lynda Pennington

xc: R.L. Cosby

So	il Filtrate	Bolids	Total Soil	Mean ± 1 sd
<u>Bample</u>	\$ O.C.	\$ 0.C	3 O.C.	Boil & TOC
82E-12-1	.007	.046	.053	
82E-12-2	.009	.056	.065	$.069 \pm .019$
82E-12-3	.007	.083	.090	-4
82E-14-1	.007	.074	.081	
82E-14-2	.006	.062	.068	$.070 \pm .011$
82E-14-3	.006	.054	.060	
82E-15-1	.014	.071	.085	
82E-15-2	.018	.074	.092	$.087 \pm .004$
82E-15-3	.012	.073	.085	
82E-17-1	.011	.101	.112	
82E-17-2	.011	.078	.089	$.094 \pm .017$
82E-17-3	.012	.068	.080	
LECO STD SOIL		1.022		
		1.034		
LECO STD SOIL T.V.	•	1.00 ± .0	04	

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Sample	Soil Filtrate	solids	Total Soil	Mean ± 1 sd Boil & TOC
82E-12-1	.007	.046	.053	
82E-12-2	.009	.056	.065	.069 ± .019
82E-12-3	.007	.083	.090	
82E-14-1	.007	.074	.081	
82E-14-2	.006	.062	.068	$.070 \pm .011$
82E-14-3	.006	.054	.060	
82E-15-1	.014	.071	.085	
82E-15-2	.018	.074	.092	.087 ± .004
82E-15-3	.012	.073	.085	
82E-17-1	.011	.101	.112	
82E-17-2	.011	.078	.089	.094 ± .017
82E-17-3	.012	.068	.080	
LECO STD SOIL		1.022 1.034		
LECO STD SOIL T	·.V.	1.00 ± .	04	

405 436 8703

Deplicates.

ROBERT S. KERR ENVIRONMENTAL RESEARCH LABORATORY UNITED STATES ENVIRONMENTAL PROTECTION AGENCY SUBSURFACE PROCESSES BRANCH R. P.O. BOX 1198 ADA, OKLAHOMA 74820

FAX NUMBER: 405/436-8703

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7		(new)	1 1 20 = 2003	$p = q \cdot q \cdot q \cdot q$		No to a figuration	
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DATE: 4-4-94

NUMBER OF PAGES (Including cover sheet): 38

TO: Todd Wiedemeier

PHONE: 303-831-8100

FAX: 303-831-8208

FROM: John Wilson

PHONE: 405-436-853 2

COMMENTS/MESSAGE:



93-BB18 Ref:

November 24, 1993

Wer. John Milson

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift Sed

Dear John:

As requested in Service Request # SF-0-35, headspace GC/MS analysis of 2 water samples for BTEXXXTMB compounds was completed. The samples were received on November 19,1993 and analyzed on November 23, 1993. RSKSOP-158 (Determination of Volatile Aromatic Compounds and Tert-Butylmethylether in Water by Automated Headspace Gas Chromatography/Mass Spectrometry (Saturn II Ion Trap Detector) was used for this analysis.

An internal standard calibration method was established for the 9 aromatic compounds. The standard curves were prepared using concentrations of 1.0 to 4000 ppb. The lower quantitation limits were 0.5 ppb.

The samples were analyzed undiluted and were prepared by adding 10 ml of sample to a headspace vial containing 2 g of sodium chloride (NaCl). 8 μ l of 125 μ g/ml fluorobenzene was added to this 10 ml liquid volume before the vial was capped.

A quantitation report for the samples and a QC standard is presented in Table 1.

If you should have any questions, please feel free to contact me.

Sincerely,

Bradley O. Blace

Bradley D. Black

xc: R.L. Cosby

G.B. Smith

D.D. Fine

J.L. Seeley

ManTach Environmental Technology, Inc.

Table 1. Quantitation Report for SR# SF-0-35.

Concentration = ppb

QC1123C 500 ppb	503	508	510	510	508	510	200	207	513
TRIP BLANK	 	!!!	 	1 1	1	1 1	! !	! !	! ! !
EPA 82-1	2740	372	486	784	1370	1140	162	495	240
Compound	Benzene	Toluene	Ethylbenzene	p-Xylene	m-Xylene	o-Xylene	1,3,5-Trimethylbenzene	1,2,4-Trimethylbenzene	1,2,3—Trimethylbenzene

= Below Quantitation Limit (0.5 ppb) QC = Quality Control Standard



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Hill AFB Monitoring Well Samples

			12-12-12-12-12-12-12-12-12-12-12-12-12-1
Location Date PH	D.O. Temp.	Depth to Fetz	•
	mall 6°	Depth to Fetz Water mg/l	
- 10163 T	•	<u>:</u>	
82 A 11/8/43 7.4	0.3 14.8	4.46 0.17	A company of the second
82 B 11/8/93 7.5	1.2 12.9	25.37 0.11	
82 C 11/9/93 6.3	0.4 14.2	22.17 0.84	· ·
82 C 11/9/93 6.3	0.4 14.2	:	
82.0 11/9/93 7.2	0.8 14.1	23,72 1.7	
\$2 E 11/8/93 7.4	2.7 16.5	6.26 0.02	
			reconstruction of the second
82F 11/8/93 7,6	1.716.8	7.30 0.04	
824 11/8/93 7.4	5.4 15.7	11.46 6.19	
	i		
MW-10 11/9/93 7.4	1.5 15.0	28.05 0.22	<u></u>
MW-11 11/9/93 7.4	0.1 14.7	25,74 0.05	
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Ref: 93-BN27/vg

December 2, 1993

or. John Wilson

R.S. Kerr Environmental Research Lab U.S. Environmental Protection Agency

P.O. Box 1198 Ada, OK 74820

THRU: S.A. Vandegrift 500

Dear John:

Below find results for methane on the Hill AFB sample as per Service Request #SF-0-35. The sample was received on November 19, 1993 and analyzed on November 23, 1993. The sample was prepared as described in the paper "Dissolved Oxygen and Methane in Water by a GC Headspace Equilibration Technique", by Kampbell et.al., in International Journal of Environmental Analytical Chemistry, volume 36, pp. 249-257. Analysis and calculation of methane was performed as per RSKSOP-147.

Bample

Methane Concentration

EPA 82-I

0.68 mg/L

If you have any questions, please feel free to see me.

Sincerely,

Byon Njuell Bryan Newell

xc: R.L. Cosby J.L. Seeley

MANATATION TECHNOLOGY

Ref: 93-BN23/vg

November 15, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

Post Office Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift SAV

Dear Don:

Find attached results for methane and carbon dioxide on Hill AFB samples as per Service Request \$5F-0-27. Samples were received and analyzed on November 10, 1993. Samples were prepared as described in the paper "Dissolved Oxygen and Methane in Water by a GC Headspace Equilibration Technique", by Kampbell et al., in International Journal of Environmental Analytical Chemistry, Volume 36, pp. 249-257. Analysis and calculations of carbon dioxide was performed as per RSKSOP-114, and analysis and calculations of methane was performed as per RSKSOP-147.

If you have any questions, please feel free to see me.

Sincerely,

Bryan Newell

Bupon Newel

xc: R.L. Cosby

J.L. Seeley

J.T. Wilson V

M.C. Cook

SF-0-27 DATA

ANALYZED 11/10/93	3	
SAMPLE	METHANE	CARBON DIOXIDE
82A	0.001	530
82B	ND	462
82C	0.002	733
82 D	ND	1122
82E	ND	452
82F	0.006	552
82H	ND	513
MW-10	0.001	590
MW-11	0.022	914
LOWER LIMITS OF QU	ANTITATION	
	√.001	0.17
UPPER LIMITS OF QUA	ANTITATION	

0.940

1519

UNITS ARE mg/L.

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Ref: 93-PR48/vg

November 16, 1993

Dr. Don Kampbell/Dr. John Wilson

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift SA

Dear Don/John:

Attached are the results of 9 Hill AFB samples submitted to ManTech Environmental as part of Service Request #SF-0-27. The samples were received on November 10, 1993, and analyzed November 11, 12, and 15. The methods used for analysis were EPA methods 353.1 and 365.1 along with Water's capillary electrophoresis method N-601. Blanks, spikes, duplicates, and known AQC samples were analyzed along with the samples for quality assurance.

If you have any questions concerning these results, please feel free to contact me.

sincerely,

Priscilla Rhydes

J.L. Seeley

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5 .	mg/1	mg/l cl	#g/I	<u>7-7</u>
Sample	MO', + MO',(N)		_804_	
82 A	.08	159	60.5	.06
82 B	.37	144	72.2	.06
82 C	.08	109	17.2	.95
82 D	.13	151	116	.12
82 E	5.61	76.4	65.8	.10
82 F	5.07	60.2	55.5	-06
82 F Dup	5.06	60.7	55.0	.06
82 H	2.01	104	55.7	.08
MW 10	17.4	33.9	53.1	.86
MW 10 Dup	17.1			
MW 11	.17	29.5	94.1	3.95
MW 11 Dup	••		7.55	3.96
AQCWP030	7.24	176	38.5	1.56
True Value	7.10	178	42.0	1.60
Spike Recover	· · · - :	971	984	106%

19



Ref: 93-LP27/vg

November 16, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

S.A. Vandegrift SAV

Dear Don:

TOC results follow for nine samples submitted under Service Request #SF-0-27. The samples were received November 10 and stored at 6°C until November 15 when analyses were done using RSRSOP-102. Blanks, duplicates, and known AQC samples were analyzed along with your samples for quality control.

Sample	mg/L TOC
82 A	2.2
82 B	3.1
82 C	6.0
82 D	5.2
82 D Dup	5.3
82 E	1.9
82 P	1.9
82 H	1.6
MW-10	5.3
MW-11	4.0
MW-11 Dup	3.8
WP030	13.6
WP030 T.V.	14.0
	Sincerely.

Lynda Pennington Lynda Pennington

xc: R.L. Cosby J.L. Seeley J. Wilson

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MANIGATICALITY TECH (I) (I) &

Ref: 93-LS24

November 17, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74821-1198

THRU: S.A. Vandegrift SAV

Dear Don:

Please find attached results for the Hill AFB analyses of aqueous samples to be analyzed by purge-and-trap/GC:FID-PID for Benzene, Toluene, Ethylbenzene, p-, m-, & o-Xylene, 1,3,5-, 1,2,4-, & 1,2,3-Trimethylbenzene and Total Fuel Carbon. We received a total of 9 samples, in duplicate, on November 10, 1993. The samples received were in capped, 40 mL VOA autosampler vials preserved with lead-lined septa and 0.4 g Na,PO,. All samples were stored at 4°C until analyzed. Samples were analyzed on November 16, 1993. All samples were acquired and processed using the MAXIMA data system. A 5 place external standard curve (1-10-100-500-1000 ppb) was used to quantitate the samples.

This work was performed under Service Request #SF-0-27. RSKSOP-133, "Simultaneous Analysis of Aromatics and Total Fuel Carbon by Dual Column-Dual Detector for Ground Water Samples" was used for these analyses.

Sincerely,

Lisa R. Secrest

xc: R.L. Cosby J. Wilson J.L. Seeley A

ĺ,

BAMPLENAME	BENZENE	BENZENE TOLLIENE	ETHYL BENZENE	PXYLENE	M-XYLENE	O-XYLENE	1,8,6-TMB	1,2,4.748	1.2.3-TMB	FUEL CARBON
100 PB	1.01E-00	1 DIE-02	4015.00	. D. E. S	200	1				
000 000 000 000						1.00c+d2	1.01E+02	1 OF EACH	1 BOE+03	W/W
BL TOWERS TO	4.25E	4.80E+01	4.95E+01	5.01E+01	4.94E+01	100007	A 775.A.	446.04		
OC. TRUE VALUE, PPB	6 MF-101	AMPLA	E COE. O.	F ONE. AL						<≥
A-04					D+1100.0		5.00E+0	6.00E+0	6.00E+01	W
	2	3	2	2	2	2	1.145.00	D ASE AS	ã	Ī
\$2.0	2	2	Ç	2	9	3			3	2
62-8 Dunksets	2	Ş	S	2	2 5	3 9	2	3	2	ş
3.5				2	2	5	2	2	2	Ş
7	2	F.38E+00	6.61E+00	2,02E±01	6.36F+00	1.82E+00	7.97E-01	A ADELM	AAIEAA	W-96-
0.23	7£48	4.ME+00	3.08E+01	1.415-00	9 BAE	A 255.01				1.135.65
8 2.6	2	Ş	2					1.185+02	7.7.540	1.50E+03
19.6	2	2 5	2 !	2	2	2	2	2	9	Ş
	2	2	2	2	2	2	9	S	ş	! 9
H-52	웆	2	9	Ş	S	9		2 %	2 ;	€ ;
MW-10	7.445.00	A 20FLO	SVE VO	60 U		2	W. 425-01	3	3	ဒ္ဓ
1460.11			1.000 F		1.000	0.00E+02	1.74E+CS	2.87E+62	2.12E+02	4.52E+03
			201020		2.21E+02	8,64E+01	S.OOE.O!	A K7E AN	S STEAM	90.514.0
	2	2	2	ş	9	5	9			ACOUNTY.
600 PPB	4716.00	4 TOFILES	4 475.00	A 575		2	5	Ę	2	< <u>*</u>
OC ORCEDVED BOD	10 T		10 C C C C C C C C C C C C C C C C C C C	4.0/6104	4.00E+02	4.745.+02	4.73E+02	4.76E+B	4.81E+02	YN
			4.90m+0	6.00E+01	4.90E+03	5.02E+01	4.65E.04	R CRE.Ast	A ONE.A	
CC, INCENALUE, PPB	6.00E+01	5.00E+01	5.00E+01	5.00E+01	8.00F.01	A ANELOS	200			S
949	1.00E-01	LOOFLA	1000	S POL					9.8E+6-	\ 2
				20430A	W. B. IE + 0.0	8-50E+00	9.55E+00	€.71E+00	9.86E+00	X

ND = None Detected; N/A = Not Analyzed; BLQ = Below Limit of Quantitation, 1 ppb



Ref: 93-DK11/vg

November 8, 1993

Dr. John Wilson

R.G. Kerr Environmental Research Lab U.S. Environmental Protection Agency

P.O. Box 1198 Ada, OK 74820

THRU: S.A. Vandegrift 5ft

Dear John:

I have determined average molecular weight for your sample extracts MW10A and MW10B from Hill AFB. The "Number-Average Molecular Weight" method was calculated. Please see the attached reference material for details. My results are as follows:

MW10A = 156

MW10B = 160

This work was performed under Service Request #SF-0-32.

In summary, methylene chloride extracts of the soil cores were analyzed by GC/MSD on October 31 and November 1, 1993. The samples were taken from crimp capped autosampler vials previously analyzed by GC/MS, August 13-17, 1993, by D. Fine under Service Request $\{SF-0-1\}$ (Ref: 93-DF5). My TIC chromatograms of the two samples are attached. Calibration curves created from the analysis of 117 different petroleum compounds including n-paraffins, isoparaffins, aromatics, olefins, naphthenes, (referred to by the acronym PIANO) and PNAs were used to determine the concentration of every detected peak in the extract in terms of $\mu g/ml$ and $\mu M/ml$. This was done by relating retention time to "response factor". Graphs of these calibration curves are attached. The number-average molecular weight is the sum of the weights of each molecular species divided by the sum over all molecular species of the number of moles of each species.

If you require further information, please feel free to contact me.

Sincerely,

David A. Kovaca

G. Smith
J.L. Seeley

Marifech Environmental Technology, Inc.



Ref: 93-DK4/vg

September 1, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift 5 PN

Dear Don:

Please find attached results of GC/MSD analysis of Hill AFB core extracts for quantitation of Benzene, Toluene, Ethylbenzene (EB), p-Xylene, m-Xylene, o-Xylene, 1,3,5-Trimethylbenzene (1,3,5-TMB), 1,2,4-Trimethylbenzene (1,2,4-TMB) and 1,2,3-Trimethylbenzene (1,2,3-TMB) as requested under Service Request #SF-0-5.

The analytical method was a modification of RSKSOP-124. Cool (38°C) on-column injection (0.5 μ l) was used with electronic pressure control (EPC) set for a constant flow of 0.9 ml/min. A 30M X 0.25 mm Restek Stabilwax (Crossbonded Carbowax-PEG, 0.5 μ m film) capillary GC column with 1 foot long X 0.53 mm ID uncoated capillary precolumn was used. Quantification was based on two standard curves: A low level curve was used for extract concentrations in the range 0.01-1.0 μ g/ml (0.01,0.1,1.0 μ g/ml). The second curve was used for quantification of concentrations >1.0 (1,10,100,333 μ g/ml).

If you require further information, please feel free to contact me.

Sincerely,

David A. Royace

xc: R.L. Cosby
G. Smith

J.L. Seeley

Units = mg...

HIII AFB Core Extracts . MSD Analyses

SR#SF-L- Ur.Kampbell

Page 1 of 6 Printed:9/1/93

BLQ < 0.01 µg/m)

Analyst: David A. Kovacs

SAMPLENAME	DENZENE	TOPOCINE			111416	X-VIETUR	1.0.0.1mg	1,6,9-1,00	1.642-170
fw/6r	9.06E-01	1,00E+00	1.07E+00	1.05E+00	1.06E+00	1.09E+00	1.10€+00	1,09E+00	1.07E+00
ZA-1	2	2	2	S	2	Q	S	2	2
2A-2	2	2	2	2	2	Q.	2	2	2
2A-3	2	9	9	2	2	2	2	2	2
2A-4	2	2	Q	2	2	2	2	2	2
2A-5	2	Ş	Q.	2	2	2	Q	2	2
12A-6	2	2	Q	2	2	9	Q	9	2
12A-7	2	Ş	2	2	2	9	2	Ş	2
12A-8	2	Ş	2	2	2	2	2	2	2
32A-9	2	9	2	9	2	9	2	2	2
2A-10	2	ş	9	2	2	ş	9	9	9
lm/sa(1.06E+01	1.04E+01	1.04E+01	1.03E+01	1.05E+01	1.05E+01	1.05E+01	1.05E+01	1.05E+01
1 m/ml	1.07E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00	1.02E+00
12A-11	2	9	9	Q	2	9	2	2	Ş
2A-12	2	9	2	Ş	2	2	S	Ş	Ş
2A-13	2	2	2	2	2	2	2	2	2
2A-14	2	2	2	2	2	2	2	2	Ş
2A-16	2	2	2	2	Ş	2	2	8	Ş
2A-16	2	Q	2	2	2	2	8	2	2
2A-17	2	2	2	2	2	2	Q.	2	2
2A-18	2	Q	9	2	2	2	2	2	Ş
2A-19	2	2	2	2	2	2	2	2	Ş
2A-20	2	2	2	2	2	2	2	2	2
pm/8rt o	1.05E+02	1.06E+02	1.07E+02	1.06E+02	1.06E+02	1.06E+02	1.06E+02	1.07E+02	1.07E+02
ig/ml QC	9.72E+01	9 .35E+01	9.28E+01	9.29E+01	9.19E+01	8.19E+01	9.18E+01	9.23E+01	9.20E+01
2A-21	2	9	9	2	2	2	2	2	2
2A-22	2	2	2	2	Q	2	2	2	Ş
12A-23	2	2	2	Š	Ş	Q	S	2	2
12A-24	2	2	2	2	2	9	Q	2	2
12A-26	9	2	오	2	2	2	2	2	2
12A-26	2	2	8	Ş	2	2	2	2	Ş
2A-27	9	2	2	Ş	2	2	2	2	Ş
2A-28	2	2	2	2	2	2	2	2	Ş
2A-29	2	2	9	Q	2	2	2	2	2

Units-mon.

HIIAFB Core Extracts ASD Analyses

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SR#SF-0-6 ... Kampbell

Page 2 of 6 Printed:9/1/93

BLQ < 0.01 µg/mf

Analyst: David A. Kovacs

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																							•											
1.2.3-TMB	Ş	9	1.03E-01	1.22E-02	8,23E-01	2	2	2	2	2	2	2	2	2	2	1.06E+02	9,44E+00	2	2	2	2	9	2	2	2	Q	2	1.04E+00	1.13E-01	2	2	Q	2	Q
1.2.4-TMB	2	950	1,016-01	1.05E-02	9.17E-01	2	2	呈	2	2	2	2	2	2	2	1.06E+02	9.41E+00	2	2	2	2	2	2	2	2	2	2	1,04E+00	1.12E-01	2	2	Ş	9	Q
1.3.6-TMB	2	BLQ	1.01E-01	1.28E-02	9.33E-01	2	Ş	ş	2	2	2	2	2	2	2	1.06E+02	9.36E+00	2	2	2	2	2	Ş	2	2	Ş	2	1.05E+00	1.12E-01	ş	2	Ş	9	2
O-XYLENE	N	B 10	1.02E-01	1.09E-02	9.35E-01	2	2	2	2	2	2	2	Q	2	2	1.06E+02	9.42E+00	2	2	2	2	2	2	9	Ş	2	2	1.04E+00	1.10E-01	Ş	2	Ş	2	2
M-XYLENE	Ä	BLQ	9.81E-02	1.01E-02	9.13E-01	2	2	2	2	2	Ş	2	2	Ş	2	1.06E+02	9.39E+00	2	2	2	2	2	2	2	Ş	2	2	1.06E+00	1.11E-01	2	2	2	2	Ω
D-XYLENE	S	2	9.94E-02	1.02E-02	9.10E-01	2	2	9	9	9	CN	2	2	2	2	1.06E+02	9.195+00	2	2	2	2	2	2	2	2	2	9	1.06E+00	1.11E-01	2	Ş	2	2	Q
	9	BLQ	1.01E-01	1.04E-02	9.20E-01	2	2	2	9	2	2	2	2	2	2	1.06E+02	9.51E+00	2	2	2	9	2	Q	2	Ş	2	2	1.05E+00	1.10E-01	2	Š	Q.	2	Q
TOLUENE	Ş	BLQ	9.95E-02	9.74E-03	9.30E-01	2	夂	2	2	2	9	2	2	2	2	1.06E+02	9.35E+00	旲	2	ջ	2	2	Q	2	2	2	Ş	1.04E+00	1.116-01	2	Š	2	2	Q
BENZENE	9	BLQ	1,08E-01	1.11E-02	9.62E-01	2	2	9	9	9	2	ą	2	2	2	1.04E+02	9.56E+00	皇	2	2	2	9	2	2	2	2	2	1.04E+00	1.18E-01	2	2	2	2	S
SAMPLENAME	82A-30	MeC12	0.1 µg/ml	0.01 µg/ml	1րց/ա	82A-31	82A-32	82A-33	82A-34	82A-35	82A-36	82A-37	82A-38	82A-39	82A-40	100 µg/m]	10 µg/ml QC	82A-41	82A-42	82A-43	82A-44	82A-45	82A-46	82A-47	82A-48	82A-49	82A-60	1 µg/m}	0.1 µg/ml	82A-61	82A-62	82A-53	82A-54	82A-55

SR#SF-0-0 Dr. Kampbell	. Kampbell		HINAF	HIII AFB Core Extracts LUMSD Analyses	CC/MSD Analy	****		Caits	Units = mgg	
ļ		•								APF
SAMPLENAME	BENZENE	TOLUENE		P-XYLENE	M-XYLENE	P-XYLENE	1.3.6-TMB	124TMB	1.2.3-TMB	₹-04
_82B-1	2	Q	Q	Ş	2	9	2	9	2	-19
82B-2	Q	2	2	Ş	2	2	Ş	2	2	94
828-3	2	, 2	Q	2	2	2	9	2	2	1
828-4	2	9	2	2	2	2	2	2	Ş	15:
828-6-	2	2	2	2	2	2	2	2	2	28
0.01 µg/ml	1.31E-02	1.10E-02	1.13E-02	1.14E-02	1.13E-02	1.08E-02	1.36E-02	1.11E-02	1.26E-02	
0.1 rolmi	0.94E-02	9.36E-02	9.41E-02	9.38E-02	9.38E-02	9.45E-02	9.29E-02	9.34E-02	9.22E-02	
1 µg/ml	9.68E-01	9.60E-01	9.47E-01	9.36E-01	9.38E-01	9.69E-01	9.46E-01	9.56E-01	9.63E-01	
10 mg/m100	9.25E+00	9.52E+00	1.00E+01	9.36E+00	9.51E+00	9.76E+00	9.30E+00	9.34E+00	9.62E+00	ı
1 µ9/m1	9.17E-01	9.92E-01	1.02E+00	1.02E+00	1.02E+00	1.03E+00	1.03E+60	1.04E+00	1.04E+00	JSE
82B-6	9	2	Q		2	2	2	2	2	PF
628-7	2	2	2	2	2	2	2	2	2	R
62B-6	2	QN	9	Ŗ	2	2	2	2	2	SKE
62B-9	2	ð	9	2	2	2	9	2	2	ERL
62B-10	8	2	2	2	S	2	2	2	2	. - A
62B-11	2	2	2	2	2	2	9	2	2	DA
62B-12	2	2	2	2	2	2	2	2	2	SS
62B-13	2	2	Q	2	2	2	9	2	2	5 B /
82B-14	2	2	Q	2	9	2	9	2	2	SP
82B-15	Š	Ş	9	Ş	SV SV	S	Ş	2	Ş	В
82B-16	2	오	2	2	2	2	2	2	2	
MeC12	BLQ	BLQ	BLQ	BLQ	BLQ	BLQ	BLQ	BLO	2	
0.1 µg/ml	1.02E-01	1.03E-01	1.04E-01	1.05E-01	1.05E-01	1.05E-01	1,04E-01	1.05E-01	1.04E-01	
1 µg/ml	9.37E-01	9.76E-01	9.64E-01	9.70E-01	9.69E-01	9.62E-01	9.43E-01	9.64E-01	9.56E-01	
62B-17	2	2	9	2	9	2	2	웆	2	
82B-18	2	2	2	Q	2	2	2	2	Q	
82B-19	2	2	ş	2	2	2	2	2	2	41
82B-20	2	9	2	Q	2	2	2	2	2	2 5
828-21	2	2	2	2	2	2	9	2	2	43
82B-22	2	2	2	2	2	2	2	2	2	6
82B-23	2	2	2	2	Q	2	2	2	2	876
828-24	2	2	2	Ş	2	2	Ş	Ş	Ş	33
628-25	2	2	2	2	2	2	2	2	2	
82C-14	Ş	9	2	2	2	2	2	2	2	P.:
										17
Analyst: Devid A. Kovacs	1A.Kovacs			BLQ<0.01 µg/m)	1 µg/m1		Page	Page 3 of 6 Printed:9/1/93	:9/1/83	
							•		U!	///
										0 /

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Units = mg.

HIII AFB Core Extracts & ASD Analyses

c.Kampbell

SR#SF-v-

SAMPLENAME

PR	? -0 4-	-19	94	1	5:	28				l	JSE	PA	R	SKE	RL	. - A	DA	SS	6B/	SP	В							46	3 5	43	6 8	376	33	ı	P. 18	
	12.3-TMB	4.91E-03	9.76E+00	1.04E+02	1.08E-01	6.63E-02	2.08E-01	9.05E-01	8.13E-03	3.63E-03	2.29E-02	1.45E-02	BĽO	3.11E-03	6.48E-02	BLQ	B CQ	1.16E-02	9.62E-02	9.63E-01	BLQ	9	BLQ	BLQ	6.18E-03	1.27E-02	2.13E-02	2	2	1.09E+02	9.95E+00	8.21E-03	8	BLQ	8.17E-01	
	124-TMB	1.67E-02	9.64E+00	1.04E+02	1.16E+00	1.03E+00	2.04E+00	4.42E+00	7.41E-02	1.68E-02	6.40E-02	3.71E-02	BLQ	8.85E-03	2.25E-01	BLQ	BLQ	1.02E-02	9.66E-02	9.91E-01	4.98E-03	2	4.16E-03	6.72E-03	6.95E-02	3.03E-02	3.99E-02	BLQ	BLQ	1.09E+02	9.86E+00	7.80E-02	3.10E-03	1.11E-02	3.11E+00	
	12.6-TMB	1.39E-02	9.41E+00	1.04E+02	1.65E+00	1,50E+00	2.34E+00	3.70E+00	6.01E-02	1.48E-02	3.88E-02	2.90E-02	4.16E-03	1.74E-02	1.95E-01	BLQ	BLQ	1.11E-02	9.85E-02	9.08E-01	BLQ	2	6.32E-03	8.71E-03	6.37E-02	4.33E-02	3.65E-02	1.47E-02	2.68E-02	1.09E+02	1.00E+01	8.82E-02	4.77E-03	3.04E-02	2.63E+00	
	O-XYLENE	2	9.77E+00	1.03E+02	1.51E-02	4.01E-03	BLQ	BLQ	BLQ	BLQ	1.36E-02	7.16E-03	BLQ	BLQ	4.61E-03	BLQ	BLQ	9.83E-03	9.86E-02	9.95E-01	BLQ	2	BŁQ	4.76E-03	BLQ	3.23E-02	4.50E-02	BLQ	BLQ	1.08E+02	1.00E+01	6.77E-03	BLQ	BLQ	7.32E-01	
À	M-XYLENE	2	9.53E+00	1.03E+02	2.57E-02	9.10E-03	9.56E-03	6.62E-02	9.91E-03	1,89E-02	6.21E-02	4.18E-02	BLQ	3.36E-03	3.46E-02	BLQ	BLQ	1.02E-02	9.86E-02	9.98E-01	BLQ	2	1.67E-02	2.75E-02	1.94E-02	1.21E-01	1.81E-01	BLQ	BLQ	1.08E+02	1.00E+01	6.29E-03	3.03E-03	B LQ	3.40E+00	
	P-XYLENE	2	9.34E+00_	1.05E+02	4.20E-02	2.96E-02	3.65E-02	8.57E-02	1.10E-02	1.05E-02	2.21E-02	1.78E-02	BLQ	BLQ	1.36E-02	BLQ	BLQ	1.02E-02	9.88E-02	1.00E+00	BLQ	2	4.54E-03	7.56E-03	6.62E-02	3.90E-02	6.51E-02	BLQ	B LQ	1.08E+02	9.98E+00	3.88E-02	BLQ	1.30E-02	1.62E+00	
		Ş	1.00E+01	1.03E+02	1.80E-02	6.18E-03	6.58E-03	2.86E-02	6.42E-03	7.95E-03	1.24E-02	1.18E-02	1.59E-02	3.35E-03	8.71E-03	BLO	BLQ	1.00E-02	9.87E-02	1.00E+00	2	2	1.15E-01	1,41E-01	1.24E-01	8.78E-02	6.13E-02	2.13E-02	3,44E-02	1.08E+02	9.96E+00	6.04E-02	9.49E-02	1.11E-01	1.48E+00	
	TOLUENE	9	9.62E+00	1.03E+02	B LQ	1.76E-02	1.92E-02	2.00E-02	BLQ	BLQ	9.69E-03	9.93E-02	1.01E+00	BLQ	BLQ	BLQ	BLQ	Bro	BLQ	3.04E-03	BLQ	Bro	1.08E+02	8.98E+00	BLQ	BLO	BLQ	BLQ								
	BENZENE	Q	9.52E+00	9.87E+01	6.21E-03	BLQ	3.67E-03	3.27E-03	BLQ	BLQ	BLQ	BLO	9.59E-03	2	BLQ	Bro	2	1.02E-02	9.87E-02	1.09E+00	BLQ	BLQ	2.03E-02	1.85E-02	2.09E-02	3.43E-02	3.16E-02	6.30E-03	7.92E-03	1.13€+02	1.10E+01	8.29E-03	1.04E-02	6.97E-02	2.71E-01	

82C-16 10µg/ml QC 100µg/ml QC 82C-20 82C-21 82C-22 82C-24 82C-25 82C-26 82C-3 82C-4 Mehod Blank 0.01µg/ml 1µg/ml 1µg/ml 1µg/ml 82C-15
Analyst: David A. Kovacs

82D-21 82D-22 82D-23

BLQ < 0.01 µg/m!

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Hill AFB Core Extracts . '15D Analyses

SR#SF-u- Jr. Kampbell

1.65E-01 7.49E-02 9.09E-02 9.50E-01 2.72E-01 BLQ	9/1/93	③
	Printed:9/1/93	*

Page 6 of 6

PR-Ø	4-19	3 94	} :	15:	30	1				US	:PF	i R	SK	ERL	F	1DA	S	5B/	'SF	В							4	Ø5	43	36	871	2 3		ρ.	19
1.2.3-TAB	1.35E-01	BLO	3.84E-02	BLQ	1.63E-02	2	1.00E+00	9.93E-02	QX	Ş	2	2	Ş	1.93E+01	BLQ	3,42E+02	2.03E+00	6.72E-01	2.34E+00	1.26E+00	9.23E+00	9.60E+01	1.01E+01	1.01E+00	7.78E-02	7.09E-02	7.83E-02	8.99E-02	1.65E-01	7.49E-02	9.09E-02	9.56E-01	2.72E-01	BLG	
1.2.4-TMB	4.40E-01	7.02E-03	1.07E-02	918	3.73E-02	2	9.89E-01	9.91E-02	9	9	Ş	9	2	6.09E+01	B10	3.43E+02	8.45E+00	2.33E+00	8.37E+00	4.72E+00	9.01E+00	9.50E+01	1.02E+01	1.02E+00	2.22E-01	1.916-01	2.06E-01	2.46E-01	4.02E-01	1.95E-01	2.4E-01	2.64E+00	7.24E-01	6.24E-03	
1.3.5-TMB	3.73E-01	7.44E-03	7.33E-02	7.70E-03	4.39E-02	2	1.02E+00	1.00E-01	NO ON	2	2	2	2	2.93E+01	BLQ	3.43E+02	2.94E+00	8.67E-01	3.04E+00	1.62E+00	8.89E+00	9.51E+01	1.03E+01	1.08E+00	8.43E-02	7.47E-02	7.96E-02	9.36E-02	1.67E-01	7.43E-02	1.03E-01	1.24E+00	3.84E-01	BLQ	
9-XYLENE	1.44E-01	3.59E-03	6.92E-02	4.86E-03	2.42E-02	9	9.93E-01	9.99E-02	2	2	2	2	2	1.99E+01	BLQ	3.44E+02	6.58E+00	1.72E+00	6.28E+00	2.31E+06	9.17E+00	9.40E+01	1.00E+01	1.01E+00	3.16E-01	3.03E-01	3.21E-01	3.18E-01	6.67E-01	3.10E-01	4.03E-01	2.04E+00	7.25E-01	BLQ	
M-XYLENE	6.65E-01	1.43E-02	1.01E-01	4.04E-03	1.11E-01	2	9.93E-01	1,01E-01	2	2	2	2	2	6.31E+01	BLQ	3,45E+02	1.05E+01	1.83E+00	4.89E+00	9.88E-01	9.02E+00	9.39E+01	9.99E+00	1.01E+00	6.17E-01	6.04E-01	6.12E-01	8.21E-01	1.16E+00	6.16E-01	8.02E-01	4.74E+00	1.84E+00	8.84E-03	
P-XYLENE	2.76E-01	6.75E-03	1.08E-02	BLQ	3.78E-02	2	9.85E-01	1.01E-01	Q	2	9	2	2	2.34E+01	BLQ	3.56E+02	4.81E+00	1,48E+00	4.69E+00	2.02E+00	8.67E+00	9.08€+01	1.02E+01	1,00E+00	2.43E-01	2.21E-01	2.33E-01	2.33E-01	4.27E-01	2.28E-01	2.81E-01	1.70E+00	6.25E-01	BLQ	
EB	2.64E-01	1.06E-02	1.28E-01	1.37E-01	1.716-01	2	9.94E-01	1.025-01	2	2	8	2	Q N	1.12E+01	BLQ	3.44E+02	3.72E+00	1.12E+00	3,39E+00	1.31E+00	9.46E+00	9.40E+01	9.76E+00	1.02E+00	1.60E-01	1.62E-01	1.59E-01	1.60E-01	2.83E-01	1.50E-01	1.87E-01	1.03E+00	3.77E-01	BLQ	
TOLUENE	BLQ	BLQ	8.09E-03	BLQ	BLQ	2	1.02E+00	1.03E-01	2	2	2	2	2	2.04E-01	BLQ	3,46E+02	1.07E+00	3.04E-01	6.91E-01	1.17E-01	9.16E+00	9.47E+01	9.81E+00	1.02E+00	4.65E-02	4.36E-02	3.50E-02	9.36E-02	2.00E-01	1.59E-01	2.31E-01	3.76E+00	1.73E+00	1.68E-02	
BENZENE	1.29E-01	1.03E-02	3.93E-02	3.88E-02	3.14E-02	2	1.35E+00	1.08E-01	21	9	2	9	Ş	1.61E+00	BLQ	J.49E+02	6.01E-01	3.33E-01	6.53E-01	6.29E-01	1.03E+01	1.00E+02	9.74E+00	9.89E-01	6.78E-01	6.38E-01	6.65E-01	7.71E-01	1.45E+00	7.87E-01	8.68E-01	7.49E-01	4.90E-01	BLQ	
SAMPLENAME	62D-24	820-25	820-38	82D-39	820-40	82E-2	1 µg/ml	0.1µg/ml	625-3	82E-13	82E-14	82E-16	82E-17	951-6	MoC12	333 µg/ml	821-16	821-16	821-17	821-18	10 µg/mlac	100 µg/ml	10 µg/ml	JE/B⊅L	821-19	821-20	621-21	621-22	821-23	821-24	821-25	821-26	821-27	821-28	

Analyst: David A. Kovacs

BLQ < 0.01 µg/ml

Units - nigita,

HIII AFB Core Extracts Can SD Analyses

SR#SF-0-5 Dr. Kampbell

12.3-TMB	1.01E+00	9.63E-02	ВГФ	BLQ	2.69E-01	3.09E+00	Ş	2	2	9.37E-03	1.60E+00	3.10E-02	8.23E-01	BLQ	BLQ	1.06E+01	1.04E+02
1.2.4-TMB	1.04E+00	9.11E-02	BLQ	BLQ	1.91E-02	7.62E+00	BLQ	2	BLQ	1.72E-02	6.38E+00	1.13E-01	3,30E+00	BLQ	BLQ	1.05E+01	1.04E+02
12.ETMB	1.08E+00	9.35E-02	BLQ	B LQ	4.18E-01	1.31E+01	BLQ	2	BLQ	1,21E-02	2.32E+00	3.10E-02	1.27E+00	BLQ	BLQ	1.04E+01	1.04E+02
O-XYLENE	1.03E+00	9.70E-02	BLQ	BLQ	BLQ	3.76E-02	오	Š	BLQ	8.50E-02	4.79E+00	1.29E-01	1.03E+00	ි ම	B LQ	1.06E+01	1.04E+02
M-XYLENE	1.01E+00	9.92E-02	BLQ	BLQ	1.28E-02	1.79E+00	2	2	S	8.98E-02	7.86E+00	6.92E-02	2.28E+00	BLQ	BLQ	1,06E+01	1.04E+02
DXXLENE	1.01E+00	9.95E-02	Bro	BLQ	2	1.05E+00	2	2	BLQ	3.64E-02	3.96E+00	1.54E-01	1.75E+00	BLQ	BLQ	1.04E+01	1.03E+02
	1.02E+00	9.81E-02	BLQ	ВГО	1.01E-01	1.24E+00	2.71E+01	1.61E+01	BLQ	2.38E-02	2,72E+00	1.21E-01	1.31E+00	BLQ BLQ	BLQ	1.08E+01	1.04E+02
TOLUENE	1.05E+00	1.03E-01	1,57E-02	1.11E-02	1.14E-02	3.20E-02	1.22E-02	7.30E-03	1.37E-02	1.64E-02	1.82E-01	1.88E-02	6.74E-02	810	BLQ	1.06E+01	1.04E+02
BENZENE	1,01E+00	1.05E-01	BLQ	BLQ	BLQ	1.36E-02	BLQ	BLO	8.31E-03	8.12E-02	7.12E-01	3.15E-01	4.22E-01	BLQ	9	1.06E+01	1.07E+02
SAMPLENAME	100/41	0.1 ua/ml	821-29	821-30	82 -31	821-32	821-33	821-34	821-36	621-36	621-37	821-38	821-39	MeCi2	MethodBlank	10 vg/m(QC	100 µg/ml

1,2,3-TMB	NO	QN	Q	Q	Ŋ	1.25E-02	9.22E-02	9.63E-01	9.52E+0	1.04E+00	QV Qv	Q.	S	QN	ND ON	S	S	2	2	2	9	Q	1.04E-01	9.56E-01	QN	Q	9	QN	QN	Q	QN	QX	QN	Q
1,2,4-TMB	QN.	Q.	Q	Q	Q.	1.11E-02	9.34E-02	9,56E-01	9.34E+00	1.04E+00	2	2	S S	2	QN	S	Q	2	Q	2	2	BLQ	1.05E-01	9.54E-01	2	QN	Q	9	Q	2	2	2	Q	QV
1,3.5-TMB	Q.	QN	S	Š	2	1.35E-02	9.29E-02	9.46E-01	9.30E+00	1.03E+00	2	Š	2	8	2	Š	Q.	오	QN	2	QN Q	BLQ	1.04E-01	9.43E-01	2	2	2	S	2	2	2	S	Ş	Q
O-XYLENE	QN	Q.	N Q	Š	2	1.08E-02	9.45E-02	9.59E-01	9.75E+00	1.03E+00	Q	2	S	2	Q	S	2	2	2	S	S	BLQ	1.05E-01	9.62E-01	2	Ş	2	2	2	Q	2	2	2	QN
m-XYLENE	QN	Ş	S	S	2	1.13E-02	9.38E-02	9.38E-01	9.51E+00	1.02E+00	2	Ş	2	2	2	2	Q	Q	Š	9	2	870	1.05E-01	9.69E-01	Q	9	2	Q	2	Q	QN Q	Q	2	QN
D-XYLENE	N	Q	2	S	Q	1.14E-02	9.38E-02	9.38E-01	9.36E+00	1.02E+00	2	2	S	2	ð	2	9	QN	9	2	2	BLQ	1.05E-01	9.70E-01	QN	Q.	Š	QN	S	Š	Š	2	S	QN
	Q	2	2	QX	2	1.13E-02	9.41E-02	9.47E-01	1.00E+01	1.02E+00	ð	2	2	2	욮	ND ND	2	Q.	운	Š	2	BLQ	1.04E-01	9.64E-01	Š	2	Ş	2	S	S	Š	2	2	QN
TOLUENE	Q.	S	2	Q.	2	1.10E-02	9.36E-02	9.60E-01	9.52E+00	9.92E-01	QN ^	2	2	S	9	<u>8</u>	Q.	2	Š	9	Š	BLQ	1.03E-01	9.76E-01	ND	Š	S	2	S	S	Q	2	2	Q
BENZENE	ON	S	2	2	2	1.31E-02	8.94E-02	9.58E-01	9,25E+00	9.17E-01	2	Š	Ş	2	2	ġ	2	오	Q	2	2	BLQ	1.02E-01	9.37E-01	2	2	2	2	Q	Q	2	2	Ş	Q
SAMPLENAME	82B-1	82B-2	82B-3	82B-4	82B-5	0.01 µg/ml	0.1 µg/ml	/ 1 µg/ml	10 µg/mlac	1 µg/mi	82B-6	82B-7	82B-8	82B-9	82B-10	82B-11	82B-12	82B-13	82B-14	82B-15	82B-16	MeC12	0.1 µg/ml	1 µg/ml	82B-17	82B-18	82B-19	82B-20	82B-21	82B-22	82B-23	82B-24	82B-25	82C-14

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Units = 1, _ .g

HIII AFB Core Extrac

SR#Sr 7.5 Dr. Kampbell

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Page 3 of 6 Printed: 9/1/93

BLQ < 0.01 µg/ml

Analyst: David A. Kovacs

SR#SF Cor. Kampbell

Units+11

BLQ < 0.01 µg/m1

Analyst: David A. Kovacs

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1,2,3-TMB	4.91E-03	9.76E+00	1.04E+02	1.08E-01	5.53E-02	2.08E-01	9.05E-01	8.13E-03	3.63E-03	2.29E-02	1.45E-02	BLQ	3.11E-03	5.48E-02	BLQ	BLQ	1.15E-02	9.52E-02	9.83E-01	BLQ	Q	BLQ	BLQ	5.18E-03	1.27E-02	2.13E-02	2	Q	1.09E+02	9.95E+00	8.21E-03	Q	BLQ	8.17E-01	
1,2,4-TMB	1.67E-02	9.54E+00	1.04E+02	1.16E+00	1.03E+00	2.04E+00	4.42E+00	7.41E-02	1.68E-02	5.40E-02	3.71E-02	B L0	8.85E-03	2.25E-01	BLQ	ВГД	1.02E-02	9.66E-02	9.91E-01	4.98E-03	ON.	4.16E-03	5.72E-03	6.95E-02	3.03E-02	3.99E-02	BLQ	BLQ	1.09E+02	9.86E+00	7.80E-02	3.10E-03	1.11E-02	3.11E+00	
1,3,5-TMB	1.39E-02	9.41E+00	1.04E+02	1.65E+00	1.50E+00	2.34E+00	3.70E+00	8.01E-02	1.48E-02	3.88E-02	2.90E-02	4.16E-03	1.74E-02	1.95E-01	BLQ	BLQ	1.11E-02	9.85E-02	9.88E-01	BLQ	Q	6.32E-03	8.71E-03	6.37E-02	4.33E-02	3.65E-02	1.47E-02	2.58E-02	1.09E+02	1.00E+01	8.82E-02	4.77E-03	3.04E-02	2.53E+00	
O-XYLENE	ON S	9.77E+00	1.03E+02	1.51E-02	4.01E-03	ВГО	BLQ	BLQ	BLQ	1.36E-02	7.16E-03	BLQ	BLQ	4.51E-03	BLQ	BLQ	9.83E-03	9.86E-02	9.95E-01	BLQ	S	BLQ	4.76E-03	ВГД	3.23E-02	4.50E-02	ВГО	BLQ	1.08E+02	1.00E+01	5.77E-03	BLQ	BLQ	7.32E-01	
M-XYLENE	QN	9.53E+00	1.03E+02	2.57E-02	9.10E-03	9.56E-03	6.62E-02	9.91E-03	1.89E-02	5.21E-02	4.18E-02	BLQ	3.36E-03	3.45E-02	BLQ	BLQ	1.02E-02	9.86E-02	9.98E-01	BLQ	Q	1.67E-02	2.75E-02	1.94E-02	1.21E-01	1.81E-01	вга	BLQ	1.08E+02	1.00E+01	5.29E-03	3.03E-03	BLQ	3.40E+00	
P-XYLENE	QN	9.34E+00	1.05E+02	4.20E-02	2.96E-02	3.65E-02	8.57E-02	1.10E-02	1,05E-02	2.21E-02	1.78E-02	BLQ	BLQ	1.36E-02	BLQ	ВГО	1.02E-02	9.88E-02	1.00E+00	BLQ	Q	4.64E-03	7.55E-03	6.62E-02	3.90E-02	5.51E-02	BLQ	BLQ	1.08E+02	9.98E+00	3.88E-02	BLQ	1,30E-02	1.62E+00	
EB	QN .	1.00E+01	1.03E+02	1.80E-02	6.18E-03	5.58E-03	2.86E-02	6.42E-03	7.95E-03	1,24E-02	1.18E-02	1.59E-02	3,35E-03	8.71E-03	ВГО	ВГО	1.00E-02	9.87E-02	1.00E+00	QN QN	QN	1.15E-01	1.41E-01	1.24E-01	8.78E-02	6.13E-02	2.13E-02	3.44E-02	1.08E+02	9.96E+00	6.04E-02	9,49E-02	1.11E-01	1.48E+00	
TOLUENE	QN C	9.62E+00	1.03E+02	BLQ	1.76E-02	1.92E-02	2.00E-02	BLQ	BLQ	BLQ	BLQ	BLQ	BLQ	BLQ	BLQ	BLQ	9.59E-03	9.93E-02	1.01E+00	BLQ	BLQ	ВГФ	BLQ	BLQ	BLQ	3.04E-03	BLQ	ВГФ	1.08E+02	9.98E+00	BLQ	BLQ	BLQ	BLQ	
BENZENE	ON C	9.52E+00	9.87E+01	6.21E-03	BLQ	3.67E-03	3.27E-03	ВГО	ВГО	BLQ	ВГО	9.59E-03	QN Q	BLQ	BLQ	2	1.02E-02	9.87E-02	1.09E+00	BLQ	BLQ	2.03E-02	1.85E-02	2.09E-02	3.43E-02	3.16E-02	6.30E-03	7.92E-03	1.13E+02	1.10E+01	8.29E-03	1.04E-02	6.97E-02	2.71E-01	
SAMPLENAME	82C-16	10 ng/ml ac	100 μց/ml	82C-19	82C-20	82C-21	82C-22	82C-23	82C-24	82C-25	82C-26	820-1	820-3	82D-4	MeC12	Method Blank	0.01 µg/ml	0.1 µg/ml	1 µg/ml	82D-5	820-6	82D-12	82D-13	82D-14·	82D-15	82D-16	820-17	82D-18	100 µg/ml	10 µg/ml	82D-19	82D-21	82D-22	82D-23	

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1,2,3-TMB	1.35E-01	BLQ	3.84E-02	BLQ	1.63E-02	QN	1.00E+00	9.93E-0	QQ	Q	Q.	NC	N Q	1.93E+01	BLQ	3.42E+02	2.03E+00	6.72E-01	2.34E+00	1.25E+00	9.23E+00	9.50E+01	1.01E+0*).	1.01E+00	7.78E-02	7.09E-02	7.83E-02	8.99E-02	1.55E-01	7.49E-02	9.09E-02	9.58E-01	2.72E-01	BLO	
1,2,4-TMB	4.40E-01	7.02E-03	1.07E-02	ВГО	3.73E-02	2	9.89E-01	9.91E-02	Q	2	2	Q	S	5.09E+01	ВГО	3.43E+02	8.45E+00	2.33E+00	8.37E+00	4.72E+00	9.01E+00	9.50E+01	1.02E+01	1.02E+00	2.22E-01	1.91E-01	2.06E-01	2.46E-01	4.02E-01	1.95E-01	2.44E-01	2,54E+00	7.246-01	6.24E-03	
1,3,5-TMB	3.73E-01	7.44E-03	7.33E-02	7.70E-03	4.39E-02	2	1.02E+00	1.00E-01	2	2	ջ	8	2	2.93E+01	BLQ	3,43E+02	2.94E+00	8.57E-01	3.04E+00	1.62E+00	8.89E+00	9.51E+01	1.03E+01	1.08E+00	8.43E-02	7.47E-02	7.96E-02	9.38E-02	1.57E-01	7.43E-02	1.03E-01	1.24E+00	3.84E-01	BLQ	
O-XYLENE	1.44E-01	3.59E-03	6.92E-02	4.86E-03	2.42E-02	S	9.93E-01	9.99E-02	Q	S	2	Ş	2	1.99E+01	BLQ	3.44E+02	5.58E+00	1.72E+00	5.28E+00	2.31E+00	9.17E+00	9.40E+01	1.00E+01	1.01E+00	3.16E-01	3.03E-01	3,21E-01	3.18E-01	5.67E-01	3.10E-01	4.03E-01	2.04E+00	7.25E-01	BLQ	
m-XYLENE	5.55E-01	1.43E-02	1.01E-01	4.04E-03	1.11E-01	200	9.93E-01	1.01E-01	2	Q	8	<u>Q</u>	8	6.31E+01	ВГО	3.45E+02	1.05E+01	1.83E+00	4.89E+00	9.88E-01	9.02E+00	9.39E+01	9.99E+00	1.01E+00	5.17E-01	6.04E-01	6.12E-01	6.21E-01	1.16E+00	6.16E-01	8.02E-01	4.74E+00	1.84E+00	8.84E-03	
P-XYLENE	2.76E-01	5.75E-03	1.05E-02	BLQ	3.78E-02	2	9.85E-01	1.01E-01	Q	Š	Q	<u>Q</u>	9	2.34E+01	BLQ	3.56E+02	4.81E+00	1,48E+00	4.69E+00	2.02E+00	8.67E+00	9.08E+01	1.02E+01	1.00E+00	2,43E-01	2,21E-01	2.33E-01	2.33E-01	4.27E-01	2.28E-01	2.81E-01	1.70E+00	6.25E-01	BLQ	
<u>EB</u>	2.64E-01	1.06E-02	1.28E-01	1.37E-01	1.71E-01	Q	9.94E-01	1.02E-01	8	문	QN	9	Q	1.12E+01	BLQ	3.44E+02	3.72E+00	1.12E+00	3.39E+00	1.31E+00	9.45E+00	9.40E+01	9.76E+00	1.02E+00	1.60E-01	1.52E-01	1.59E-01	1.50E-01	2.83E-01	1.50E-01	1.87E-01	1.03E+00	3,77E-01	860	
TOLUENE	BLQ	BLQ	8,09E-03	BLQ	ВГО	Q	1.02E+00	1.03E-01	<u>Q</u>	2	Q	S	2	2,04E-01	BLQ	3.45E+02	1.07E+00	3.04E-01	5.91E-01	1.17E-01	9.15E+00	9.47E+01	9.81E+00	1.02E+00	4.55E-02	4.36E-02	3.50E-02	9.36E-02	2.00E-01	1.59E-01	2.31E-01	3.75E+00	1.73E+00	1.68E-02	
BENZENE	1.29E-01	1.03E-02	3.93E-02	3.88E-02	3.14E-02	QN	1.05E+00	1.08E-01	QN	2	2	2	Q	1.61E+00	BLO	3.49E+02	5.01E-01	3.33E-01	6.53E-01	6.29E-01	1.03E+01	1.00E+02	9.74E+00	9.89E-01	6.78E-01	5.38E-01	6.65E-01	7.71E-01	1.45E+00	7.87E-01	8.66E-01	7.49E-01	4.90E-01	ВГО	
SAMPLENAME	820-24	82D-25	820-38	820-39	820-40	82F-2	1 ua/mi	0.1 ua/ml	82E-3	82E-13	82E-14	82E-15	82E-17	821-5	MeC12	333 ua/m)	821-15	821-16	821-17	821-18	10 µq/m/QC	100 µg/ml	10 µg/ml	1 µq/m²	821-19	821-20	821-21	821-22	821-23	821-24	821-25	821-26	821-27	821-28	

Units=mg/kg

HIII AFB Core Extract. J. C/MSD Analyses

Dr. Kampbell

SR#S

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Page 5 of 6 Printed: 9/1/93

BLQ < 0.01 µg/ml

Analyst: David A. Kovacs

Dr. Kampbell

SR#C

Analyst: David A. Kovacs

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Units E. (かつかいか) といっていない 1.2.4-TMB 1,3,6-TMB 2222 O-XYLENE 22222 C/MSD Analyses m-XYLENE 99999 HIII AFB Core Extrac -XYLENE 22222 22222 TOLUENE 2222 SR#SF- 5 Dr. Kampbell BENZENE 1.31E-02 8.94E-02 9.58E-01 9.25E+00 **9999** SAMPLENAME 10 µg/ml QC 1 µg/ml QC 82B-6 82B-7 82B-8 82B-10 82B-11 82B-12 82B-13 82B-14 82B-14 82B-14 0.01 µg/ml 0.1 µg/ml 1 բց/այ 82B-1 82B-2 82B-3 82B-4 82B-5

22222

1.25E-02 9.22E-02 9.63E-01 9.52E+00 1.04E+00 1.04E-01 9.56E-01 1,2,3-TMB BLQ 1.04E-01 9.43E-01 무 원 1.08E-02 9.45E-02 9.59E-01 9.75E+00 1.03E+00 1.14E-02 9.38E-02 9.38E-01 9.36E+00 1.02E+00 99999999 9 9 Ş 99999999999

2 2

1.02E-01 9.37E-01

0.1 µg/ml 1 µg/ml 82B-17

82B-18 82B-19 82B-20 82B-21

82B-22 82B-23 Analyst: David A. Kovacs

BLQ < 0.01 µg/ml

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1,2,3-TMB	4.91E-03	9.76E+00	1.04E+02	1.08E-01	5.53E-02	2.08E-01	9.05E-01	8.13E-03	3.63E-03	2.29E-02	1.45E-02	BLQ	3.11E-03	5.48E-02	BLQ	BLQ	1.15E-02	9.52E-02	9.83E-01	BLQ	Q	BLQ	BLQ	5.18E-03	1.27E-02	2.13E-02	Q	QN	1.09E+02	9.95E+00	8.21E-03	QN	BLQ	8.17E-01
1,2,4-TMB	1.67E-02	9.54E+00	1.04E+02	1.16E+00	1.03E+00	2.04E+00	4.42E+00	7.41E-02	1.68E-02	5.40E-02	3.71E-02	BLQ	8.85E-03	2.25E-01	BLQ	BLQ	1.02E-02	9.66E-02	9.91E-01	4.98E-03	9	4.16E-03	5.72E-03	6.95E-02	3.03E-02	3.99E-02	BLQ	BLQ	1.09E+02	9.86E+00	7.80E-02	3.10E-03	1.11E-02	3.11E+00
1,3,5-TMB	1.39E-02	9.41E+00	1.04E+02	1.65E+00	1.50E+00	2.34E+00	3.70E+00	8.01E-02	1.48E-02	3.88E-02	2.90E-02	4.16E-03	1.74E-02	1.95E-01	ВГО	ВГО	1.11E-02	9.85E-02	9.88E-01	BLQ	QN	6.32E-03	8.71E-03	6.37E-02	4.33E-02	3.65E-02	1.47E-02	2.58E-02	1.09E+02	1.00E+01	8.82E-02	4.77E-03	3.04E-02	2.53E+00
O-XYLENE	Q	9.77E+00	1.03E+02	1.51E-02	4.01E-03	aro	BLQ	BLQ	BLQ	1.36E-02	7.16E-03	вго	BLQ	4.51E-03	BLQ	BLQ	9.83E-03	9.86E-02	9.95E-01	BLQ	Š	BLQ	4.76E-03	BLQ	3.23E-02	4.50E-02	ВГО	BLQ	1.08E+02	1.00E+01	5.77E-03	BLQ	BLQ	7.32E-01
M-XYLENE	Q	9.53E+00	1.03E+02	2.57E-02	9.10E-03	9.56E-03	6.62E-02	9.91E-03	1.89E-02	5.21E-02	4.18E-02	BLQ	3.36E-03	3.45E-02	BLQ	BLQ	1.02E-02	9.86E-02	9.98E-01	ВГО	Q	1.67E-02	2.75E-02	1.94E-02	1.21E-01	1.81E-01	ВГО	BLQ	1.08E+02	1.00E+01	5.29E-03	3.03E-03	BLQ	3.40E+00
P-XYLENE	QN	9.34E+00	1.05E+02	4.20E-02	2.96E-02	3.65E-02	8.57E-02	1.10E-02	1.05E-02	2.21E-02	1.78E-02	BLQ	ВГО	1.36E-02	BLQ	BLQ	1.02E-02	9.88E-02	1.00E+00	BLQ	9	4.64E-03	7.55E-03	6.62E-02	3.90E-02	5.51E-02	BLQ	BLQ	1.08E+02	9.98E+00	3.88E-02	BLQ	1.30E-02	1.62E+00
EB	Q	1.00E+01	1.03E+02	1.80E-02	6.18E-03	5.58E-03	2.86E-02	6.42E-03	7.95E-03	1.24E-02	1.18E-02	1.59E-02	3,35E-03	8.71E-03	ВГО	BLQ	1.00E-02	9.87E-02	1.00E+00	QX	Q	1.15E-01	1.41E-01	1.24E-01	8.78E-02	6.13E-02	2.13E-02	3.44E-02	1.08E+02	9.96E+00	6.04E-02	9.49E-02	1.11E-01	1.48E+00
TOLUENE	QN	9.62E+00	1.03E+02	ВГО	1.76E-02	1.92E-02	2.00E-02	BLQ	BLQ	ВГО	BLQ	ВГО	870	ВГО	BLQ	B LQ	9.69E-03	9.93E-02	1.01E+00	ВГО	BLQ	ВГФ	BLQ	ВГО	BLQ	3.04E-03	BLQ	BLQ	1.08E+02	9.98E+00	ВГО	ВГФ	BLQ	вга
BENZENE	N	9.52E+00	9.87E+01	6.21E-03	BLQ	3.67E-03	3.27E-03	BLQ	BLQ	BLQ	BLQ	9.59E-03	Q	BLQ	ВГО	2	1.02E-02	9.87E-02	1.09E+00	BLQ	BLQ	2.03E-02	1.85E-02	2.09E-02	3.43E-02	3.16E-02	6.30E-03	7.92E-03	1.13E+02	1.10E+01	8.29E-03	1.04E-02	6.97E-02	2.71E-01
SAMPLENAME	82C-16	10 µg/m1QC	100 µg/ml	82C-19	82C-20	82C-21	82C-22	82C-23	82C-24	82C-25	82C-26	820-1	820-3	82D-4	MeC12	Method Blank	0.01 µg/ml	0.1 µg/ml	1 µg/ml	82D-5	82D-6	820-12	820-13	82D-14·	82D-15	82D-16	820-17	82D-18	100 µg/ml	10 µg/mľ	82D-19	82D-21	82D-22	82D-23

Units a. J

'MSD Analyses

HIII AFB Core Extra

SR#S" 0.1" Tr. Kampbell

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BLQ < 0.01 µg/m1

Analyst: David A. Kovacs

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Pr. Kampbell	
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SR#	

HIII AFB Core Extra. MSD Analyses

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Units=my/kg

1,2,3-TMB	1.35E-01	BLQ	3.84E-02	BLQ	1.63E-02	Q	1.00£+00	9.93E-02	QN QN	Q	QN N	ON ON	QN N	1.93E+01	ВГФ	3.42E+02	2.03E+00	6.72E-01	2.34E+00	1.25E+00	9.23E+00	9.50E+01	1.01E+01	1.01E+00	7.78E-02	7.09E-02	7.83E-02	8.99E-02	1.55E-01	7.49E-02	1
1,2,4-TMB	4.40E-01	7.02E-03	1.07E-02	BLQ	3.735-02	S	9.89E-01	9.91E-02	Q.	2	2	2	S	5.09E+01	ВГО	3.43E+02	8.45E+00	2.33E+00	8.37E+00	4.72E+00	9.01E+00	9.50E+01	1.02E+01	1.02E+00	2.22E-01	1.91E-01	2.06E-01	2.46E-01	4.02E-01	1.95E-01	
1,3,5-TMB	3.73E-01	7.44E-03	7.33E-02	7.70E-03	4.39E-02	2	1.02E+00	1.00E-01	2	2	S	NO NO	2	2.93E+01	BLQ	3.43E+02	2.94E+00	8.57E-01	3.04E+00	1.62E+00	8.89E+00	9.51E+01	1.03E+01	1.08E+00	8.43E-02	7.47E-02	7.96E-02	9.38E-02	1.57E-01	7.43E-02	
O-XYLENE	1.44E-01	3.59E-03	6.92E-02	4.86E-03	2.42E-02	QN	9.93E-01	9.99E-02	QX	2	Q	Q	Q	1.99E+01	BLQ	3.44E+02	5.58E+00	1.72E+00	5.28E+00	2.31E+00	9.17E+00	9.40E+01	1.00E+01	1.01E+00	3.16E-01	3.03E-01	3.21E-01	3.18E-01	5.67E-01	3.10E-01	
M-XYLENE	5.55E-01	1.43E-02	1.01E-01	4.04E-03	1.11E-01	S	9.93E-01	1.01E-01	Q	Q	QN	QN	Q	6.31E+01	ВГО	3.45E+02	1.05E+01	1.83E+00	4.89E+00	9.88E-01	9.02E+00	9.39E+01	9.99E+00	1.01E+00	5.17E-01	6.04E-01	6.12E-01	6.21E-01	1.16E+00	6.16E-01	70 100
D-XYLENE	2.76E-01	5.75E-03	1.05E-02	BLQ	3.78E-02	2	9.85E-01	1.01E-01	8	S	2	2	Š	2.34E+01	BLQ	3.56E+02	4.81E+00	1,48E+00	4.69E+00	2.02E+00	8.67E+00	9,08E+01	1.02E+01	1.00E+00	2,43E-01	2.21E-01	2.33E-01	2.33E-01	4.27E-01	2.28E-01	70 170 0
EB	2.64E-01	1.06E-02	1.28E-01	1.37E-01	1.71E-01	QX	9.94E-01	1.02E-01	S	2	ON	Q	2	1.12E+01	860	3.44E+02	3.72E+00	1.12E+00	3.39E+00	1.31E+00	9.45E+00	9.40E+01	9.76E+00	1.02E+00	1.60E-01	1.52E-01	1.59E-01	1.50E-01	2.83E-01	1.60E-01	TAG Y
TOLUENE	BLQ	BLQ	8.09E-03	BLQ	BLQ	S	1.02E+00	1.03E-01	2	2	2	S	2	2.04E-01	ВГО	3.45E+02	1.07E+00	3.04E-01	5.91E-01	1.17E-01	9.15E+00	9.47E+01	9.81E+00	1.02E+00	4.55E-02	4.36E-02	3.50E-02	9.36E-02	2.00E-01	1,59E-01	**
BENZENE	1.29E-01	1.03E-02	3.93E-02	3.88E-02	3.14E-02	8	1.05E+00	1.08E-01	S	Q	2	QN	S	1.61E+00	BLQ	3.49E+02	5.01E-01	3.33E-01	6.53E-01	6.29E-01	1.03E+01	1.00E+02	9.74E+00	9.89E-01	6.78E-01	5.38E-01	6.65E-01	7.71E-01	1.45E+00	7.87E-01	20 100 0
SAMPLENAME	82D-24	82D-25	82D-38	820-39	82D-40	82E-2	1 րց/m	0.1 µg/ml	82E-3	82E-13	82E-14	82E-15	82E-17	821-5	MeC12	333 µg/m!	821-15	821-16	821-17	821-18	10 µg/ml QC	100 µg/ml	10 µg/ml	1 μց/ալ	821-19	821-20	821-21	821-22	821-23	821-24	20.00

Analyst: David A, Kovacs

BLQ < 0.01 µg/m]

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7.49E-02 9.09E-02 9.5BE-01 2.72E-01 **B**C0

7.43E-02 1.03E-01

4.03E-01 3.10E-01

2.54E+00 2.44E-01

7.24E-01

3.84E-01 BLQ 1.24E+00

2.04E+00 7.25E-01 BLQ

1.84E+00 8.84E-03

4.74E+00

1.70E+00 2.81E-01

1.03E+00 1.87E-01

> 3.75E+00 1.73E+00

1.68E-02

2.31E-01

8.66E-01 7.49E-01 4.90E-01

821-25 821-26

821-27 821-28

3.77E-01

6.25E-01 BLQ

6.16E-01 8.02E-01 6.24E-03

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1,2,3-TMB	1.01E+00	9.53E-02	BLQ	ВГО	2.59E-01	3.096+00	Q	2	Q	9.37E-03	1.50E+00	3.10E-02	8.23E-01	BLO	BLO	1.06E+01	1.04E+02
12.4-TWB	1.04E+00	9.11E-02	BLQ	. BLQ	1.91E-02	7.62E+00	BLQ	Q	ВГО	1.72E-02	5.38E+00	1.13E-01	3.30E+00	8,0	BLO	1.05E+01	1.04E+02
1.3.6-TMB	1.08E+00	9.35E-02	BLQ	BLQ	4.18E-01	1.31E+01	BLQ	2	BLQ	1.21E-02	2.32E+00	3.10E-02	1.27E+00	BLQ	BLQ	1.04E+01	1.04E+02
O-XYLENE	1.03E+00	9.70E-02	BLQ	BLQ	BLQ	3.76E-02	9	S	ВГО	8.50E-02	4.79E+00	1.29E-01	1.03E+00	BLQ	BLQ	1.08E+01	1.04E+02
M-XYLENE	1.01E+00	9.92E-02	ВГО	BLQ	1.28E-02	1.79E+00	2	2	QN	8.98E-02	7.86E+00	5.92E-02	2.28E+00	BLQ	BLQ	1.06E+01	1.04E+02
p-XYLENE	1.01E+00	9.95E-02	ВГО	BLQ	ջ	1.05E+00	2	2	ВГО	3.64E-02	3.96E+00	1.54E-01	1.75E+00	BLQ	BLQ	1.04E+01	1.03E+02
	1.02E+00	9.81E-02	BLQ	BLQ	1.01E-01	1.24E+00	2.71E+01	1.61E+01	ВГФ	2.38E-02	2.72E+00	1.21E-01	1.31E+00	BLQ	BLQ	1.08E+01	1.04E+02
TOLUENE	1.05E+00	1.03E-01	1.57E-02	1.11E-02	1.14E-02	3.20E-02	1.22E-02	7.30E-03	1.37E-02	1.64E-02	1.82E-01	1.88E-02	6.74E-02	BLQ	ВГО	1.06E+01	1.04E+02
BENZENE	1.01E+00	1.05E-01	BLQ	BLQ	gra	1.36E-02	BLQ	BLQ	8.31E-03	8.12E-02	7.12E-01	3.15E-01	4.22E-01	BLQ	Q	1.06E+01	1.07E+02
SAMPLENAME	1 µg/mi	0.1 µg/ml	821-29	821-30	821-31	821-32	821-33	821-34	821-35	821-36	821-37	821-38	821-39	MeC12	Method Blank	10 µg/ml QC	100 µg/ml

Analyst: David A. Kovacs

BLQ < 0.01 µg/m1

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Ref: 93-DK8/vg

October 21, 1993

Dr. John T. Wilson R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74820

THRU: S.A. Yandegrift AR

Dear John:

Please find attached results of GC/MSD analysis of Hill AFB core extracts for quantitation of Benzene, Toluene, Ethylbenzene (EB), p-Xylene, m-Xylene, o-Xylene, 1,3,5-Trimethylbenzene (1,3,5-TMB), 1,2,4-Trimethylbenzene (1,2,4-TMB) and 1,2,3-Trimethylbenzene (1,2,3-TMB) as requested under Service Request #SF-0-26.

The analytical method was a modification of RSKSOP-124. Cool (38°C) on-column injection (0.5 μ l) was used with electronic pressure control (EPC) set for a constant flow of 0.9 ml/min. A 30M X 0.25 mm Restek Stabilvax (Crossbonded Carbovax-PEG, 0.5 μm film) capillary GC column with 1 foot long X 0.53 mm ID uncoated capillary precolumn was used. Quantification was based on two standard curves: A low level curve was used for extract concentrations in the range 0.01-1.0 μ g/ml (0.01, 0.1, 1.0 μ g/ml). The second curve was used for quantification of concentrations >1.0 $(1, 10, 100 \mu g/ml)$.

If you require further information, please feel free to contact me.

xc: R.L. Cosby J.L. Seeley G. Smith

Unite = my/kg

HIII AFB Core Extract GC/MSD Analyses

Service nequest SF-0-26 Dr. Wilson

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Page 1 of f Printed: 10/21/93

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	12.3-TMB	9.15€+01	1.07E+00	1.71€+00	2.53E+01	5.92E+01	1.54E+01	1.85E+01	B LQ	B LQ	2	810	BLQ	1.07E+00	1.09E-01	BLO	B C0	2	B LO	910	1.07E+00
	124-TMB	9.10E+01	1.03E+00	4.43E+00	6.98E+01	1.67E+02	4.27E+01	4.99E+01	BLQ	BLQ	BLQ	BLQ	810 810	1.06E+00	1.04E-01	BLO	979	BLO	BLQ	B (0	1.03E+00
•	1.3.6-TMB	D.40E+01	1.06E+00	2.30E+00	3.68E+01	8.88E+01	2.33E+01	2.81E+01	8 60	BLQ	910	BLG	BLQ	1.06E+00	1.01E-01	Bro	BLO	96	BLO	BLO	1.06E+00
	9-XXI ENE	9.22E+01	1.03E+00	1.61E+00	3.66E+01	1.00E+02	2.08E+01	1.82E+01	BLO	Bro	9 6	Bro	Bro	1.05E+00	9.93E-02	BLQ	BLQ	BLQ	BLO	8 50	1.03E+00
	M-XYLENE	9.22E+01	1.03E+00	3.67E+00	9.93E+01 ~	2.94E+02	6.23E+01	5.27E+01	8 [0	BLQ	810	BLQ	4.08E-03	1.05E+00	9.86E-0 2	BLQ	5.43E-03	BLQ	9 LQ	B LQ	1.03E+00
	P-XYLENE	9.39E+01	1.03E+00	1.22E+00	3.44E+01	1.05E+02	2.23E+01	1.99E+01	B LQ	BLQ	BLQ	ВГО	BLQ	1.06E+00	9.83E-02	BLQ	BLQ	BLQ	BLQ	BLQ	1.03E+00
		9.24E+01	1.03E+00	5.56E-01	1.75E+01	4.77E+01	4.83E+00	1.45E+01	B LO	BLQ	BLQ	B LQ	BLQ	1.08E+00	9.74E-02	BLQ	BLQ	BLO	BLQ	BLQ BLQ	1.03E+00
	г,	9.28E+01	•		•		-														-
	BENZENE	9.78E+01	1.05E+00	80	4.01E-01	4.55E+00	5.17E-01	3.26E-02	BLQ	BLQ	BLQ	BLQ	2	9.73E-01	1.04E-01	BLQ	D'B	ВГО	Š	Ş	1.05E+00
	SAMPLE	100 pg/ml QC	1 pg/mt	621-1	621-2	621-3	621-4	821-5	82I-8	821-7	821-8	6 21-9	821-10	1 pg/mi	0.1 µg/m	821-11	821-12	821-13	821-14	Method Blank	1 µg/m]

Analyst: David A. Kovacs

BLQ<0.01 µg/ml



Ref: 93-RC13/vg

September 21, 1993

er, John Filson.

R.S. Kerr Environmental Research Lab U.S. Environmental Protection Agency

Post Office Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift 4

Dear John:

Attached is a report of the data generated from the analyses of 143 sample core extracts from Hill AFB, UT. The extracts, which were submitted under Service Request #SF-0-5, were analyzed for total fuel content as JP-4 jet fuel only. The reported values for fuel carbon were computed from the JP-4 determinations. I have also attached a report of the quality control analyses that were performed concurrently with the sample analyses.

Data quantification, peak identification, component concentration calculations, and dilution factor corrections were performed by MAXIMA chromatography software. JP-4 data was quantified with a 7-point external standard calibration curve ranging from 50-50,000 ng/ μ l.

The Minimum Detectable Limit (MDL) for JP-4 is determined by the concentration of the lowest calibration standard, which is 50 ng/ μ l. Since the MDL is determined by a calibration standard, it may also be defined as the Minimum Quantifiable Limit (MQL). It is important to note that values less than the MQL are reported in this data set, but cannot be considered quantified since they lie outside the range of the standard curve. All such unquantified data are approximations extrapolated from the JP-4 standard curve.

The samples from Service Request #SF-0-5 had an average mass of 14.68 g, and were extracted with 5.0 ml of methylene chloride. For simplicity's sake, I have assumed complete extraction of the sample's contents into the 5.0 ml of solvent.

In order to compute the MQL of JP-4 in the average sample core, assume the following:

Sample mass = 14.68 g
Extract volume = 5.0 ml
Extraction efficiency = 100%
Determined mass of JP-4 = 50 ng
(in 1.0 µl of extract)

Monthch Environmental Technology, Inc.

Computation of the total mass of JP-4 in 5.0 ml of extract is as follows:

1.
$$\left(\frac{50 \text{ pg}}{1.0 \text{ pg}}\right)$$
 $\left(\frac{1000 \text{ pg}}{1000 \text{ pg}}\right)$ $\frac{5.0 \text{ pg}}{1000 \text{ pg}}$ = 250 pg

Consider that 22.28 g of sample was extracted with the 5.0 ml aliquot of methylene chloride and the original concentration is computed by division of the extracted mass of JP-4 by the sample mass:

2.
$$\frac{250 \ \mu g}{14.68 \ g} = 17.03 \ \mu g/g$$

Therefore, 17.03 μ g/g (or mg/kg, or ppm if you prefer either of these units) is the Minimum Quantifiable Limit (MQL) of JP-4 determined in these samples.

It should be realized that JP-4 determinations are based on the summation of multiple peak areas detected over a defined period of time rather than the area of a specific peak, which is typical of individual fuel component determinations. When using this method of determination, it is entirely possible for a single peak or a group of peaks not attributable to JP-4 to register enough area to be mistakenly represented as JP-4.

Sample extracts were received from Mark Blankenship on August 26, 1993. Analyses were started on August 26, 1993, and concluded on September 16, 1993. Sample extracts and quality control samples were analyzed according to RSKSOP-72, Rev. No. 1, excepting the modifications listed in the attached outline.

If you have any questions concerning this report, please contact me at your convenience.

Sincerely,

Landy Calladay

xc: R.L. Cosby ... J.L. Seeley

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1 /	

Hill	AFB Field Dat	a Number 2
Sample	Depth (ft)	JP-4 (mg/kg)
82 I-14 TO 82 I-8	13.8-16.28	1.2 to 0.73
82 I-7	16.28-16.64	2.4
82 I-6	16.64-17.00	30.4
8a I-5	17.0-17.36	5330 and 4330
82 I-4	17.36-17.72	3770
82 I-3	17.72-18.08	14800
82 I-2	18.08-18.44	5870
82 I-1	18.44-18.80	398
82 I-27	18.8-19.12	67.30
82 I-26	19.12-19.45	276.00
82 I-25	19.45-19.77	17.60
82 I-24	19.77-20.09	14.30
82 I-23	20.09-20.42	24.00
82 I-22	20.42-20.74	17.90
82 I-21 TO 82 I-19	20.74-21.71	12.96
82 1-18	21.71-22.03	720.00
82 I-17	22.03-22.35	1290.00
82 I-16	22.35-22.68	385.00
82 I-15	22.68-23.00	1190.00
82 1-39	23.0-23.2	485.00
82 I-38	23.2-23.4	8.06
82 I-37	23.4-23.76	1370.00
82 I-36	23.76-24.12	4.20
82 I-35	24.12-24.48	4.96
82 I-34	24.48-24.89	2.87
82 I-33	24.89-25.20	4.43
82 I-32	25.20-25.56	3830.00
82 I-31	25.56-25.92	834.00
82 I-30 TO 82 I-28	25.92-27.00	5.96

(4)

Hill	AFB Field Dat	a Number 2
Sample	Depth (ft)	TPH (mg/kg)
82 I-14 TO 82 I-8	13.8-16.28	<10
82 I-7 ·	16.28-16.64	138
82 I-6	16.64-17.00	139
8a I √ 5	17.0-17.36	3530
82 I-4	17.36-17.72	11500
82 I-3	17.72-18.08	28300
82 I-2	18.08-18.44	5160
82 I-1	18.44-18.80	6080
82 I-27	18.8-19.12	<10
82 I-26	19.12-19.45	<10
82 I-25	19.45-19.77	<10
82 I-24	19.77-20.09	<10
82 I-23	20.09-20.42	<10
82 I-22	20.42-20.74	<10
82 I-21 TO 82 I-19	20.74-21.71	<10
82 I-18	21.71-22.03	276
82 I-17	22.03-22.35	856 <u>±</u> 80
82 I-16	22.35-22.68	<10
82 I-15	22.68-23.00	643
82 I-39	23.0-23.2	<10
82 I-38	23.2-23.4	<10
82 I-37	23.4-23.76	340
82 I-36	23.76-24.12	<10
82 I-35	24.12-24.48	<10
82 I-34	24.48-24.89	<10
82 I-33	24.89-25.20	<10
82 T-32	25.20-25.56	410±256
82 I-31	25.56-25.92	<10
62 I-30 TO 82 I-28	25.92-27.00	<10

Hill	AFB Field Dat	a Number 2
Sample	Depth (ft)	JP-4 (mg/kg)
82 C-1	14.0	
82 C-2	13.5	
82 C-3	18.1	
82 C-4	17.8	
82 C-5	17.5	
82 C-6	17.2	
82 C-7	16.9	
82 C-8	16.6_	
82 C-9	16.3	
82 C-10	16.0	
82 C-11	15.7	
82 C-12	15.4	
82 C-13	22.9	
82 C-14	22.6	0.62
82 C-15	skipped	
82 C-16	22.3	1.01
82 C-17	22.1	
82 C-18	broke	
82 C-19	22.0	638.0
82 C-20	21.7	593.0
82 C-21	21.55	698.0
82 C-22	21.4	820.0
82 C-23	21.1	26.0
82 C-24	20.8	1.02
82 C-25	20.5	2.88
82 C-26	20.2	1.95

Hill	AFB Field Dat	a Number 2
Sample	Depth (ft)	TPH (mg/kg)
82 C-1	14.0	
82 C-2	13.5	
82 C-3	18.1	
82 C-4	17.8	
82 C-5	17.5	
82 C-6	17.2	
82 C-7	16.9	
82 C-8	16.6	
82 C-9	16.3	
82 C-10	16.0	
82 C-11	15.7	
82 C-12	15.4	
82 C-13	22.9	
82 C-14	22.6	<10
82 C-15	skipped	
82 C-16	22.3	<10
82 C-17	22.1	<10
82 C-18	broke	
82 C-19	22.0	444
82 C-20	21.7	530±14
82 C-21	21.55	173
82 C-22	21.4	352
82 C-23	21.1	<10
82 C-24	20.8	<10
82 C-25	20.5	<10
82 C-26	20.2	<10
·		

SR4SF-0-5 / Kampbell / Hill AFE

all conc. are ug/g

Sample I.D.	Dilution Factor	₽-4	Fuel Carbon (JR-4 x 0.85)
02 A1	1	1.14	
82 A2	î	0.79	0.97 0. 6 7
82 A3	ĩ	0.50	0.43
82 A4	1	0.68	0.58
82 A5	1	0.93	0.79
82 A6	1	0.73	0.62
82 A7	1	0.83	0.70
82 A8	1	1.36	1.16
62 A9 62 A 10	1	0.49	0.41
82 All	1	1.71	1.45
82 A12	1 1	1.30	1.11
82 A13	' i'	(1.63 0.68	1.39
82 3 14	ī)	0.99	0.58 0.84
82 A15	ī'	1.25	1.06
82 1 16	ı	0.81	0.69
82 A17	1	0.97	0.83
82 A18	1	2.72	2.31
82 1 19	1	0.64	0.54
82 A 20	1	0.76	0.65
82 A 21	1	1.23	1.05
82 A22 82 A23	1	0.79	0.67
82 A24	1	0.97	0.82
82 A25	i	0.76	0.65
82 A26	i	0.70 0 .9 7	0.59
2 A27	ī	0.68	0.83
9 2 A 28	ī	0.78	0.59 0.66
d2 A 29	1	1.03	0.88
82 A30	1	1.52	1.29
82 A31	1	0.72	0.61
82 A32	1	1.55	1.32
82 A33	1	0.83	0.71
82 A 34 82 A 35	1	0.76	0.64
82 A36	1	0.53	0.45
82 A37	1	0.98	0.84
82 A38	i	0.49 0.47	0.42
82 A39	ī	0.52	0.40
82 A40	ĩ	0.45	0.45 0.38
82 A 41	ī	0.84	0.72
82 A 42	1	3.37	2.86
82 λ 43	1	0.86	0.73
82 A44	1	0.74	0.63
82 A45	1	1.40	1.19
82 A46	1	2.59	2.20
82 A47 82 A48	1	2.01	1.71
82 A48 82 A49	1	1.54	1.31
82 A50	1	0.98	0.83
82 A51	i	0.52 0.56	0.45
82 A52	î	0.83	0.47
82 A53	î	0.68	0.71
82 A54	i	1.11	0.58
82 A55	ĩ	0.43	0. 94 0.37
	•		0.31

NOTE: all reported values are corrected for dilution factors where applicable

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SR#SF-0-5 / Kampbell / Ril AFE

all conc. are ug/g

Sample	I.D.	Dilution Factor	JP-4	Fuel Carbon (JP-4 x 0.85)
2 B 1		1	4.22	3.59
2 B2		1	1.53	1.30
B3		1	1.49	1.27
B4		1	1.06	0.90
B5		1	1.17	1.00
2 B6		1	1.16	0.99
B8		1	1.26 1.61	1.07
B9		i	1.35	1.37 1.15
B10		i	1.09	0.93
B11		î	1.15	0.98
B12		ī	1.44	1.22
B13		ī	1.27	1.08
B14		ĩ	1.52	1.29
B15		ī	1.04	0.88
B16		ī	0.83	0.71
B17	f 🛊	4 1	0.58	0.50
5 18	' #	1	0.69	0.59
B19	i.	1	0.99	0.85
B20		ı	0.71	0.60
B21		1	0.95	0.81
B22		1	1.31	1.11
B23		1	1.16	0.99
B24		À	0.66	0.56
B25		h lı	1.20	1.02
C14		1	0.62	0.53
C16		ı	1.01	0.86
C19		1	638. 00	542.00
C20	i i	ı	593.00	504.00
C21	•	1	698.00	593.00
C22		1	820.00	697.00
C23		1	26.00	22.10
C24 C25		1	1.02	0.87
C25		1	2.08	2.45
C.2.0		1	1.95	1.66
D1		1	1.12	0.95
D3		1	1.93	1.64
D4		1	79.60	67.70
D5		1	0.81	0.69
D6 D12		1	0.76	0.64
D13		1	3.09 3.30	2.63
D14		i	3.25	2.87
D15		1	2.41	2.76
D16		i	2.67	2.05 2.27
D17		i	0.56	0.48
D18		1	1.92	1.63
D19		1	2.72	2.31
D21		ī	1.83	1.56
D22		î	2.22	1.89
D23			572.00	486.00
D24		1 1	77.10	65.50
D25			1.69	1.44
D38		1	3.96	3.37
		1	4.12	3.50
D39 D40		i	6.12	5.20

NOTE: all reported values are corrected for dilution factors where applicable

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SR#SF-0-5 / Kampbell / Hill _B all conc. are ug/g

0	Sample I.D.	Dilution Factor	JP-4	Fuel Carbon (JP-4 x 0.85)
	82 E2	1	4.12	3.50
	82 E3	1	7.17	6.09
	62 E13	1	5.25	4.46
	82 E14	1	1.49	1.27
	82 E15	1	1.29	1.10
	62 217	1	1.69	1.61
	82 IS	1	5330.00	4530.00
	82 I15	ĩ	1190.00	1010.00
	82 I16	1	385.00	327.00
	82 I17	1	1290.00	1100.00
	82 I18	1	720.00	612.00
.'	82 I19	1	15.00	12.80
۳	82 I20	1	12.10	10.30
	62 I21	1	11.80	10.00
	82 I22	1	17.90	15.20
	82 123	1	24.00	20.40
	82 I24	1	14.30	12.20
	82 I25	1	17.60	15.00
	82 I26	1	276.00	235.00
	82 I27	1 1	67.30	57.20
	82 I28	1	5.24	4.45
	8 2 I 29	1 /	5.76	4.90
	82 I30	1 '	6.89	5.86
	92 I31	1	834.00	709.00
	☑ I32	1	3830.00	3260.00
	7 133	1	4.43	3.77
	2 134	1	2.87	2.44
	62 I3 5	1	4.96	4.22
	82 I36	1	4.20	3.57
1	82 I37	1	1370.00	1160.00
i	82 138	1	8.06	6.85
	62 I39	1	485.00	412.00

all reported values are corrected for dilution factors where applicable

SR#SF-0-5 / Rampbell / QC Te Sample I.D.

APR-04-1994 15:36

blk MeCl2 26AUG93 101.00 100 jp4 500 jp4 493.00 1000 jp4 5000 jp4 10000 jp4 50000 jp4 963.00 5190.00 10200.00 49000.00 blk MeCl2 31AUG93 1.61 8.61 Method blank #1 53.80 50 Jp4 500 jp4 1000 jp4 5000 jp4 492.00 \$46.00 5190.00 10000 jp4 50000 jp4 10400.00 50700.00 1.45 1492993 blk MeC12 1.72 Method blank #2 51.90 50 jp4 500 jp4 1000 jp4 5000 jp4 482.00 966.00 4750.00

blk MeCl2 - methylene chloride solvent blank jp4 = JP-4 fuel standard (ng/ul)

10000 jp4

9060.00 46900.00

P.29 425 436 8723 USEPA RSKERL-ADA SSB/SPB HP5890 GC - PRATING CONDITIONS Instrument Control Analyses: "SH-2-JP4" Program: "RWC-AS10" 2. Calibration: "DK-5-BTEX" B. Temperature Program Initial Temp & Time: 10°C for 3.00 min Level 1: Rate = 4°C/min to 70°C, Final Time = 0.00 Level 2: Rate = 10°C/min to 270°C, Final Time = 3. 2.00 4. Run Time: 40.00 min Oven, Equilibration Time: 1.00 min 5. C. Miscellaneous Peak Width: 0.02 1. Attentuation: 2⁵ 2. 3. Chart Speed: 0.50 Threshold = 0 4. 5. Offset = 10% MAXIMA PEAK ITEGRATION Peak Detection Parameters Baseline Points: 18 1. Filter Window (in points): 9 2. Intg. Sensitivity (coarse): 10.50 μ V/sec 3. Intg. Sensitivity (fine): $5.00 \mu V/sec$ Skim Ratio: 100.004. 5. B. Peak Rejection Criteria Minimum Area: 2000 µV-sec Minimum Height: 300.0 µV Minimum Width: 3.00 sec C. Integration Events 0.00: Disable Peak Skimming 1. 0.00: Disable Peak Detection 2. 5.00: Enable Peak Detection 5.12: Set Baseline 3. 4. 5. 5.50: Set Baseline 5.77: Set Baseline 6.

MAXIMA DATA ACQUISITION IV.

7.

8.

9.

Preacquisition Delay: 5.00 min

7.60: Set Baseline

18.25: Set Baseline

21.78: Set Baseline 10. 24.84: Set Baseline 11. 27.61: Set Baseline 12. 30.16: Set Baseline 13. 32.85: Set Baseline 14. 34.65: Set Baseline 15. 35.93: Set Baseline 16. 39.54: Set Baseline

B. Duration: 35.00 min C. Rate: 3.00 points/sec

Run Time: 40.00 min

v. MAXIMA CALIBRATION CURVES

JP-4

Calibration Range = $50 - 50,000 \text{ ng/}\mu\text{l}$ 1.

Summation of all peaks detected from 5.00 - 40.00 2. minutes



Ref: 93-RC16/vg

October 20, 1993

Dr. John Wilson

R.S. Kerr Environmental Research Lab U.S. Environmental Protection Agency

Post Office Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift SW

Dear John:

Attached is a report of the data generated from the analyses of 14 sample core extracts from Hill AFB, UT. The extracts, which were submitted under Service Request #SF-0-26, were analyzed for total fuel content as JP-4 jet fuel only. The reported values for fuel carbon were computed from the JP-4 determinations. I have also attached a report of the quality control analyses that were performed concurrently with the sample analyses.

Data quantification, peak identification, component concentration calculations, and dilution factor corrections were performed by MAXIMA chromatography software. JP-4 data was quantified with a 7-point external standard calibration curve ranging from 50 - 50,000 ng/ μ l.

The Minimum Detectable Limit (MDL) for JP-4 is determined by the concentration of the lowest calibration standard, which is 50 ng/ μ l. Since the MDL is determined by a calibration standard, it may also be defined as the Minimum Quantifiable Limit (MQL). It is important to note that values less than the MQL are reported in this data set, but cannot be considered quantified since they lie outside the range of the standard curve. All such unquantified data are approximations extrapolated from the JP-4 standard curve.

The samples from Service Request #SF-0-26 had an average mass of 15.23 g, and were extracted with 5.0 ml of methylene chloride. For simplicity's sake, I have assumed complete extraction of the sample's contents into the 5.0 ml of solvent.

In order to compute the MQL of JP-4 in the average sample core, assume the following:

Sample mass = 15.23 g
Extract volume = 5.0 ml
Extraction efficiency = 100%
Determined mass of JP-4 = 50 ng
(in 1.0 \(mu\)l of extract)

Manifech Environmental Technology, Inc.

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Computation of the total mass of JP-4 in 5.0 ml of extract is as follows:

1.
$$\left(\frac{50 \text{ pg}}{1.0 \text{ pg}}\right) \left(\frac{1000 \text{ pg}}{1000 \text{ pg}}\right) \left(\frac{5.0 \text{ pg}}{1000 \text{ pg}}\right) = 250 \text{ pg}$$

Consider that 22.28 g of sample was extracted with the 5.0 ml aliquot of methylene chloride and the original concentration is computed by division of the extracted mass of JP-4 by the sample mass:

2.
$$\frac{250 \text{ } \mu\text{g}}{15.23 \text{ g}} = 16.41 \text{ } \mu\text{g/g}$$

Therefore, 16.41 $\mu g/g$ (or mg/kg, or ppm if you prefer either of these units) is the Minimum Quantifiable Limit (MQL) of JP-4 determined in these samples.

It should be realized that JP-4 determinations are based on the summation of multiple peak areas detected over a defined period of time rather than the area of a specific peak, which is typical of individual fuel component determinations. When using this method of determination, it is entirely possible for a single peak or a group of peaks not attributable to JP-4 to register enough area to be mistakenly represented as JP-4.

Sample extracts were received from Mark Blankenship on October 15, 1993. Analyses were started on October 18, 1993, and concluded on October 19, 1993. Sample extracts and quality control samples were analyzed according to RSKSOP-72, Rev. No. 1, excepting the modifications listed in the attached outline.

If you have any questions concerning this report, please contact me at your convenience.

Singerely

Randy Callavay

xc: R.L. Cosby J.L. Seeley

SR#SF-0-26 /	Wilson / Eil.	78 .	ll conc. are ug/g	0
Sample I.D.	Dilution Factor	J9-4	Fuel Carbon (JP-4 z 0.85)	`
6 2 I1	1	398.00	338.00	
82 12	ī	5870.00	4990.00	
62 13	10	14800.00	12600.00	
82 14	ī	3770.00	3200.00	
82 IS	ī	4330.00	3600.00	
82 I6	ī	30.40	25.80	
82 I7	ĩ	2.35	2.00	
82 18	ī	0.73	0.62	
82 19	1	0.84	0.72	
82 I10	1	0.86	0.73	
82 Ill	1 ,	0.83	0.71	
82 I12	1	0.88	0.75	
82 II3	1 4	1.24	1.05	
82 114	1 7	0.98	0.83	

NOTE: all reported values are corrected for dilution factors where applicable

SRIST-0-26 / Wilson / QC T :

all conc. are mg/wl (

Sample I.b.

JP-4

blk MeCl2	1800793	1.70
Nethod blank		2.21
500 1p4		520.00
5000 jp4		4880.00
50000 jp4		47400.00
blk MeCl2	210CT93	2.96
1000 jp4		976.00
10000 p4		9130.00

blk MeCl2 - methylene chloride solvent blank jp4 = JP-4 fuel standard (ng/ul)

P.34 USEPA RSKERL-ADA SSB/SPB 405 436 8703 HP5890 GC - PERATING CONDITIONS I. Instrument Control Analyses: "SH-2-JP4" 1. Program: "RWC-AS10" 2. Calibration: "DK-5-BTEX" 3. Temperature Program B. Initial Temp & Time: 10°C for 3.00 min Level 1: Rate = 4°C/min to 70°C, Final Time = 0.00 Level 2: Rate = 10°C/min to 270°C, Final Time = 3. 2.00 Run Time: 40.00 min 4. Oven Equilibration Time: 1.00 min 5. C. Miscellaneous 1. Peak Width: 0.02 2. Attentuation: 2⁵ Chart Speed: 0.50 3. 4. Threshold = 0 Offset = 10% 5. II. MAXIMA PEAK ITEGRATION Peak Detection Parameters Baseline Points: 18 Filter Window (in points): 13 2. Intg. Sensitivity (coarse): 5.00 μ V/sec Intg. Sensitivity (fine): 5.00 μV/sec 4. B. Peak Rejection Criteria Minimum Area: 2000 µV-sec 1. 2. Minimum Height: 300.0 μ V 3. Minimum Width: 3.00 sec

- C. Integration Events
 - 0.00: Disable Peak Skimming 0.00: Disable Peak Detection
 - 5.00: Enable Peak Detection 3.
 - 4. 19.96: Set Baseline
 - 5. 21.74: Set Baseline
 - 6. 23.23: Set Baseline
 - 7. 26.20: Set Baseline
 - 8. 27.58: Set Baseline
 - 28.66: Set Baseline 30.20: Set Baseline 9.
 - 10.
 - 32.81: Set Baseline 11.

IV. MAXIMA DATA ACQUISITION

- Preacquisition Delay: 5.00 min A.
- B. Duration: 35.00 min
- C. Rate: 3.00 points/sec
- Run Time: 40.00 min D.

٧. MAXIMA CALIBRATION CURVES

- JP-4
 - Calibration Range = $50 50,000 \text{ ng/}\mu\text{l}$ 1.
 - Summation of all peaks detected from 5.00 40.00 2. minutes

FAX



MONTGOMERY WATSON

4525 So. Wasatch Blvd. Suite 200 Salt Lake City, UT 84124-4799

Tel: 801 272-1900 Fax: 801 272-0430

Date:

July 29, 1994

To:

Todd Wiedemeir

Fax No:

From:

Bob Glascott

Reference:

Subject:

Survey Data

No. of Pages:

(including cover) 3

Todd, here is the survey data, please check the attached map to see that everything is labeled properly, I had problems reading your original fax with the designations. If anything was missed etc. please call and we'll get it fixed. When you finish with the appendicies for the Intrinsic Remediation manual I'd like to get a copy, keep me posted, thanks. B

If you do not receive all pages, or if there are any problems with this transmission, please call Bob Glascott at 801 273-2471

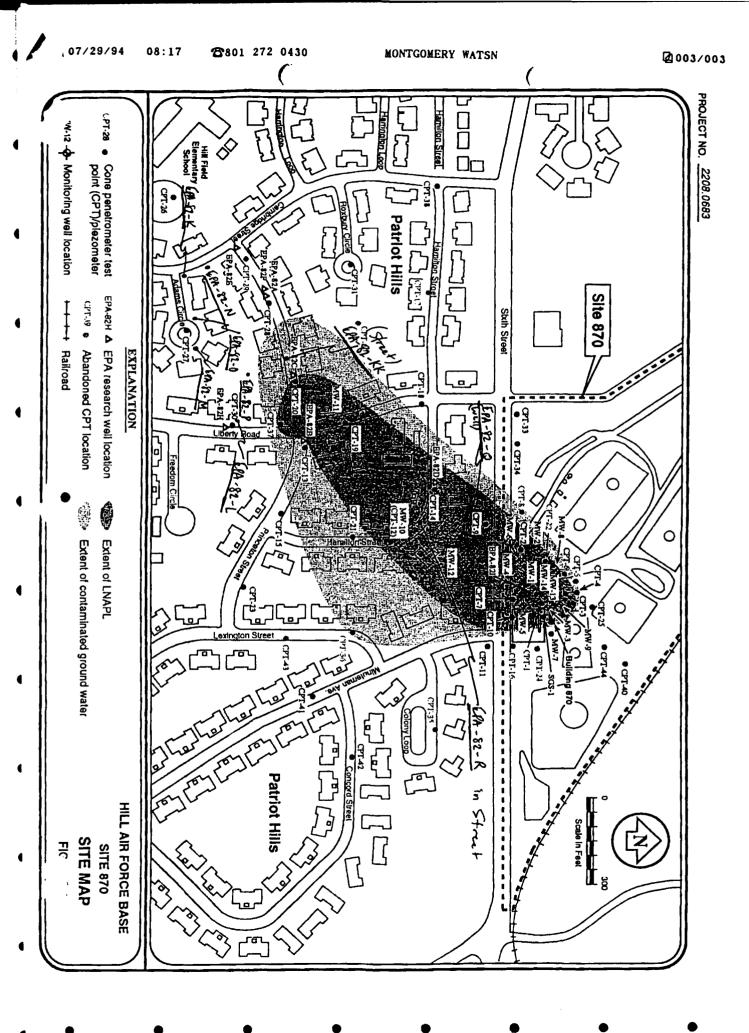
PATRIOT HELS/HAFB WELLS AND BORINGS JMM WATSON 27 JULY 1994

Well No.	Northing	Easting	<u>Elevation</u>	Note
EPA-82L	282834.32	1851944.25	4614.15	Boring
EPA-82M	282698.09	1861700.50	4605.01	Boring
EPA-820	282688.82	1861594.50	4602.30	Boring
EPA-82K	282656.22	1861458.62	4598.38	Boring
EPA-82N	282738.09	1861425.23	4599.81	Boring
EPA-82KK	282995.57	1861711.36	4614.97	Boring
EPA-82P	282865.35	1861776.37	4612.65	Boring
EPA 82-R	283471.51	1862263.77	4660.14	Boring
EPA 82-Ø J	283645.85	1862398.75	4676.17	Outcase
EPA 82-Q'J	283645.85	1862398.75	4675.82	PVC

SS ENGINEERING-SCIENCE, INC.

Total Aprin = Base of Sumperny Futernal

ID = 0.25 Screen rength = Scriple totals



JOHN. CRD

Wiedemeier, Todd

Engineering Science, Inc.

1700 Broadway, Suite 900

Denver, CO 80290

303/831-8100

FAX: 303-831-8208

Home phone: 303/969-0159

From John Wilson USEPA, Ada, OK. Pluse the to

(60) 17.7

i 5

Printed 25-Jul-94 SF-0-70

DP-P&T/GC-FID:PID Analyses for Dr. Kampbell & Dr. Wilson ルールー E-NES

910 810 8LQ 8LQ 8LQ 8LQ 1.27E 403 1.31E 404 8LQ 6.35E 400 4.30E 401 1.30E 401 5.00E 101 5.30E 102 78E+02 43E+02 1,2,4-1748 4.87E+01 5.00E+01 5.45E+02 4.17E+02 4.85E+02 ND 9.58E+00 3.98E+02 .25E+02 1.44E+02 1,3,5-TMB BLO BLO BLO 2 2 2 5.00E+01 5.00E+01 5.18E+02 BLQ BLQ 2.30E+03 1.78E+03 6.04E+02 9.98E+00 3.18E+00 O-XYLENE 5.07E+01 910 910 물 물 물 5.13E+03 4.22E+03 BLQ 1.00E+01 5.72E+02 4.92E+01 5.00E+01 5.17E+02 8LQ 8LQ **M.XYLENE** .42E+02 1.93E+01 .83E+01 8 8 8 8 8 1.62E+03 1.37E+03 BLO 3.79E+02 2.38E+01 8.53E+00 2.72E+02 5.00E+01 5.28E+02 BLQ BLQ 9.24E+00 **D-XYLENE** 2.59E+01 BLQ BLO D 81.0 81.0 ETHYLBENZENE 5.00E+01 5.25E+02 ND BLQ 9.55E+02 8.16E+02 BLQ 9.24E+00 1.03E+02 9.72E+00 4.54E+02 2.27E+01 5.22E+01 81.0 81.0 BLO BLO 5.28E+02 3.816+03 TOLUENE 5.00E+01 9.74E+00 9.71E+00 5.87E+03 9.77E+00 1.01E+01 BLO B BL0 BCo BLO ջ 2 4.58E+02 BLQ 4.28E+03 BLO 5.04E+01 5.00E+01 5.60E+03 8.00E+00 5.01E+02 7.28E+00 .01E+01 BENZENE BLO BLQ BLO 2 2 OC, OBSERVED, PPB OC, TRUE VALUE, PPB 500 PPB SAMPLE NAME 82-F Duplicate 10 PPB 82·L1 82·H 82-C 82-B 82.D 82.E 82.A 82-X 82.) 402 436 8703

ND = None Detected; BLQ = Belcw Limit of Quantitation, 1 ppb; N/A = Not Analyzed

Z0.9

NZEPA RSKERL-ADA SSB√SPB

82-M Ouplicate

6.56E-00 6.33E-00 BLO BLO

2.33E+00 2.23E+00

7.43E+00

2.20E+01

3.58E+01 1.29E+01

2.02E+01

1.59E 02 3.03E 02 9LO 1.62E 01 1.01E 02 4.79E 01 5.00E 01

2.15E+02 BLQ 9.89E+00

7.77E+01

5.09E+00 4.41E+02 BLQ

1.88E+01 8.47E+02

1.15E+01

3.50E+00

BLO BLO

22

4.05E+00 5.10E+00 BLQ BLQ

7.59E+00 7.63E+00 BLQ BLQ

2.89E+00 2.77E+00 BLQ BLQ

4.00E+00 1.58E+00 1.50E+00

3.00E+00 3.10E+00

BLO BLO BLO

7.19E+00

1.88E+01

4.01E+00

27.28 82-13 82-M

1.44E+00

BLO BLO BLO BLO BLO 1.08E+03

5.00E+01 1.03E+03

4.72E+01

4.98E+01 5.00E+01

4.95E+01 5.00E+01

.80E+01

.01E+02

9.78E+01 4.87E+01

9.90E+01 4.83E+01 5.00E+01

> ac, TRUE VALUE, PPB QC, OBSERVED, PP&

100 PPB

MW-10 MW-11 **MW-12**

85-0

82.P

82.N

5.10E+01

0.00E-01

.00E+01

5.00E+01 1.02E+03

5.00E+01 1.01E+03

1.03E+02

.01E+02

.73E+01

9.45E+00 9.82E+01

BLO

.90E+02 BLQ .82E+00 .01E+02

1.82E+02 BLQ

5.47E+01

2.00E+01

8 S B

R B B

11:24 10L-27-1994

Printed 25-Jul-94 SF-0-70			Units = ng/ml. Analyst:1. Black	i.t. 81qck	
SAMPLE NAME	1,2,4-TMB	1,2,3-TMB	Total Fuel Carbon	_ . ^ / sa	
•				-	
OC, OBLERVED, PPB	4.77E+01	4.79E+01	ΝA		
OC, TRUE VALUE, PPB	5.00E+01	5.00E+01	ΝΆ		
500 PPB	5.385+02	5.42E+02	∀Z	. -	
82.A	BLQ	BLO	BLO		
82.B	BLO	018	BLO		
82-C	1.43E+02	4.20E+01	1.32E+03	- -	
82-D	1.76E+02	6.04E+01	3.135+03	 	
82-E	BLO	BLO	BLO		
82.F	BLQ	<u>Q</u>	BLO	<u>.</u>	
82.F Duplicate	8.0	2	BLO	·•	
82·H	80	2	90	<u>. </u>	
82-1	1.276+33	4.36E+02	2.68E+04		
82-7	1,31€+03	5,15E+02	1.84E+04		
82.K	BLO	2	910	-	
10 PPB	9.35E+00	9.88E+00	ΑZ	س.	
. 82-L1	4.33E+02	2.23E+02	3.72E+03		
82-12	2,86E+01	1.52E+01	4.31E+02	-	
82-L3	1.385+01	6.88E+00	9.82E+01	-	
M-28	4.56E+00	3.08E+00	2.98E+01	<u>.</u>	
82-M Duplicate	4.33E+00	2.93E+00.	2.82E+01	·	
82·N	BLO	BLO	80	· · ·	
82.0	BLO	BLQ	BLQ		
82.P	1.59€+02	5.78E+01	5.39E+02		
MW-10	3.03E+02	1.97E+02	3.67E+03		
MW-11	BLQ	BLO	BLQ	***************************************	
MW-12	3.82E+01	1.33E+01	5.96E+02		
100 PPB	1.01E+02	9.88E+01	ΥX	-	
	4.78E+01	4.58E+01	K Z	,,,,,, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
QC, TRUE VALUE, PPB	5.00E+01	5.00E+01	∀ N	 L."	
1000 PPB	1.08E+03	1.07E+03	Ϋ́		

22222

≈ ≈

ロコニロ

ND = None Detected; BLQ = Below L

402 436 8703 6.03

2 2 2

22

NZEWA RSKERL-ADA SSB/SPB

107-53-1994 11:34

Printed 25-Jul-84 SF-0-70			Units = ng/mL Analyst: L Bla	st: L 1914
SAMPLENAME	1,2,4-TMB	1,2,3-TMB	Total Fuel Carbon	••
OC, OB: ERVEO, PPB	4,77E+01	4.70E+01	A/N	
QC, TRUE VALUE, PPB	\$.00E+01	5.00E+01	¥	
500 PPB	5.36E+02	5,42E+02	¥	••
62.A	BLQ	87.0	BLO	
85.B	8 8	BLO	BLO	
(83.c	1.436+02	4.28E+01	1.32E+03	
· 82-D	1.76E+02	6.04E+01	3,135+03	
. 82∙€	28	BLO	BLO	
82.F	ි වූ	2	910	
82.f Duplicate	979	2	BLQ	_
82.H	8F0	2	9,0	•
62.1	. 1.27E+03	4.38E+02	2.58E+04	,
62.7	1,316+03	5,15E+02	1.04E+04	
	aro	2	978	•
10 PPB	9.35E+00	9.98E+00	Ϋ́Z	
82·L1	4.335+02	2.23E+02	3.72E+03	-
82.12	2.86E+01	1.52E+01	4.31E+02	
82·U3	1.38E+01	6.88E+00	9.62E+01	
62·M	4.56E+00	3.06E+00	2.88E+01	
82-M Duplicate	4.33E+00	2.93€+00.	2.82E+01	
85-N	BLC	BLQ	8CQ	<u>.</u>
82-0	BLO	BLQ	B C0	•
82.5	1.50E+02	5.79E+01	5.39E+02	
) ww.10	3,03E+02	1.97E+02	3.67E+03	
11.MM	910 810	BLQ B	970	
MW.12	3.625+01	1,33E+01	5.96E+02	-
100 PPB	1.01E+02	9.88E+01	¥	-
OC, OBSERVED, PPB	4.78E+01	4.58E+01	₹	-
OC, THUE VALUE, PPB	5.00E+01	5.00E+01	ΥX	-
1000 PPB	1.06E+03	1.07E+03	¥	

405 436 8703 P.02

NZELY KSKERL-ADA SSB/SPB

91:81 1661-82-JUL

	11:41	Air force BAS	<u> </u>
	Field	Data	•
Samol	TOTAL NIK mall calog	Ferrious 10AN mg/d	Hydrogen Sulf
824	492	4.05	ms/4
82 A	530	4.05	4.1
82 F	490	•5	۷.1
85 E	357	۷.05	<u> </u>
82 3	429	• 1	##** =
82 D	657	7.4	. •1
m.w10	502	٠٥ .	•5
82 I	4 91	10.3	۷.۱
mwn	504	4.05	. —
mw12	450	4.05	
82 L I	. 130	9.4	۷.1
8262	732	.1	۷.1
821-3	706	. •1	
82 M	686	4.05	
BSN	32. e	4.05	_
850	566	۷،05	
8215	498	4.05	~ .
82 P	792	. 2	
82 3	430	1.3	

4

1 1/2

<u>Sample</u>	mg/1 NO' ₂ + NO' ₃ (N)	mg/l Cl	mg/1 80 ⁻² ,	<u>Conductivity</u>
82L1 82L1 Dup 82L2 82L3 82M 82N 82N Dup	<.05 <.05 .05 .30 1.80 1.14	112 86.4 90.1 73.8 120 120	<.5 36.0 61.0 35.4 42.6 44.8	1730 1731 1645 1588 1509 1336
Blank AQC AQC T.V. Spike Rec.	<.05 11.0 11.0 102%	<.5 40.6 41.2 102%	<.5 91.3 92.0 98%	
Sample	mg/l NO ₂ + NO ₃ (N)	mg/l Cl	mg/1 _50 ⁻²	Conductivity

Sample	$\frac{\text{mg/l}}{\text{NO}_2 + \text{NO}_3(\text{N})}$	mg/1 Cl'	mg/1 50 ⁻² ,	Conductivity
82J 82J Dup 82K 82O 82P	.05 .05 4.44 1.63 <.05	158 60.0 78.4 148	<.5 59.8 37.1 <.5	1328 1328 1220 1455 1704
Blank AQC AQC T.V. Spike Rec.	<.05 11.0 11.0 102%	<.5 40.6 41.2 102%	<.5 91.3 92.0	

Samples Received Tuly 11, 1994

<u>Sample</u>	mg/L TOC
82 A	2.8
82 B	2.2
82 D	10.3
82 E	1.7
82 F	4.4
82 H	2.6
82 I	67.1
MW-10	9.3
MW-11	3.5
MW-12	2.4
MW-12 Lab Dup	2.4
WP031 II	80.0
RO H ₂ O	<0.1

Samples Received July 12, 1994

<u>Sample</u>	mg/L Toc
82 L1	5.6
82 Ll Field Dup	4.4
82 L2	3.1
82 L3	2.4
82 M	2.9
82 N ,	3.7
WP031 II	79.9
RO H ₂ O	<0.1

Samples Received July 14, 1994

<u>Sample</u>	mq/L TOC
82 J	46.0
82 K	2.4
82 O	2.8
82 P	6.8
82 P Lab Dup	6.8
WP031 II	79.9
RO H ₂ O	<0.1

True Value of WP031 II = 82.0

Sample	mg/1 NO ₂ + NO ₃ (N)	mg/l Cl	mg/l so",	Cond.
82A	<.05	156	58.6	1,677
82A Dup				1,677
828	.15	145	74.2	1,450
82D	<.05	221	<.5	1,953
82E	4.39	354	37.0	2,050
82F	1.67	46.9	52.3	1,208
82F Dup		46.1	52.5	-
82H	1.51	129	62.3	1,431
82I	<.05	76.7	<.5	1,139
MW10	2.67	47.1	19.5	1,123
MW10 Dup				1,123
MW11	<.05	27.0	99.1	1,161
MWll Dup	<.05	26.8	102	
MW12	7.73	13.2	29.2	999
Blanks	<.05	<.05	<.05	
AQCWP031	.49	40.6	91.9	~~~~
True Value	.52	41.2 ~	92.0	
Spike Recove		96%	93%	

SF-0-70 DATA

LYZED 7/13/	94		
SAMPLE	METHANE	ETHYLENE	ETHANE
LAB BLANK	BLQ	ND	ND
82 A	0.001	ND	NO
82 B	0.001	ND	ND
82 D	0.002	0.001	0.003
82 E	0.001	NO	ND
82 F	0.577	ND	0.007
82 H	0.001	ND	NO
82 I	1.886	0.001	0.004
82 I LAB DUP	1.755	0.001	0.003
MW-10	0.006	ND	0.001
MW-11	0.005	ND	0.001
MW-12	0.005	ND	0.000
ANALYZED 7/14/9	94		
SAMPLE	METHANE	ETHYLENE	ETHANE
LAB BLANK	BLQ	ND	ND
82 L1	0.018	ND	0.001
rail FIELD DUP	0.018	ND	0.001
● 82 L2	0.003	ND	0.001
82 L3	0.002	ND	0.001
82 M	0.121	ND	0.001
82 N	0.004	ND	0.001
ANALYZED 7/15/9	4		
SAMPLE	METHANE	ETHYLENE	ETHANE
LAB BLANK	BLQ	ND	ND
82 J	0.052	0.009	0.009
82 K	0.003	ND	0.001
82 O	0.001	ND	0.001
82 P	0.004	ND	0.001
STANDARDS	METHANE	ETHYLENE	ETHANE
10 PPM CH4	10.00	ND	ND
100 PPM CH4	100.00	ND	ND
1060 PPM CH4	995.11	ND	ND
1 % CH4	1.01	ND	ND
4 % CH4	4.00	ND	NO
10 PPM C2H4	ND	10.01	NO
) PPM C2H4	ND	100.00	ND





CLIENT: Montgomery

ATTN:

ANALYSIS:

4525 So. Wasatch #200 Salt Lake City, UT 84124

LAB NO: 22313 GROUP NO: 4674 DATE SAMPLED:

11/06/91

TIME SAMPLED: 1350 DATE RECEIVED: 11/07/91

Mr. Dave Fulton

DATE REPORTED: 11/14/91 DISPOSAL DATE: 12/14/91

SAMPLE ID: SB870A-01/16'-17'

Total Petroleum Hydrocarbons by EPA SW-846 Methods

3550/8015 Modified [Utah]. Benzene, Toluene,

Ethylbenzene, Xylenes by EPA SW-846 Methods 5030/8020.

	RESULT	LIMIT OF
COMPOUNDS	DRY WEIGHT	QUANTITATION
Moisture	21.9 %	
Benzene	150 ug/kg	10.0 ug/kg
Toluene	129 ug/kg	10.0 ug/kg
Ethylbenzene	57.0 ug/kg	10.0 ug/kg
m,p-Xylene	203 ug/kg	10.0 ug/kg
o-Xylene	115 ug/kg	10.0 ug/kg
TPH	< 10.0 mg/kg	10.0 mg/kg

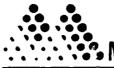
Date Analyzed (TPH): 11/12/91 Date Analyzed (BTEX): 11/14/91

Note:

Diesel fuel calibration standards were used for TPH quantitation.

Respectfully submitted,

Kenneth A. Roberts, B.S.



Mountain States Analytical

The Quality Solution

CLIENT: Montgomery

4525 So. Wasatch #200

Salt Lake City, UT 84124-

Phone:

801-272-1900 801-272-0430 (FAX)

ATTN:

Mr. David Fulton

HAFB Project:

Date Samples Rec'd: 11/07/91

MSAI Group No.:

Sample Matrix: Non-Aqueous/Solid

Report Date:

11/14/91

4674

P.O. Number:

2208.0312

LAB SAMPLE

SAMP SAMPLE DESCRIPTION

NO. DATE TIME

22313 11/06/91 1350 SB870A-01/16'-17'

22314 11/06/91 1400 53870A-01/18'-19'

ANALYSES PERFORMED

RESULT

BTEX/TPH 8015/8020(D) See Attach ---Homogenization-Vol. GC Complete ---

21.9 % Moisture

BTEX/TPH 8015/8020(D)

Moisture

See Attach ---

Homogenization-Vol. GC Complete ---

19.4 %

110V 2 0 1991

Respectfully submitted,

deun (2 Acres. nn A. Sorensen, B.S.

Manager, Technical Operations

1645 West 2200 South, Salt Lake City, Utah 84119 (801) 973-0050 FAX (801) 972-6278





Montgomery CLIENT:

4525 So. Wasatch #200

LAB NO: GROUP NO: 22314 4674

Salt Lake City, UT 84124

DATE SAMPLED: 11/06/91 TIME SAMPLED:

Mr. Dave Fulton

DATE RECEIVED: 11/07/91 DATE REPORTED: 11/14/91

DISPOSAL DATE: 12/14/91

SAMPLE ID: SB870A-01/18'-19'

ANALYSIS:

ATTN:

Total Petroleum Hydrocarbons by EPA SW-846 Methods

3550/8015 Modified [Utah]. Benzene, Toluene,

Ethylbenzene, Xylenes by EPA SW-846 Methods 5030/8020.

COMPOUNDS	RESULT DRY WEIGHT	LIMIT OF QUANTITATION
Moisture	19.4 %	
Benzene Toluene Ethylbenzene m,p-Xylene o-Xylene TPH	564 ug/kg 145 ug/kg 341 ug/kg 1,640 ug/kg 609 ug/kg 98.3 mg/kg	20.0 ug/kg 20.0 ug/kg 20.0 ug/kg 20.0 ug/kg 20.0 ug/kg 10.0 mg/kg
= 1		

Date Analyzed (TPH): 11/12/91 11/14/91 Date Analyzed (BTEX):

Note:

Diesel fuel calibration standards were used for TPH quantitation.

Respectfully submitted,

Kenneth A. Roberts, B.S.

Manager, Organics Department

1645 West 2200 South, Salt Lake City, Utah 84119 (801) 973-0050 FAX (801) 972-6278



REMARKS RECEIVED BY: (SIGNATURE) RECEIVED BY: (SIGNATURE) DATE / TIME DATE / TIME REMARKS ANALYSIS USE I COLUMN PER BOTHE DATE / TIME CHAIN OF CUSTODY RECORD REUNQUISHED BY: (SIGNATURE) REUNOUISHED BY: (SIGNATURE) NO. OF CON-TAINERS RECEIVED FOR LABORATORY BY: (SIGNATURE) SECTION OF COLOR OF C 158870A-01/18-11 STATION LOCATION 10-1048 K DATE / TIME DATE / TIME PROJECT NAME CBVB LABORATORIES
PROJECT/JOB # **MONTGOMERY** Zuco SAMPLERS: (Signature) 1/6/4, 11-60 "16/4, [1352] 3ME 2208.0312. REUNOUSHED BY: RELINQUISHED BY: (SIGNATURE) REUNQUISHED BY: (SIGNATURE) DATE ₹ ö

(8)





CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200 Salt Lake City, UT 84124 LAB NO: 22369

GROUP NO: 4687 DATE SAMPLED: 11/07/91

TIME SAMPLED: 1111
DATE RECEIVED: 11/08/91
DATE REPORTED: 11/21/91

ATTN:

Mr. David Fulton

DATE REPORTED: 11/21/91 DISPOSAL DATE: 12/21/91

SAMPLE ID: SB870A 02/15'16'

ANALYSIS:

Total Petroleum Hydrocarbons by EPA SW-846 Methods

3550/8015 Modified [Utah]. Benzene, Toluene,

Ethylbenzene, Xylenes by EPA SW-846 Methods 5030/8020.

COMPOUNDS	RESULT DRY WEIGHT	LIMIT OF QUANTITATION
Moisture	18.9 %	
Benzene	43.2 ug/kg	10.0 ug/kg
Toluene	51.3 ug/kg	10.0 ug/kg
Ethylbenzene	52.2 ug/kg	10.0 ug/kg
m,p-Xylene	365 ug/kg	10.0 ug/kg
o-Xylene	92.3 ug/kg	10.0 ug/kg
TPH	23.2 mg/kg	10.0 mg/kg
Date Analyzed (TPH):	11/13/91	
Date Analyzed (BTEX):	11/20/91	

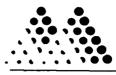
Note:

Diesel fuel calibration standards were used for TPH quantitation.

Respectfully submitted,

Flynd Alighel

Kenneth A. Roberts, B.S. Manager, Organics Department



The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200

Salt Lake City, UT 84124

Phone: ATTN:

801-272-1900 801-272-0430 (FAX) Mr. David Fulton

Project: HAFB

Date Samples Rec'd: 11/08/91

MSAI Group No.: 4687

Sample Matrix: Non-Aqueous/Solid

Report Date: 11/21/91

P.O. Number: 2208.0312

		SAMPLE DATE	SAMP TIME	SAMPLE	DESCRIPTION	ANALYSES PERFORMED	RES	JLT
	22369	11/07/91	1111	SB870A	02/15'-16'	BTEX/TPH 8015/8020(D) Homogenization-Vol. GC Moisture	See Attach Complete 18.9	
]	22370	11/07/91	1122	SB870A	02/17'-18'	BTEX/TPH 8015/8020(D) Homogenization-Vol. GC Moisture	See Attach Complete 24.2	
l	.2371	11/07/91	1427	SB870A	03/11'-12'	BTEX/TPH 8015/8020(D) Homogenization-Vol. GC Moisture	See Attach Complete 7.26	
]	22372	11/07/91	1530	SB870A	03/19'-20'	BTEX/TPH 8015/8020(D) Homogenization-Vol. GC Carbon, Organic TOC sw Moisture	See Attach Complete 1,100 20.3	 mg/kg
] 	22373	11/07/91	1630	SB870A	03/29'-30'	BTEX/TPH 8015/8020(D) Homogenization-Vol. GC Moisture	See Attach Complete 14.0	

Respectfully submitted,

Douglas W. Later, ih.D. Laboratory Director

Glenn A. Sorensen, B.S. Manager, Technical Operations

1645 West 2200 South, Salt Lake City, Utah 84119 (801) 973-0050 FAX (801) 972-6278



TAYARINYA (OF IN THE CHOICE

Mountain States Analytical

The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200 Salt Lake City, UT 84124 LAB NO: 22370
GROUP NO: 4687
DATE SAMPLED: 11/07/91

TIME SAMPLED: 11/07/91

ATTN: Mr. David Fulton

DATE RECEIVED: 11/08/91 DATE REPORTED: 11/21/91 DISPOSAL DATE: 12/21/91

, clev

SAMPLE ID: SB870A 02/17'18'

ANALYSIS: Total Petroleum Hydrocarbons by EPA SW-846 Methods

3550/8015 Modified [Utah]. Benzene, Toluene,

Ethylbenzene, Xylenes by EPA SW-846 Methods 5030/8020.

COMPOUNDS	RESULI DRY WEIG	
Moisture	24.2	%
Benzene	13.0	ug/kg 10.0 ug/kg
Toluene	60.2	ug/kg 10.0 ug/kg
Ethylbenzene	57.7	ug/kg 10.0 ug/kg
m,p-Xylene	386	ug/kg 10.0 ug/kg
o-Xylene	123	ug/kg 10.0 ug/kg
TPH		mg/kg 10.0 mg/kg
Date Analyzed (TI	PH): 11/13/91	L
Date Analyzed (B)		

Note:

Diesel fuel calibration standards were used for TPH

quantitation.

Respectfully submitted,

Kenneth A. Roberts, B.S.

Manager, Organics Department

1645 West 2200 South, Salt Lake City, Utah 84119 (801) 973-0050 FAX (801) 972-6278



Member: American Council of Independent Laboratories, Inc.

Agalytical Report

Mountain States Analytical

The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200 Salt Lake City, UT 84124 LAB NO: 22371
GROUP NO: 4687
DATE SAMPLED: 11/07/91
TIME SAMPLED: 1427

DATE RECEIVED: 11/08/91

ATTN: Mr. David Fulton

DATE REPORTED: 11/21/91 DISPOSAL DATE: 12/21/91

SAMPLE ID: SB870A 03/11'-12'

ANALYSIS: Total Petroleum Hydrocarbons by EPA

SW-846 Methods 3550/8015 Modified [Utah] Benzene, Toluene, Ethylbenzene, Xylenes

by EPA SW-846 Methods 5030/8020

COMPOUNDS	RESULT DRY WEIGHT	LIMIT OF QUANTITATION	
Moisture	7.3 %		
Benzene Toluene Ethylbenzene m,p-Xylene o-Xylene TPH	9,400 ug/kg 115,000 ug/kg 66,700 ug/kg 494,000 ug/kg 140,000 ug/kg 2,790 mg/kg	5,000 ug/kg 5,000 ug/kg 5,000 ug/kg 5,000 ug/kg 5,000 ug/kg 200 mg/kg	
Date Analyzed (TPH):	11/13/91		

Date Analyzed (TPH): 11/13/91 Date Analyzed (BTEX): 11/20/91

Note:

. ₹

A. Gasoline calibration standards were used for TPH quantitation.

Respectfully submitted,

Kenneth A. Roberts, B.S.



The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200 Salt Lake City, UT 84124 LAB NO: 22373
GROUP NO: 4687
DATE SAMPLED: 11/07/91

TIME SAMPLED: 1630
DATE RECEIVED: 11/08/91

ATTN:

Mr. David Fulton

DATE REPORTED: 11/21/91 DISPOSAL DATE: 12/21/91

SAMPLE ID: SB870A 03/29'-30'

ANALYSIS:

Total Petroleum Hydrocarbons by EPA SW-846 Methods 3550/8015 Modified [Utah] Benzene, Toluene, Ethylbenzene, Xylenes

by EPA SW-846 Methods 5030/8020

COMPOUNDS	RESULT DRY WEIGHT	LIMIT OF QUANTITATION
Moisture	14.0 %	
Benzene	22,200 ug/kg	5,000 ug/kg
Toluene	187,000 ug/kg	5,000 ug/kg
Ethylbenzene	83,100 ug/kg	5,000 ug/kg
m,p-Xylene	567,000 ug/kg	5,000 ug/kg
o-Xylene	177,000 ug/kg	5,000 ug/kg
TPH	15,100 mg/kg	1,000 mg/kg
Date Analyzed (TPH):	11/13/91	
Date Analyzed (BTEX):	11/20/91	

Note:

. 氢.

A. Gasoline calibration standards were used for TPH quantitation.

Respectfully submitted,

Kenneth A. Roberts, B.S.



The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200 Salt Lake City, UT 84124 LAB NO: 22372 GROUP NO: 4687 DATE SAMPLED: 11/07/91 TIME SAMPLED: 1530

Mr. David Fulton ATTN:

DATE RECEIVED: 11/08/91 DATE REPORTED: 11/21/91 DISPOSAL DATE: 12/21/91

SAMPLE ID: SB870A 03/19'-20'

Total Petroleum Hydrocarbons by EPA SW-846 Methods ANALYSIS:

3550/8015 Modified [Utah]. Benzene, Toluene,

Ethylbenzene, Xylenes by EPA SW-846 Methods 5030/8020.

COMPOUNDS	RESULT DRY WEIGHT	LIMIT OF QUANTITATION
Moisture	20.3 %	
Benzene Toluene Ethylbenzene m,p-Xylene o-Xylene TPH	338 ug/kg 595 ug/kg 138 ug/kg 867 ug/kg 276 ug/kg < 10.0 mg/kg	10.0 ug/kg 10.0 ug/kg 10.0 ug/kg 10.0 ug/kg 10.0 mg/kg

Date Analyzed (TPH): 11/13/91 Date Analyzed (BTEX): 11/20/91

Note:

Diesel fuel calibration standards were used for TPH

quantitation.

Respectfully submitted,

Kenneth A. Roberts, B.S.





J.M. Montgomery Engineers CLIENT:

4525 So. Wasatch #200

Salt Lake City, UT 84124-

Mr. Robert Glascot

SAMPLE ID: 870-WS-1/32'

SAMPLE NO:

0001523 SAMPLE SET NO: 000297S

11/23/92 DATE SAMPLED:

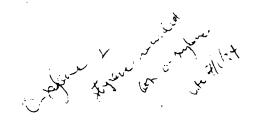
TIME SAMPLED:

DATE RECEIVED: 11/25/92 DATE REPORTED:

DISPOSAL DATE: 01/09/93

ANALYSIS: Volatiles - Water Matrix [EPA 601/602] (Capillary)

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Chloromethane	<	2.0 ug/l	2.0 ug/l
Vinyl Chloride	<	2.0 ug/l	2.0 ug/l
Bromomethane	<	2.0 ug/l	2.0 ug/l
Chloroethane	<	2.0 ug/l	2.0 ug/l
Fluorotrichloromethane	<	2.0 ug/l	2.0 ug/l
1,1-Dichloroethene	<	1.0 ug/l	1.0 ug/l
Dichloromethane	<	1.0 ug/l	1.0 ug/l
trans-1,2-Dichloroethene	<	1.0 ug/l	1.0 ug/l
1,1-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Chloroform	<	1.0 ug/l	1.0 ug/l
1,1,1-Trichloroethane	<	1.0 ug/l	1.0 ug/l
Carbon Tetrachloride	<	1.0 ug/l	1.0 ug/l
Benzene		17.4 ug/l	1.0 ug/l
1,2-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Trichloroethene (TCE)	<	1.0 ug/l	1.0 ug/l
1,2-Dichloropropane	<	1.0 ug/l	1.0 ug/l
Bromodichloromethane	<	1.0 ug/l	1.0 ug/l
cis-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
trans-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
Toluene		1.8 ug/l	1.0 ug/l
Tetrachloroethene (PCE)	<	1.0 ug/l	1.0 ug/l
Chlorodibromomethane	<	1.0 ug/l	1.0 ug/l
Chlorobenzene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene	<	1.0 ug/l	1.0 ug/l
Bromoform	<	2.0 ug/l	2.0 ug/l
m,p-Xylene		4.9 ug/l	1.0 ug/l
o-Xylene/Styrene*		1.3 ug/l	1.0 ug/l





0001523 CLIENT: J.M. Montgomery Engineers LAB NO: 4525 So. Wasatch #200 GROUP NO: 000297S Salt Lake City, UT 84124-DATE SAMPLED: 11/23/92 TIME SAMPLED: 1500 Mr. Robert Glascot DATE RECEIVED: 11/25/92 DATE REPORTED: 12/10/92

SAMPLE ID: 870-WS-1/32'

-Page 2-

COMPOUND(s)	FIN	AL RESULT	LIMIT OF QUANTITATION
1,1,2,2-Tetrachloroethane 1,1,2-Trichloroethane 1,2-Dichlorobenzene 1,3-Dichlorobenzene 1,4-Dichlorobenzene	< < < <	1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l	1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l

Date Analyzed:

12/02/92

*These compounds coelute under the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

DISPOSAL DATE:

01/09/93

Kenneth A. Roberts, B.S.

GC Group Leader

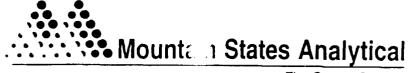


J.M. Montgomery Engineers SAMPLE NO: 0001524 CLIENT: 000297S SAMPLE SET NO: 4525 So. Wasatch #200 11/23/92 Salt Lake City, UT 84124-DATE SAMPLED: TIME SAMPLED: 1630 DATE RECEIVED: Mr. Robert Glascot 11/25/92 ATTN: 12/10/92 DATE REPORTED: SAMPLE ID: 870-WS-1/42' DISPOSAL DATE: 01/09/93

ANALYSIS: Volatiles - Water Matrix [EPA 601/602] (Capillary)

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Chloromethane	<	20.0 ug/l	20.0 ug/l
Vinyl Chloride	<	20.0 ug/l	20.0 ug/1
Bromomethane	<	20.0 ug/l	20.0 ug/l
Chloroethane	<	20.0 ug/l	20.0 ug/l
Fluorotrichloromethane	<	20.0 ug/l	20.0 ug/l
1.1-Dichloroethene	<	10.0 ug/l	10.0 ug/l
Dichloromethane	<		10.0 ug/l
trans-1,2-Dichloroethene	<	10.0 ug/l	10.0 ug/l
1,1-Dichloroethane	<	10.0 ug/l	10.0 ug/l
Chloroform	<	10.0 ug/l	10.0 ug/l
1,1,1-Trichloroethane	<	10.0 ug/l	10.0 ug/l
Carbon Tetrachloride	<	10.0 ug/l	10.0 ug/l
Benzene		30.5 ug/l	10.0 ug/l
1,2-Dichloroethane	<	10.0 ug/l	10.0 ug/l
Trichloroethene (TCE)	<	10.0 ug/l	10.0 ug/l
1,2-Dichloropropane	<	~ .	10.0 ug/l
Bromodichloromethane	<		10.0 ug/l
cis-1,3-Dichloropropene	<		10.0 ug/l
trans-1,3-Dichloropropene	<	10.0 ug/l	10.0 ug/l
Toluene		113 ug/l	10.0 ug/l
Tetrachloroethene (PCE)	<	10.0 ug/l	10.0 ug/l
Chlorodibromomethane	<	10.0 ug/l	10.0 ug/l
Chlorobenzene	<	10.0 ug/l	10.0 ug/l
Ethylbenzene		56.4 ug/l	10.0 ug/l
Bromoform	<	20.0 ug/l	20.0 ug/l
m,p-Xylene		369 ug/l	10.0 ug/l
o-Xylene/Styrene*		103 ug/l	10.0 ug/l





CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200

Salt Lake City, UT 84124-

Mr. Robert Glascot

SAMPLE ID: 870-WS-1/42'

ATTN:

LAB NO: 0001524

GROUP NO: 000297S

DATE SAMPLED: 11/23/92 TIME SAMPLED: 1630

DATE RECEIVED: 11/25/92

DATE REPORTED: 12/10/92

DISPOSAL DATE: 01/09/93

-Page 2-

COMPOUND(s)	FI	NAL RESULT	LIMIT OF QUANTITATION	
1,1,2,2-Tetrachloroethane	<	10.0 ug/l	10.0 ug/l	
1,1,2-Trichloroethane	<	10.0 ug/l	10.0 ug/l	
1,2-Dichlorobenzene	<	10.0 ug/l	10.0 ug/l	
1,3-Dichlorobenzene	<	10.0 ug/l	10.0 ug/l	
1,4-Dichlorobenzene	<	10.0 ug/l	10.0 ug/l	

Date Analyzed: 12/09/92

*These compounds coelute under the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

Kenneth A. Roberts, B.S.

GC Group Leader





CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200

Salt Lake City, UT 84124-

Mr. Robert Glascot

SAMPLE ID: 870-WS-1/52'

ATTN:

0001533 SAMPLE NO:

SAMPLE SET NO: 000297S

11/24/92 DATE SAMPLED: TIME SAMPLED: 830

11/25/92 DATE RECEIVED:

DATE REPORTED: 12/10/92 01/09/93 DISPOSAL DATE:

ANALYSIS: Volatiles - Water Matrix [EPA 601/602] (Capillary)

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Chloromethane	<	2.0 ug/l	2.0 ug/l
Vinyl Chloride	<	2.0 ug/l	2.0 ug/l
Bromomethane	<	2.0 ug/l	2.0 ug/l
Chloroethane	<	2.0 ug/l	2.0 ug/l
Fluorotrichloromethane	<	2.0 ug/l	2:0 ug/l
1,1-Dichloroethene	<	1.0 ug/l	1.0 ug/l
Dichloromethane	<	1.0 ug/l	1.0 ug/l
trans-1,2-Dichloroethene	<	1.0 ug/l	1.0 ug/l
1,1-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Chloroform	<	1.0 ug/l	1.0 ug/l
1,1,1-Trichloroethane	<	1.0 ug/l	1.0 ug/l
Carbon Tetrachloride	<	1.0 ug/l	1.0 ug/l
Benzene		27.0 ug/l	1.0 ug/l
1,2-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Trichloroethene (TCE)	<	1.0 ug/l	1.0 ug/l
1,2-Dichloropropane	<	1.0 ug/l	1.0 ug/l
Bromodichloromethane	<	1.0 ug/l	1.0 ug/l
cis-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
trans-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
Toluene		59.3 ug/l	1.0 ug/l
Tetrachloroethene (PCE)	<	1.0 ug/l	1.0 ug/l
Chlorodibromomethane	<	1.0 ug/l	1.0 ug/l
Chlorobenzene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene		21.6 ug/l	1.0 ug/l
Bromoform	<	2.0 ug/1	2.0 ug/l
m,p-Xylene		107 ug/l	1.0 ug/l
o-Xylene/Styrene*		36.4 ug/1	1.0 ug/l





The Quality Solution

James M. Montgomery Engineers 4525 South Wasatch Blvd., Suite 200

Salt Lake City, UT 84124 Telephone: (801) 272-1900 Facsimile: (801) 272-0403

Sample Number:

0001533

Sample Set: Date Reported: 0002978

Date Received:

10 DEC 1992 25 NOV 1992

Disposal Date:

8 JAN 1993

Attention: Project:

Robert Glascot

Case Number:

HAFB USTs VOCs/BTEXN

Purchase Order: 2208.0585

Customer Number: 870-WS-1/52'

Date Sampled:

24 NOV 1992

Matrix:

Water/Waste Water

Containers:

Catalog Dry Number Result **Analysis** Method Result 05515 EPA 600 Series 601/

Volatile Aromatics/Halocarbons

602

See Attached

Reporting Units

1 Analysis for GC

Reviewed and approved by Kenneth Roberts, B.S. GC Group Leader

1 Analysis for Sample Number 0001533





CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200

Salt Lake City, UT 84124-

SAMPLE NO: 0001526 SAMPLE SET NO: 000297S

DATE SAMPLED: 11/24/92 TIME SAMPLED: 1015

ATTN: Mr. Robert Glascot

SAMPLE ID: 870-WS 2/49'

DATE RECEIVED: 11/25/92 DATE REPORTED: 12/10/92 DISPOSAL DATE: 01/09/93

ANALYSIS: Volatiles - Water Matrix [EPA 601/602] (Capillary)

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Chloromethane	<	2.0 ug/l	2.0 ug/l
Vinyl Chloride	<	2.0 ug/l	2.0 ug/l
Bromomethane	<	2.0 ug/l	2.0 ug/l
Chloroethane	<	2.0 ug/l	2.0 ug/l
Fluorotrichloromethane	<	2.0 ug/l	2.0 ug/l
1,1-Dichloroethene	<		1.0 ug/l
Dichloromethane	<	1.0 ug/l	1.0 ug/l
trans-1,2-Dichloroethene	<	1.0 ug/l	1.0 ug/l
1,1-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Chloroform	<		1.0 ug/l
1,1,1-Trichloroethane	<	1.0 ug/l	1.0 ug/l
Carbon Tetrachloride	<.	1.0 ug/l	1.0 ug/l
Benzene		8.4 ug/l	1.0 ug/l
1,2-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Trichloroethene (TCE)	<	1.0 ug/l	1.0 ug/l
1,2-Dichloropropane	<	1.0 ug/l	1.0 ug/l
Bromodichloromethane	<	1.0 ug/l	1.0 ug/l
cis-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
trans-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
Toluene		13.8 ug/l	1.0 ug/l
Tetrachloroethene (PCE)	<	1.0 ug/l	1.0 ug/l
Chlorodibromomethane	<	1.0 ug/l	1.0 $ug/1$
Chlorobenzene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene		4.5 ug/l	1.0 ug/l
Bromoform	<	2.0 ug/l	2.0 ug/l
m,p-Xylene		30.2 ug/l	1.0 ug/l
o-Xylene/Styrene*		9.4 ug/l	1.0 ug/l





J.M. Montgomery Engineers CLIENT:

4525 So. Wasatch #200

Salt Lake City, UT 84124-

Mr. Robert Glascot ATTN:

SAMPLE ID: 870-WS 2/49'

0001526 LAB NO:

000297S GROUP NO:

11/24/92 DATE SAMPLED:

TIME SAMPLED: 1015

DATE RECEIVED: 11/25/92

12/10/92

DATE REPORTED:

DISPOSAL DATE: 01/09/93

-Page 2-

COMPOUND(s)	FINAL RESULT	LIMIT OF QUANTITATION
1,1,2,2-Tetrachloroethane 1,1,2-Trichloroethane 1,2-Dichlorobenzene 1,3-Dichlorobenzene 1,4-Dichlorobenzene	<pre></pre>	1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l

Date Analyzed: /

12/02/92

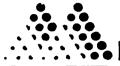
*These compounds coelute under/the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

Kenneth A. Roberts, B.S.

GC Group Leader





The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200

Salt Lake City, UT 84124-

ATTN: Mr. Robert Glascot

SAMPLE ID: 870-WS-2/59'

SAMPLE NO: 0001528 SAMPLE SET NO: 000297S

DATE SAMPLED: 11/24/92

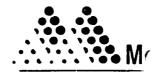
TIME SAMPLED: 1200 DATE RECEIVED: 11/25/92

DATE REPORTED: 12/10/92 DISPOSAL DATE: 01/09/93

ANALYSIS: Volatiles - Water Matrix [EPA 601/602] (Capillary)

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Chloromethane	<	2.0 ug/l	2.0 ug/l
Vinyl Chloride	<	2.0 ug/l	2.0 ug/l
Bromomethane	<	2.0 ug/l	2.0 ug/l
Chloroethane	<	2.0 ug/l	2.0 ug/l
Fluorotrichloromethane	<	2.0 ug/l	2.0 ug/l
1,1-Dichloroethene	<	1.0 ug/l	1.0 ug/l
Dichloromethane	<	1.0 ug/l	1.0 ug/l
trans-1,2-Dichloroethene	<	1.0 ug/l	1.0 ug/l
1,1-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Chloroform	<	1.0 ug/l	1.0 ug/l
1,1,1-Trichloroethane	<	1.0 ug/l	1.0 ug/l
Carbon Tetrachloride	<	1.0 ug/l	1.0 ug/l
Benzene		24.0 ug/l	1.0 ug/l
1,2-Dichloroethane	<		1.0 ug/l
Trichloroethene (TCE)	<	J.,	1.0 ug/l
1,2-Dichloropropane	<	1.0 ug/l	1.0 ug/l
Bromodichloromethane	<	1.0 ug/l	1.0 ug/l
cis-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
trans-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
Toluene		68.0 ug/l	1.0 ug/l
Tetrachloroethene (PCE)	<	1.0 ug/l	1.0 ug/l
Chlorodibromomethane	<	1.0 ug/l	1.0 ug/l
Chlorobenzene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene		50.7 ug/l	1.0 ug/l
Bromoform	<	2.0 ug/l	2.0 ug/l
m,p-Xylene		294 ug/l	50.0 ug/l
o-Xylene/Styrene*		93.7 ug/l	1.0 ug/l





The Quality Solution

J.M. Montgomery Engineers CLIENT:

LAB NO: DATE SAMPLED: 0001528

4525 So. Wasatch #200

GROUP NO: 000297S

Salt Lake City, UT 84124-

11/24/92

Mr. Robert Glascot

1200 TIME SAMPLED: DATE RECEIVED: 11/25/92

DATE REPORTED: 12/10/92

SAMPLE ID: 870-WS-2/59'

ATTN:

01/09/93 DISPOSAL DATE:

-Page 2-

COMPOUND(s)	. AL RESULT	LIMIT OF QUANTITATION
1,1,2,2-Tetrachloroethane 1,1,2-Trichloroethane 1,2-Dichlorobenzene 1,3-Dichlorobenzene 1,4-Dichlorobenzene	<pre>1.0 ug/l 4</pre>	1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l

Date Analyzed:

12/02/92

*These compounds coelute under the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

Kenneth A. Roberts, B.S.

GC Group Leader



0001529

000297S

11/24/92

11/25/92

12/10/92 01/09/93

1315



The Quality Solution

SAMPLE NO:

SAMPLE SET NO:

DATE SAMPLED: TIME SAMPLED:

DATE RECEIVED:

DATE REPORTED:

DISPOSAL DATE:

J.M. Montgomery Engineers CLIENT:

4525 So. Wasatch #200

SAMPLE ID: 870-WS-2/69'

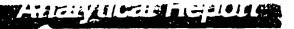
ATTN:

Salt Lake City, UT 84124-

Mr. Robert Glascot

ANALYSIS: Volatiles - Water Matrix [EPA 601/602] (Capillary)

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
		2.0/1	2.0 ug/l
Chloromethane	<	2.0 ug/l	2.0 ug/1 2.0 ug/1
Vinyl Chloride	<	2.0 ug/l	2.0 ug/l
Bromomethane	<	2.0 ug/l	2.0 ug/1 2.0 ug/1
Chloroethane	<	2.0 ug/l	2.0 ug/1
Fluorotrichloromethane	<	2.0 ug/l	1.0 ug/l
1,1-Dichloroethene	<	1.0 ug/l	1.0 ug/1
Dichloromethane	<	1.0 ug/l	— — — — — — — — — — — — — — — — — — —
trans-1,2-Dichloroethene	<	1.0 ug/l	1.0 ug/l
1,1-Dichloroethane	<	,	1.0 ug/l
Chloroform	<		1.0 ug/l
1,1,1-Trichloroethane	<	1.0 ug/l	1.0 ug/l
Carbon Tetrachloride	<	1.0 ug/l	1.0 ug/l
Benzene		43.5 ug/l	1.0 ug/l
1,2-Dichloroethane	<		1.0 ug/l
Trichloroethene (TCE)	<		1.0 ug/l
1,2-Dichloropropane	<	1.0 ug/l	1.0 ug/l
Bromodichloromethane	<		1.0 ug/l
cis-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
trans-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
Toluene		71.7 ug/l	1.0 ug/l
Tetrachloroethene (PCE)	<	1.0 ug/l	1.0 ug/l
Chlorodibromomethane	<	1.0 ug/l	1.0 ug/l
Chlorobenzene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene		38.2 ug/l	1.0 ug/l
Bromoform	<	2.0 ug/l	2.0 ug/l
m,p-Xylene		258 ug/l	50.0 ug/l
o-Xylene/Styrene*		63.6 ug/l	1.0 ug/l





The Quality Solution

James M. Montgomery Engineers 4525 South Wasatch Blvd., Suite 200

Salt Lake City, UT 84124 Telephone: (801) 272-1900 Facsimile: (801) 272-0403

Sample Number: 0001529 Sample Set: 000297S Date Reported: 10 DEC 1992 Date Received: 25 NOV 1992 Disposal Date: 8 JAN 1993

Attention: Project:

Robert Glascot HAFB USTs VOCs/BTEXN

Case Number: Purchase Order: 2208.0585 Customer Number: 870-WS-2/69' Date Sampled: Matrix:

24 NOV 1992 Water/Waste Water

Containers:

2

Analysis	Catalog Number	Method	Result	Dry Result	Reporting Units
Volatile Aromatics/Halocarbons	05515	EPA 600 Series 601/ 602	See Attached		

1 Analysis for GC

Reviewed and approved by Kenneth Roberts, B.S. GC Group Leader

1 Analysis for Sample Number 0001529



malytical Report



The Quality Solution

J.M. Montgomery Engineers LAB NO: 36821 CLIENT: 4525 S Wasatch #200 GROUP NO: 9132 DATE SAMPLED: 10/19/92 Salt Lake City, UT 94124 TIME SAMPLED: 1700 10/20/92 ATTN: Mr. David Fulton DATE RECEIVED: 10/21/92 DATE REPORTED: SAMPLE ID: CPT-10 DISPOSAL DATE: 11/20/92 ANALYSIS DATE: 10/20/92

ANALYSIS:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT	
Chloromethane	-10 ng/1	10 110/1	
	<10 ug/l <10 ug/l	10 ug/l 10 ug/l	
Vinyl Chloride Bromomethane	<10 ug/1 <10 ug/1	10 ug/1 10 ug/l	
Chloroethane	<10 ug/1 <10 ug/1	10 ug/l	
Trichlorofluoromethane		5 ug/l	
	<5 ug/l	100 ug/l	
Acrolein	<100 ug/l		
1,1-Dichloroethene	<5 ug/l	5 ug/l	
Methylene Chloride	12 ug/l	5 ug/l	
Acrylonitrile	<100 ug/l	100 ug/l	
1,1-Dichloroethane	<5 ug/l	5 ug/l	
1,2-Dichloroethene (total)	<5 ug/l	5 ug/l	
Chloroform	<5 ug/l	5 ug/l	
1,1,1-Trichloroethane	<5 ug/l	5 ug/l	
Carbon Tetrachloride	<5 ug/l	5 ug/l	
Benzene	<5 ug/l	5 ug/l	
1,2-Dichloroethane	<5 ug/l	5 ug/l	
Trichloroethene	<5 ug/l	5 ug/l	
1,2-Dichloropropane	<5 ug/l	5 ug/l	
Bromodichloromethane	<5 ug/l	5 ug/l	
2-Chloroethylvinyl ether	<10 ug/l	10 ug/l	
cis-1,3-Dichloropropene	<5 ug/l	5 ug/l	
Toluene	11 ug/l	5 ug/l	
trans-1,3-Dichloropropeme	<5 ug/l	5 ug/l	
1,1,2-Trichloroethane	<5 ug/l	5 ug/l	
Tetrachloroethene	<5 ug/l	5 ug/l	
Dibromochloromethane	<5 ug/l	5 ug/l	
Chlorobenzene	<5 ug/l	5 ug/l	
Ethylbenzene	16 ug/l	5 ug/l	
Xylenes (Total)	160 ug/l	5 ug/l	
Bromoform	<5 ug/l	5 ug/l	
1,1,2,2-Tetrachloroethane	<5 ug/l	5 ug/l	





The Quality Solution

CLIENT:

J.M. Hontgomery Engineers

4525 So. Wasatch #200

Salt Lake City, UT 84124-

Phone:

801-272-1900 801-272-0430 (FAX)

ATTN:

Mr. David Fulton

Project: UST Site 870 2208.0402

Date Samples Rec'd: 10/20/92

MSAI Group No.:

9132

Sample Matrix: Aqueous Report Date:

10/22/92

P.O. Number:

LAB SAMPLE NO. DATE

SAMP SAMPLE DESCRIPTION

TIME

35281 10/19/92 1700 CPT-10

ANALYSES PERFORMED

RESULT

PP Volatiles 8240 GCMS See Attach ---

Douglas W. Later, Ph.D.

Glénn A. Sorensen, B.S.

Manager, Technical Operations



HAFB UST

The Quality Solution

ANALYSIS DATE:

LAB NO: 3135 James M. Montgomery Engineers CLIENT: 665S GROUP NO: 4525 South Wasatch Blvd. 12/18/92 DATE SAMPLED: Salt Lake City, UT 84124 1145 TIME SAMPLED: 12/18/92 DATE RECEIVED: Mr. Robert Glascot ATTN: DATE REPORTED: 01/11/93 DISPOSAL DATE: 02/10/93 **CPT-14** SAMPLE ID: 01/01/93

ANALYSIS:

PROJECT:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
COMPOUNDS Chloromethane Vinyl Chloride Bromomethane Chloroethane Trichlorofluoromethane Acrolein 1,1-Dichloroethene Methylene Chloride Acrylonitrile 1,1-Dichloroethane 1,2-Dichloroethane 1,1-Trichloroethane Carbon Tetrachloride Benzene 1,2-Dichloroethane Trichloroethene 1,2-Dichloropropane Bromodichloromethane 2-Chloroethylvinyl ether cis-1,3-Dichloropropene Toluene trans-1,3-Dichloropropene 1,1,2-Trichloroethane Tetrachloroethene Dibromochloromethane Chlorobenzene	<pre> < 500,000 ug/l < 500,000 ug/l < 500,000 ug/l < 500,000 ug/l < 250,000 ug/l</pre>	500,000 ug/l 500,000 ug/l 500,000 ug/l 500,000 ug/l 250,000 ug/l
Ethylbenzene Xylenes (Total)	1,400,000 ug/l 13,000,000 ug/l	/ _



James M. Montgomery Engineers 4525 South Wasatch Blvd., Suite 200

Salt Lake City, UT 84124 Telephone: (801) 272-1900 Facsimile: (801) 272-0403

Sample Number: 0003135 Sample Set: 000665S Date Reported: 6 JAN 1993 Date Received: 18 DEC 1992 Disposal Date: 2 FEB 1993

Attention: Project:

Robert Glascot **HAFB UST**

Case Number:

Purchase Order: 2208.0580

Customer Number: CPT-14 Date Sampled:

18 DEC 1992

Matrix:

Combustible Liquids

Containers:

2

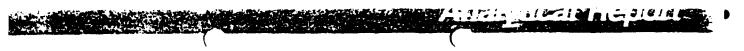
	Catalog			Dry	Reporting
Analysis	Number	Method	Result	Result	Units
Priority Pullutant Volatile Organics	01177	EPA SW-846 8240	See Attached		

I Analysis for GC/MS

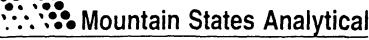
Reviewed and approved by John Hayes, B.S. Supervisor, GCMS Group

1 Analysis for Sample Number 0003135









J.M. Montgomery Engineers CLIENT: 4525 So. Wasatch #200

Mr. Robert Glascot

Salt Lake City, UT 84124-

SAMPLE SET NO: 000297S DATE SAMPLED: TIME SAMPLED:

SAMPLE NO:

0001530

11/24/92

11/25/92 DATE RECEIVED: DATE REPORTED: 12/10/92 DISPOSAL DATE: 01/09/93

SAMPLE ID: CPT-40

ATTN:

ANALYSIS: Volatiles - Water Matrix [EPA 601/602] (Capillary)

LIMIT OF RESULT **OUANTITATION** COMPOUND(s) 2.0 ug/l 2.0 ug/l Chloromethane 2.0 ug/l 2.0 ug/lVinyl Chloride 2.0 ug/l2.0 ug/l Bromomethane < $2.0 \, \text{ug/l}$ 2.0 ug/l Chloroethane < $2.0 \, \text{ug/l}$ $2.0 \, \text{ug/l}$ Fluorotrichloromethane < 1,1-Dichloroethene 1.0 ug/l
 1.0 ug/l < 1.0 ug/l $1.0 \, \text{ug/l}$ 1.0 ug/lDichloromethane 1.0 ug/l 1.0 ug/l trans-1,2-Dichloroethene 1,1-Dichloroethane 1.0 ug/l Chlcroform 1.0 ug/l 1,1,1-Trichloroethane 1.0 ug/l Carbon Tetrachloride 1.0 ug/l Benzene 1.0 ug/l $1.0 \, \text{ug/l}$ < 1,2-Dichloroethane 1.0 ug/l $1.0 \, ug/l$ Trichloroethene (TCE) < 1.0 ug/l 1,2-Dichloropropane < 1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/lBromodichloromethane cis-1,3-Dichloropropene 1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l trans-1,3-Dichloropropene 1.0 ug/l < < 1.0 ug/lToluene 1.0 ug/l Tetrachloroethene (PCE) < 1.0 ug/l Chlorodibromomethane 1.0 ug/l 1.0 ug/lChlorobenzene < 1.0 ug/l 1.0 ug/l < Ethylbenzene 2.0 ug/l $2.0 \, \text{ug/l}$ < Bromoform m,p-Xylene < 1.0 ug/l1.0 ug/l1.0 ug/l o-Xylene/Styrene* 1.0 ug/l





The Quality Solution

0001530 J.M. Montgomery Engineers LAB NO: CLIENT: GROUP NO: 000297S 4525 So. Wasatch #200 DATE SAMPLED: Salt Lake City, UT 84124-

11/24/92 TIME SAMPLED: 1345

DATE RECEIVED: 11/25/92 Mr. Robert Glascot ATTN: 12/10/92 DATE REPORTED:

DISPOSAL DATE: 01/09/93 SAMPLE ID: CPT-40

-Page 2-

COMPOUND(s)	FIN	AL RESULT	LIMIT OF QUANTITATION
1,1,2,2-Tetrachloroethane 1,1,2-Trichloroethane	< <	1.0 ug/l 1.0 ug/l	1.0 ug/l 1.0 ug/l
1,2-Dichlorobenzene 1,3-Dichlorobenzene 1,4-Dichlorobenzene	< <	1.0 ug/l 1.0 ug/l 1.0 ug/l	1.0 ug/l 1.0 ug/l 1.0 ug/l

Date Analyzed: 12/02/92

*These compounds coelute under the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

Kenneth A. Roberts, B.S.

GC Group Leader



CLIENT:

J.M. Montgomery Engineers

4525 So Wasatch #200

Salt Lake City, UT 84124-

Mr. Robert Glascot

SAMPLE ID: CPT-42

SAMPLE NO: 0001531

SAMPLE SET NO: 000297S

DATE SAMPLED: 11/24/92

137-12/25100- 3141-41419

TIME SAMPLED: 1455 11/25/92 DATE RECEIVED:

DATE REPORTED: 12/09/92

DISPOSAL DATE: 01/08/93

Gasoline Contamination in Water (BTEX) [EPA 602] ANALYSIS:

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Benzene	<	1.0 ug/l	1.0 ug/l
Toluene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene	<	1.0 ug/l	1.0 ug/l
m,p-Xylene	<	1.0 ug/l	1.0 ug/l
o-Xylene/Styrene*	<	1.0 ug/l	1.0 ug/l
Naphthalene	<	1.0 ug/l	1.0 ug/l

Date Analyzed: 12/03/92

*These compounds coelute under the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

Kenneth A. Roberts, B.S.

GC Group Leader





James M. Montgomery Engineers 4525 South Wasatch Blvd., Suite 200 Salt Lake City, UT 84124

Telephone: (801) 272-1900 Facsimile: (801) 272-0403

Attention: Project:

Robert Glascot HAFB USTs

Case Number:

VOCs/BTEXN

Purchase Order: 2208.0585

Sample Number: Sample Set:

0001532 000297S

Date Reported: Date Received:

10 DEC 1992 25 NOV 1992

Disposal Date:

8 JAN 1993

Customer Number: CPT-43

Date Sampled:

24 NOV 1992

Matrix:

Water/Waste Water

Containers:

Dry

Result

Catalog Number Analysis

04264

EPA 602 SW-846

Method

Result See Attached Reporting Ùnits

Btex & Naphthalene

5030/8020

I Analysis for GC

Reviewed and approved by Kenneth Roberts, B.S. GC Group Leader

1 Analysis for Sample Number 0001532





The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 So Wasatch Dr. #200

Salt Lake City, UT 84124-

Mr. Robert Glascot

SAMPLE ID: CPT-42

. ②

ATTN:

SAMPLE NO: 0001634

SAMPLE SET NO: 000322S 11/30/92 DATE SAMPLED:

TIME SAMPLED: 1350 12/01/92 DATE RECEIVED:

DATE REPORTED: 12/10/92 DISPOSAL DATE: 01/09/93

ANALYSIS: Gasoline Contamination in Water (BTEX) [EPA 602]

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Benzene	<	1.0 ug/l	1.0 ug/l
Toluene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene	<	1.0 ug/l	1.0 ug/l
m,p-Xylene	<	1.0 ug/l	1.0 ug/l
o-Xylene/Styrene*	<	1.0 ug/l	1.0 ug/l
-Naphthalene	<	1.0 ug/l	1.0 ug/l
Toluene Ethylbenzene m,p-Xylene o-Xylene/Styrene*	< < <	1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l	1.0 ug/l 1.0 ug/l 1.0 ug/l 1.0 ug/l

Date Analyzed: 12/03/92

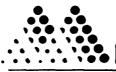
*These compounds coelute under the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

Kenneth A. Roberts, B.S.

GC Group Leader





The Quality Solution

James M. Montgomery Engineers 4525 South Wasatch Blvd., Suite 200

Salt Lake City, UT 84124 Telephone: (801) 272-1900 Facsimile: (801) 272-0403

Sample Number:

0001634 000322S

Sample Set: Date Reported: Date Received:

Disposal Date:

14 DEC 1992

1 DEC 1992 18 JAN 1993

Attention:

Robert Glascot

Project: Case Number: Hill AFB BTEXN

Purchase Order: 2208.0585

Customer Number: CPT-42

Date Sampled:

30 NOV 1992

Matrix:

Wastewater

Containers:

2

Reporting Units

Analysis

Catalog Number

Method

Result

Dry Result

Btex & Naphthalene

04264

EPA SW-846 5030/ 8020

See Attached

1 Analysis for GC

Reviewed and approved by Kenneth Roberts, B.S. GC Group Leader

1 Analysis for Sample Number 0001634





J.M. Montgomery Engineers

4525 So Wasatch #200

Salt Lake City, UT 84124-

SAMPLE SET NO: 0002975 DATE SAMPLED: 11/24/92 TIME SAMPLED:

1600

ATTN:

Mr. Robert Glascot

DATE RECEIVED: DATE REPORTED:

SAMPLE NO:

11/25/92 12/09/92

0001532

SAMPLE ID: CPT-43

DISPOSAL DATE:

01/08/93

ANALYSIS:

Gasoline Contamination in Water (BTEX) [EPA 602]

ON
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/1
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/1
/1
/1

Date Analyzed: 12/03/92

*These compounds coelute under the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

Kenneth A. Roberts, B.S.

GC Group Leader

CHAIN OF CUSTODY RECORD/LAB WORK REQUEST

Chain of Custody Number Cooler Number Lot Control ID Page Air Bill No.

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MONTGOMERY WATSON, INC.

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			1				1					-						2 Unbroken on Outer	
' Matrix:	WG - Ground Water	DC - Drum Solids		² Sampling Technique:	Ing Tea	hnla			S	ECIA!	L INS	TRUC	TIONS	(l.e. n	SPECIAL INSTRUCTIONS (I.e. metale list)	ř.,		AN N	
SO- Soil		LD. Drum Liquids		Composite=C	site=C	• •		とせ): k :	72	147	- -\$	ユ	ر ح	A Nile: Mess: the to tap the detection	オジャ	25	3 Present on Sample	

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	RellAquisheid by					
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DC - Drum Solids LD- Drum Lquids EP/TCLP Leachate	Date	11/27/11				,
WG - Ground Water D LF - Product AA - Air SW - Wipe	Received by	Harring (Union	/			
Matrix: SO-Soil SE-Sediment WS-Surface Water	Relinquished by	THE WILL	S.			

þ





CLIENT: J.M. Montgomery Engineers

4525 So Wasatch Dr. #200 Salt Lake City, UT 84124SAMPLE NO: 0001635 SAMPLE SET NO: 000322S DATE SAMPLED: 11/30/92

ATTN: Mr. Robert Glascot

TIME SAMPLED: 1410
DATE RECEIVED: 12/01/92
DATE REPORTED: 12/10/92

SAMPLE ID: CPT-43

DISPOSAL DATE: 01/09/93

ANALYSIS: Gasoline Contamination in Water (BTEX) [EPA 602]

COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Benzene	<	1.0 ug/l	1.0 ug/l
Toluene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene	<	1.0 ug/l	1.0 ug/l
m,p-Xylene	<	1.0 ug/l	1.0 ug/l
o-Xylene/Styrene*	<	1.0 ug/l	1.0 ug/l
Naphthalene	<	1.0 ug/l	1.0 ug/l

Date Analyzed: 12/03/92

*These compounds coelute under the conditions used. The result represents the total amount for these compounds.

Respectfully submitted,

Kenneth A. Roberts, B.S.

GC Group Leader





James M. Montgomery Engineers 4525 South Wasatch Blvd., Suite 200

Salt Lake City, UT 84124 Telephone: (801) 272-1900 Facsimile: (801) 272-0403 Sample Number:

0001635 000322S

Sample Set:
Date Reported:
Date Received:

14 DEC 1992 1 DEC 1992

Disposal Date:

18 JAN 1993

Attention:

Robert Glascot

Project: Case Number: Hill AFB

Case Number: BTEXN
Purchase Order: 2208.0585

Customer Number: CPT-43

Date Sampled:

30 NOV 1992

Matrix: Containers:

Wastewater

	Ca	talog
Analysis	Nu	mber

04264

Method

Result

Dry Reporting Result Units

Btex & Naphthalene

EPA SW-846 5030/ 8020 See Attached

1 Analysis for GC

Reviewed and approved by Kenneth Roberts, B.S. GC Group Leader

1 Analysis for Sample Number 0001635



555 East Walnut Street PO Box 7009 Pasadena, Calkonna 91109-7009 (818) 796-9141

Sample # 920810001 Sample 10 CPI-7
Sample Type Water Sampled 07-aug-1992 Received 08-aug-1992 Reported 14-aug-1992

Volatile Organics HSL

(ML/SW 8240

84214 Hill Air Force Base/JMM-SLC 4525 Wasatch Blvd Salt Lake City , UT ATTN: Dave Fulton

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Laboratory Report

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Parameter	Units	Result	XRec Conc.	Oitution	Det.Limit	Prepared	8	Anal yzed	By
1,1,2-Trichloroethane (1,1,2-T)/ 5 n	2		1000	200			13- aug- 1992) }
1,1-Dichloroethylene (1,10CE)		2		1000	200			13-aug-1992	jkc
1,1-Dichloroethane	1/64	2		1000	200			13-aug-1992	<u>ب</u>
		2		1000	200			13-aug-1992	jkc
	1/80	2		1000	200			13-aug-1992	jhc
	J/gu	9		1000	500			13-809-1992	jhc
	1/60	2		1000	200			13-aug-1992	jhc
(p-0CB)	1/60	9		1000	200			13 - aug - 1992	jłc
2-Butanone (NEK)	7/85	2		1000	10000			13-aug-1992	jłc
her	1/60	ON.		1000	1000			13-aug-1992	jt
2-Hexanone	1/61			1000	10000			13-aug-1992	ji S
entanone (MIBK)	J/6n	9	٠	1000	1000			13-aug-1992	jhc
Acetone Acetone Company of the Compa	1/60	2		1000	10000			13- aug- 1992	jhc
Acrolein	1/6n	9		1000	1000			13-aug-1992	jħc
Acrylonitrile	1/6n	A		1000	1000			13-aug-1992	jhc
Benzene)/6n	QN	-	1000	200			13-aug-1992	jhc
cis-1,2-Dichloroethene)/Bn	9		1000	200			13-aug-1992	jhc
Chlorobenzene	1/60	9		1000	200			13-aug-1992	jhc
cis-1,3-Dichlaropropene	1/60	9		1000	200			13-aug-1992	jþc
Bromoform	1/60	9		1000	200			13-aug-1992	jtc
Chloroform (Trichloromethene)	/g/	2		1000	500			13-aug-1992	jhc
Chloroethane	J/gu	9		1000	1000			13-aug-1992	jłc
Carbon disulfide	1/gn	9		1000	200			13-aug-1992	٠ <u>١</u>
ride	ug/l	9		1000	200			13-aug-1992	jhc
Dibromochlaromethene	1/60	2		1000	200			13-aug-1992	jħc
Dichlorobromomethane	ng/f	9		1000	200			13-aug-1902	jhe
Ethyl benzena	1/61	1800		1000	500			13-BUN-1992	<u>کر</u>
Methyl Bromide	J/gu	9		1000	1000			13-aug-1992	jhc
Nethyl Chloride)/gu	오		1000	1000			13-aug-1992	jhc

Report #: 2253

ABORATORIES

555 East Walnut Street, PO Box 7009 Pasadena, Caldonia 91109-7009 (818) 796-9141

Sampled <u>07-aug-1992</u> Received <u>08-aug-1992</u> Reported 14-aug-1992 Project VOA Sample # 920810001 Sample 1D CPI-7 Sample Type Water

Volatile Organics HSL

(ML/SW 8240

Hill Air Force Base/JMM-SLC

Laboratory Report

4525 Wasatch Blvd

84214 Salt Lake City , UT ATTN: Dave Fulton

	Ilajts	Result	%Rec Conc.	Dilution	Det.Limit	Prepared	8	Analyzed	8,	
Parameter		2		1000	3000			13-aug-1992	jhc	
Nethylene Chloride	\/B	0097		1000	200			13-aug-1992	j	
m, p-Xylenes	7 9	1000		1000	200			13-aug-1992	<u>ج</u>	
0-XV; ene %		, Q		1000	200			13-aug-1992	jhc	
1,1,2,<-letrachioroethane		9		1000	200			13-aug-1992	흱	
retrachioroginylend (rut)			tr.	1000	200			13-aug-1992	jhc	
Styrene		9		1000	\$00			13-aug-1992	έ	
trans-1, Z-D) chioroethane				1000	200			13-aug-1992	jhc	
1,1,1-Irichloroethane) <u>\$</u>		1000	200			13-aug-1992	jhc	
Trichloroethylene (105)) }		1000	1000			13-aug-1992	jhc	
Trichlorofluoromethane	150	9		1000	200			13-aug-1992	ž	
Lians . 1 Substitution to the substitution of	8	Q		1000	10000			13-aug-1992	jhc	
Tetranydroturan Tetrang)/6n	OK.		1000	200			13-aug-1992) <u>H</u> C	
		2		1000	1000			13-aug-1992	ğ	
Vinyi Acetate	3.5	9		1000	10000			13-aug-1992	jhc	

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Report #: 2253

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CLIENT: J.M. Montgomery Engineers

4525 S. Wasatch #200

Salt Lake City, UT 84124

ATTN: Mr. David Fulton

SAMPLE ID: CPT-7

LAB NO: 34822 GROUP NO: 8810

09/30/92

DATE SAMPLED: TIME SAMPLED: 1000

DATE RECEIVED: 10/02/92

DATE REPORTED: 10/21/92

DISPOSAL DATE: 11/20/92

ANALYSIS DATE: 10/09/92

ANALYSIS:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Chloromethane	* 71 ug/l	50 ug/l
Vinyl Chloride	<500 ug/l	500 ug/l
Bromomethane	<500 ug/l	500 ug/l
Chloroethane	<500 ug/l	500 ug/l
Trichlorofluoromethane	<250 ug/l	250 ug/l
Acrolein	<5,00ug/l	5,000 ug/l
1,1-Dichloroethene	<250 ug/l	250 ug/l
Methylene Chloride	<250 ug/l	250 ug/l
Acrylonitrile	<5,00ug/l	5,000 ug/l
1,1-Dichloroethane	<250 ug/l	250 ug/l
1,2-Dichloroethene (total)	<250 ug/l	250 ug/l
Chloroform	<250 ug/l	250 ug/l
1,1,1-Trichloroethane	<250 ug/l	250 ug/l
Carbon Tetrachloride	<250 ug/l	250 ug/l
Benzene	680 ug/l	250 ug/l
1,2-Dichloroethane	<250 ug/l	250 ug/l
Trichloroethene	<250 ug/l	250 ug/l
1,2-Dichloropropane	<250 ug/l	250 ug/l
Bromodichloromethane	<250 ug/l	250 ug/l
2-Chloroethylvinyl ether	<500 ug/l	500 ug/l
cis-1,3-Dichloropropene	<250 ug/l	250 ug/l
Toluene	* 34 ug/l J	50 ug/l
trans-1,3-Dichloropropene	<250 ug/l	250 ug/l
1,1,2-Trichloroethane	<250 ug/l	250 ug/l
Tetrachloroethene	* <50 ug/l	50 ug/l
Dibromochloromethane	<250 ug/l	250 ug/l
Chlorobenzene	<250 ug/l	250 ug/l
Ethylbenzene	1,400ug/l	250 ug/l
Xylenes (Total)	5,700ug/l	250 ug/l

J - estimated value

-Continued-



The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 So. Wasatch #200

Salt Lake City, UT 84124-

801-272-1900 801-272-0430 (FAX) Phone:

ATTN: Mr. David Fulton Project: HAFB UST Site 870

Date Samples Rec'd: 10/02/92

MSAI Group No.: 8810 Sample Matrix: Aqueous Report Date: 10/20/92

P.O. Number: 2208.0402

	SAMPLE DATE	SAMP TIME	SAMPLE DESCRIPTION	AN	alyses pere	PORME)		RESU	ЛŢ
34822	09/30/92	1000	CPT-7	PP	Volatiles	8240	GCMS	See	Attach	
34823	09/30/92	1320	T-870-5-MW-U-92-HF	PP	Volatiles	8240	GCMS	See	Attach	
34824	09/30/92	1100	T-870-27-MW-U-92-HF	PP	Volatiles	8240	GCMS	See	Attach	
34825	09/30/92	1325	T-870-11-MW-U-92-HF	PP	Volatiles	8240	GCMS	See	Attach	
34826	10/01/92	1200	T-870-12-MW-U-92-HF	PP	Volatiles	8240	GCHS	See	Attach	
34827	10/01/92	1500	T-870-10-MW-U-92-HF	PP	Volatiles	8240	GCMS	See	Attach	
34828	10/01/92	0	Trip Blank	PP	Volatiles	8240	GCMS	See	Attach	

Respectfully submitted

Douglas W. Later, Ph.D. Laboratory Director

Glenn A. Sorensen, B.S.

Manager, Technical Operations

CLIENT: James M. Montgomery PROJECT NO. : 92-1016

4525 S. Wasatch Blvd.

SAMPLE NO. : 143 REPORT DATE : 10/09/92 SLC, Utah 84124

REVIEWED BY : RAK Attn: David A. Fulton : 1 OF 2 PAGE

CLIENT ID No. : None AUTHORIZED BY : DAF CLIENT P.O. : None SAMPLE MATRIX : Ground Water

SAMPLE DATE : 08/14/92 SUBMITTAL DATE: 08/14/92 ANALYSIS DATE : 08/14/92 SAMPLED BY : NKT/RAK SAMPLE SOURCE : GWS-01 : NKT ANALYST

Organic Monitoring-Drinking Water Volatiles Full Suite

Sample Analysis			
Parameter	Result	Unit	Detection Level
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotehane Chloroform Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromoethane (EDB) 1,2-Dibromoethane Dibromomethane 1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para)	0.195 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
Dichlorodifluoromethane 1,1-Dichloroethane 1,2-Dichloroethane	N/A N/A N/A	mg/L mg/L mg/L	0.005 0.005 0.005

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 143

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

SAMPLE SOURCE: GWS-01 PAGE : 2 OF 2

Sample Analysis			
Parameter	Result	Unit	Detection Level
cis 1,2-Dichloroethene	N/A	mg/L	0.005
trans 1,2-Dichloroethene	N/A	mg/L	0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	N/A	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
cis 1,3-Dichloropropene	N/A	mg/L	0.005
trans 1,3-Dichloropropene .	N/A	mg/L	0.005
Ethylbenzene	0.072	mg/L	0.005
Isoproylbenzene	N/A	mg/L	0.005
4-Isopropyltoluene	N/A	mg/L	0.005
Dichloromethane	N/A	mg/L	0.005
Napthalene	N/A	mg/L	0.005 0.005
Propylbenzene	N/A	mg/L	0.005
Styrene	N/A N/A	mg/L	0.005
1,1,2,2-Tetrachloroethane	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethene	N/A	mg/11	0.005
(Tetrachloroethylene)	< 0.005	mg/L	0.005
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005
Toluene	0.946	mg/L	0.005
1,2,3-Trichlorobenzene	N/A	mg/L	0.005
1,2,4-Trichlorobenzene	N/A	mg/L	0.005
1,1,1-Trichloroethane	N/A	mg/L	0.005
1,1,2-Trichloroethane	N/A	mg/L	0.005
Trichloroethene (TCE)	N/A	mg/L	0.005
Fluorotrichloromethane	N/A	mg/L	0.005
1,2,3-Trichloropropane	N/A	mg/L	0.005
1,2,4-Trimethylbenzene	N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
p-m-Xylene	0.062	mg/L	0.005
o-Xylene	0.027	mg/L	0.005
			L

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 107

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF

SAMPLE MATRIX : Ground Water CLIENT P.O. : None SAMPLED BY : JMM Personnel SAMPLE DATE : 08/06

SAMPLED BY : JMM Personnel SAMPLE DATE : 08/06/92 SAMPLE SOURCE : MW-03 SUBMITTAL DATE: 08/12/92

ANALYST : NKT ANALYSIS DATE : 08/12/92

Organic Monitoring-Drinking Water Volatiles Full Suite

Sample Analysis			
Parameter	Result	Unit	Detection Level
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chloroform Chloroform Chloromethane 2-Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromo-3-chloropropane Dibromomethane Dibromomethane 1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta)	12.179	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Dichloroethane	N/A N/A N/A	mg/L mg/L mg/L	0.005 0.005 0.005
1,2-Dichloroethane	N/A	mg/L	0.005

James M. Montgomery 4525 S. Wasatch Blvd. CLIENT: PROJECT NO. : 92-1016

SAMPLE NO. : 107 REPORT DATE : 10/09/92 SLC, Utah 84124

REVIEWED BY : RAK SAMPLE SOURCE: MW-03 : 2 OF 2 PAGE

Sample Analysis			
Paramet: r	Result	Unit	Detection Level
cis 1,2-Dichloroethene	N/A	mg/L	0.005
trans 1,2-Dichloroethene	N/A	mg/L	0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	n/a	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
cis 1,3-Dichloropropene	N/A	mg/L	0.005
trans 1,3-Dichloropropene .	N/A	mg/L	0.005
Ethylbenzene	< 0.005	mg/L	0.005
Hexachlorobutadiene	N/A	mg/L	0.005
Isoproylbenzene	N/A	mg/L	0.005
4-Isopropyltoluene	N/A	mg/L	0.005
Dichloromethane	N/A	mg/L	0.005
Napthalene	N/A	mg/L	0.005
Propylbenzene	N/A	mg/L	0.005
Styrene	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethene		1	
(Tetrachloroethylene)	2.722	mg/L	0.005
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005
Toluene	6.728	mg/L	0.005
1,2,3-Trichlorobenzene	N/A	mg/L	0.005
1,2,4-Trichlorobenzene	N/A	mg/L	0.005
1,1,1-Trichloroethane	N/A	mg/L	0.005
1,1,2-Trichloroethane	N/A	mg/L	0.005
Trichloroethene (TCE)	N/A	mg/L	0.005
Fluorotrichloromethane	Ņ/A	mg/L	0.005
1,2,3-Trichloropropane	N/A	mg/L	0.005
1,2,4-Trimethylbenzene	N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
p-m-Xylene	4.300	mg/L	0.005
o-Xylene	3.369	mg/L	0.005
L			



34827 LAB NO: J.M. Montgomery Engineers GROUP NO: 8810 4525 S Wasatch #200 10/01/92 DATE SAMPLED: Salt Lake City, UT 84124 TIME SAMPLED: 1500 DATE RECEIVED: 10/02/92 Mr. David Fulton ATTN: DATE REPORTED: 10/16/92 DISPOSAL DATE: 11/15/92 T-870-10-MW-U-92-HF SAMPLE ID: ANALYSIS DATE: 10/12/92

ANALYSIS:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Chloromethane	<10 ug/l	10 ug/l
Vinyl Chloride	<10 ug/l	10 ug/l
Bromomethane	<10 ug/l	10 ug/l
Chloroethane	<10 ug/l	10 ug/l
Trichlorofluoromethane	<5 ug/l	5 ug/l
Acrolein	<100 ug/l	100 ug/l
1,1-Dichloroethene	<5 ug/l	5 ug/l
Methylene Chloride	<5 ug/l	5 ug/l
Acrylonitrile	<100 ug/l	100 ug/l
1,1-Dichloroethane	<5 ug/l	5 ug/l
1,2-Dichloroethene (total)	<5 ug/l	5 ug/l
Chloroform	<5 ug/l	5 ug/l
1,1,1-Trichloroethane	<5 ug/l	5 ug/l
Carbon Tetrachloride	<5 ug/l	5 ug/l
Benzene	<5 ug/l	5 ug/l
1,2-Dichloroethane	<5 ug/l	5 ug/l
Trichloroethene	<5 ug/l	5 ug/l
1,2-Dichloropropane	<5 ug/l	5 ug/l
Bromodichloromethane	<5 ug/l	5 ug/l
2-Chloroethylvinyl ether	<10 ug/l	10 ug/l
cis-1,3-Dichloropropene	<5 ug/l	5 ug/l
Toluene	17 ug/l	5 ug/l
trans-1,3-Dichloropropene	<5 ug/l	5 ug/l
1,1,2-Trichloroethane	<5 ug/l	5 ug/l
Tetrachloroethene	<5 ug/l	5 ug/l
Dibromochloromethane	<5 ug/l	5 ug/l
Chlorobenzene	<5 ug/l	5 ug/l
Ethylbenzene	<5 ug/l	5 ug/l
Xylenes (Total)	110 ug/l	5 ug/l
Bromoform	<5 ug/l	5 ug/l
1,1,2,2-Tetrachloroethane	<5 ug/l	5 ug/l

Respectfully submitted,

John G. Hayes, B.S. Supervisor, GCMS Group





J.M. Montgomery Engineers CLIENT:

4525 S Wasatch #200

Salt Lake City, UT 84124

Mr. David Fulton ATTN:

SAMPLE ID:

T-870-(2-MW-U-92-HF

LAB NO:

34826 GROUP NO: 8810

DATE SAMPLED: 10/01/92

TIME SAMPLED: 1200 DATE RECEIVED: 10/02/92

DATE REPORTED: 10/16/92 DISPOSAL DATE: 11/15/92

ANALYSIS DATE: 10/12/92

ANALYSIS:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Chloromethane	<10 ug/l	10 ug/l
Vinyl Chloride	<10 ug/l	10 ug/l
Bromomethane	<10 ug/l	10 ug/l
Chloroethane	<10 ug/l	10 ug/l
Trichlorofluoromethane	<5 ug/l	5 ug/l
Acrolein	<100 ug/l	100 ug/l
1,1-Dichloroethene	<5 ug/l	5 ug/l
Methylene Chloride	11 ug/l	5 ug/l
Acrylonitrile	<100 ug/l	100 ug/l
1,1-Dichloroethane	<5 ug/l	5 ug/l
1,2-Dichloroethene (total)	<5 ug/l	5 ug/l
Chloroform	<5 ug/l	5 ug/l
1,1,1-Trichloroethane	<5 ug/1	5 ug/l
Carbon Tetrachloride	<5 ug/l	5 ug/l
Benzene	10 ug/l	5 ug/l
1,2-Dichloroethane	<5 ug/l	5 ug/l
Trichloroethene	<5 ug/l	5 ug/l
1,2-Dichloropropane	<5 ug/1	5 ug/l
Bromodichloromethane	<5 ug/l	5 ug/l
2-Chloroethylvinyl ether	<10 ug/l	10 ug/l
cis-1,3-Dichloropropene	<5 ug/l	5 ug/1
Toluene	<5 ug/l	5 ug/l
trans-1,3-Dichloropropene	<5 ug/l	5 ug/l
1,1,2-Trichloroethane	<5 ug/l	5 ug/l
Tetrachloroethene	<5 ug/l	5 ug/l
Dibromochloromethane	<5 ug/l	5 ug/l
Chlorobenzene	<5 ug/l	5 ug/l
Ethylbenzene	29 ug/l	5 ug/l
Xylenes (Total)	300 ug/l	5 ug/l
Bromoform	<5 ug/l	5 ug/l
1,1,2,2-Tetrachloroethane	<5 ug/l	5 ug/l

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Respectfully submitted,

hin all Hayes John G. Hayes, B.S. Supervisor, GCMS Group



The Quality Solution

CLIENT: J.M. Montgomery Engineers 4525 S. Wasatch #200

Salt Lake City, UT 84124

Mr. David Fulton ATTN:

T-870-11 (MW-U)92-HF SAMPLE ID:

34825 LAB NO:

GROUP NO: 8810 DATE SAMPLED: 09/30/92

1325 TIME SAMPLED: DATE RECEIVED: 10/02/92

DATE REPORTED: 10/14/92

DISPOSAL DATE: 11/13/92 ANALYSIS DATE: 10/09/92

ANALYSIS:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Chloromethane	<10 ug/l	10 ug/.l
Vinyl Chloride	<10 ug/l	10 ug/l
Bromomethane	<10 ug/l	10 ug/l
Chloroethane	<10 ug/l	10 ug/l
Trichlorofluoromethane	<5 ug/l	5 ug/l
Acrolein	<100 ug/l	100 ug/l
1,1-Dichloroethene	<5 ug/l	5 ug/l
Methylene Chloride	<5 ug/l	5 ug/l
Acrylonitrile	<100 ug/l	100 ug/l
1,1-Dichloroethane	<5 ug/l	5 ug/l
1,2-Dichloroethene (total)	<5 ug/l	5 ug/l
Chloroform	<5 ug/l	5 ug/l
1,1,1-Trichloroethane	<5 ug/l	5 ug/l
Carbon Tetrachloride	<5 ug/l	5 ug/l
Benzene	26 ug/l	5 ug/l
1.2-Dichloroethane	<5 ug/l	5 ug/l
Trichloroethene	<5 ug/l	5 ug/l
1.2-Dichloropropane	<5 ug/l	5 ug/l
Bromodichloromethane	<5 ug/l	5 ug/l
2-Chloroethylvinyl ether	<10 ug/l	10 ug/l
cis-1,3-Dichloropropene	<5 ug/l	5 ug/l
Toluene	33 ug/l	5 ug/l
trans-1,3-Dichloropropene	<5 ug/l	5 ug/l
1,1,2-Trichloroethane	<5 ug/l	5 ug/l
Tetrachloroethene	<5 ug/l	5 ug/l
Dibromochloromethane	<5 ug/l	5 ug/l
Chlorobenzene	<5 ug/l	5 ug/l
Ethylbenzene	21 ug/l	5 ug/l
Xylenes (Total)	180 ug/l	5 ug/l
Bromoform	<5 ug/l	5 ug/l
1,1,2,2-Tetrachloroethane	<5 ug/l	5 ug/l

Respectfully submitted,

John G. Hayes, B.S. Supervisor, GCMS Group



The Quality Solution

CLIENT: J.M. Montgomery Engineers

Mr. David Fulton

4525 S. Wasatch #200 Salt Lake City, UT 84124

LAB NO: 34824 GROUP NO: 8810

DATE SAMPLED: 09/30/92

TIME SAMPLED: 1100 DATE RECEIVED: 10/02/92

DATE REPORTED: 10/21/92

DISPOSAL DATE: 11/20/92 ANALYSIS DATE: 10/09/92

SAMPLE ID:

ANALYSIS:

ATTN:

T-870-27-MW-U-92-HF

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

-Page 2-

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Bromoform 1,1,2,2-Tetrachloroethane	<50 ug/l J 2 ug/l	50 ug/l 5 ug/l

J - Estimated Value

Comment: Due to the sample matrix and level of target compounds, dilution was required. The limits of quantation were raised accordingly. The compounds which are reported with "J" values were taken from the original 5.0 ml analysis.

Respectfully submitted,

John + A whoys

John G. Hayes, B.S. Supervisor, GCMS Group





34823 CLIENT: J.M. Montgomery Engineers LAB NO: 9810 GROUP NO: 4525 S. Wasatch #200 09/30/92 DATE SAMPLED: Salt Lake City, UT 84124 1320 TIME SAMPLED: 10/02/92 DATE RECEIVED: Mr. David Fulton ATTN: 10/21/92 DATE REPORTED: T-870-5-MW U-92-HF 11/20/92 DISPOSAL DATE: SAMPLE ID: ANALYSIS DATE: 10/09/92

ANALYSIS: Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
COMPOUNDS Chloromethane Vinyl Chloride Bromomethane Chloroethane Trichlorofluoromethane Acrolein 1,1-Dichloroethene Methylene Chloride Acrylonitrile 1,1-Dichloroethane 1,2-Dichloroethane 1,2-Trichloroethane		10 ug/l 100 ug/l 100 ug/l 100 ug/l 50 ug/l
Carbon Tetrachloride Benzene 1,2-Dichloroethane Trichloroethene 1,2-Dichloropropane Bromodichloromethane 2-Chloroethylvinyl ether cis-1,3-Dichloropropene Toluene trans-1,3-Dichloropropene 1,1,2-Trichloroethane Tetrachloroethene Dibromochloromethane Chlorobenzene Ethylbenzene Xylenes (Total)	<pre><50 ug/l 74 ug/l <50 ug/l <90 ug/l <90 ug/l </pre>	50 ug/l

J - Estimated Value

-Continued-



The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 S. Wasatch #200

Salt Lake City, UT 84124

Mr. David Fulton ATTN:

SAMPLE ID:

CPT-7

LAB NO: 34822 GROUP NO:

8810 DATE SAMPLED: 09/30/92

TIME SAMPLED: 1000

DATE RECEIVED: 10/02/92

DATE REPORTED: 10/21/92 DISPOSAL DATE: 11/20/92

ANALYSIS DATE:

10/09/92

ANALYSIS:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

-Page 2-

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Bromoform 1,1,2,2-Tetrachloroethane	<250 ug/l * <50 ug/l	250 ug/l 50 ug/l

Comment: Due to the sample matrix and level of target compounds, dilution was required. The limits of quantitation were raised accordingly. In an attempt to acheive lower detection limits for Tetrachloroethene, the sample was rerun at lower dilutions. A 5.0 ml portion could not be performed due to the excessive signal. A 1.0 ml aliquot was performed and Tetrachloroethene was not detected. The "*" compounds are from the 1.0 ml analysis. The 1.0 ml analysis was performed outside of holding time.

Respectfully submitted,

John G. Hayes, B.S. Supervisor, GCMS Group

lu H. Changs





The Quality Solution

34824 CLIENT: J.M. Montgomery Engineers LAB NO: 4525 S. Wasatch #200 GROUP NO: 8810 09/30/92 Salt Lake City, UT 94124 DATE SAMPLED: TIME SAMPLED: Mr. David Fulton DATE RECEIVED: 10/02/92 ATTN: DATE REPORTED: 10/21/92 T-870-27-MW-U-92-HF DISPOSAL DATE: 11/20/92 SAMPLE ID: ANALYSIS DATE: 10/09/92

ANALYSIS: Priority Pollutants by GCMS (Volatiles) Notation Definition

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Compounds Chloromethane Vinyl Chloride Bromomethane Chloroethane Trichlorofluoromethane Acrolein 1,1-Dichloroethene Methylene Chloride Acrylonitrile 1,1-Dichloroethane 1,2-Dichloroethane 1,2-Dichloroethane Carbon Tetrachloride Benzene 1,2-Dichloroethane Trichloroethane Trichloroethane Trichloroethane Trichloroethane Trichloroethane Trichloroethene 1,2-Dichloropropane Bromodichloromethane 2-Chloroethylvinyl ether cis-1,3-Dichloropropene Toluene trans-1,3-Dichloropropene 1,1,2-Trichloroethane Tetrachloroethene	RESULTS <100 ug/l <100 ug/l <100 ug/l <100 ug/l <50 ug/l	100 ug/l 100 ug/l 100 ug/l 100 ug/l 100 ug/l 50 ug/l 1,000 ug/l 50 ug/l
Dibromochloromethane Chlorobenzene Ethylbenzene Xylenes (Total)	<50 ug/l <50 ug/l 150 ug/l 890 ug/l	50 ug/l 50 ug/l 50 ug/l 50 ug/l

J - Estimated Value

-Continued-

Analylical Report



The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 S. Wasatch #200

Salt Lake City, UT 84124

Mr. David Fulton

SAMPLE ID:

T-870-5-MW-U-92-HF

LAB NO:

34823

GROUP NO: 8810

DATE SAMPLED: 09/30/92

1320 TIME SAMPLED:

10/02/92 DATE RECEIVED:

10/21/92 DATE REPORTED:

DISPOSAL DATE:

11/20/92

10/09/92 ANALYSIS DATE:

ANALYSIS:

ATTN:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

-Page 2-

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Bromoform 1.1.2.2-Tetrachloroethane	<50 ug/l <50 ug/l	50 ug/l 50 ug/l

Comment: Due to the matrix and level of target compounds in the sample, dilution was required. The limits of quantation were raised accordingly. The compounds which are reported with "J" values were taken from the original 5.0 ml analysis.

Respectfully submitted,

John G. Hayes, B.S. Supervisor, GCMS Group



The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 S Wasatch #200

Salt Lake City, UT 84124

Mr. Bob Glascok ATTN:

SAMPLE ID:

T-870;-MW-6;-U-92-HF

LAB NO:

GROUP NO: 7730

DATE SAMPLED:

TIME SAMPLED: DATE RECEIVED: 09/04/92

DATE REPORTED: 09/30/92

DISPOSAL DATE: 10/31/92

ANALYSIS DATE: 09/14/92

ANALYSIS:

TCL VOLATILES (SOW - 2/88)

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Chile was a base	<50 ug/l	50 ug/l
Chloromethane	<50 ug/1	50 ug/1
Vinyl Chloride	<50 ug/1	50 ug/l
Bromomethane	<50 ug/1	50 ug/l
Chloroethane	<25 ug/1	25 ug/l
1,1-Dichloroethene		100 ug/l
Acetone	<100 ug/l	25 ug/l
Carbon Disulfide	<25 ug/l <25 ug/l	25 ug/1 25 ug/1
Methylene Chloride		25 ug/1 25 ug/1
1,1-Dichloroethane	<25 ug/l	
Vinyl Acetate	<25 ug/l	25 ug/l
2-Butanone	<100 ug/l	100 ug/l 25 ug/l
1,2-Dichloroethene (total)	<25 ug/l	25 ug/l 25 ug/l
Chloroform	<25 ug/l <25 ug/l	25 ug/1
1,1,1-Trichloroethane		25 ug/l 25 ug/l
Carbon Tetrachloride	<25 ug/l	25 ug/1 25 ug/1
Benzene	<25 ug/l	25 ug/1 25 ug/1
1,2-Dichloroethane	<25 ug/l	25 ug/1 25 ug/1
Trichloroethene	<25 ug/l	25 ug/l 25 ug/l
1,2-Dichloropropane	<25 ug/l	25 ug/1 25 ug/1
Bromodichloromethane	<25 ug/l	25 ug/1 25 ug/1
cis-1,3-Dichloropropene	<25 ug/l	
4-Methyl-2-Pentanone	<50 ug/1	50 ug/l
Toluene	<25 ug/l	25 ug/l
trans-1,3-Dichloropropene	<25 ug/l	25 ug/l
1,1,2-Trichloroethane	<25 ug/l	25 ug/l
Tetrachloroethene	<25 ug/l	25 ug/l
2-Hexanone	<50 ug/l	50 ug/l
Dibromochloromethane	<25 ug/l	25 ug/l
Chlorobenzene	<25 ug/l	25 ug/l
Ethylbenzene	<25 ug/l	25 ug/l
Xylenes (total)	<25 ug/l	25 ug/l
Styrene	<25 ug/l	25 ug/l

-Continued-





The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 S Wasatch #200

Salt Lake City, UT 84124

ATTN: Mr. Bob Glascok

SAMPLE ID:

T-870-MW-6-U-92-HF

LAB NO: GROUP NO: 31657

7730

06/04/92 DATE SAMPLED:

1105

TIME SAMPLED:

DATE RECEIVED: 06/04/92

DATE REPORTED: 09/30/92

DISPOSAL DATE: 10/31/92

ANALYSIS DATE: 06/13/92

ANALYSIS:

TCL VOLATILES

- Page 2 -

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Bromoform 1.1.2.2-Tetrachloroethane	<25 ug/l <25 ug/l	25 ug/l 25 ug/l

Comment: Due to the sample matrix, dilution was required. Limits of quantitation were raised accordingly.

Respectfully submitted,

John G Hayes, B.S.

In D. Hayer

Supervisor, GCMS Group

Alegily 11 (Fall is (Folding)



The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 S Wasatch #200

Salt Lake City, UT 84124

ATTN: Mr. Robert Glascok

SAMPLE ID: T-870(MW-7)U-92-HF

LAB NO: 31786

GROUP NO: 7776
DATE SAMPLED: 09/07/92

TIME SAMPLED: 1440 DATE RECEIVED: 09/08/92

DATE REPORTED: 09/16/92 DISPOSAL DATE: 10/17/92

ANALYSIS DATE: 09/15/92

ANALYSIS: TCL VOLATILES (SOW - 2/88)

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Chloromethane	<10 ug/l	10 ug/l
Vinyl Chloride	<10 ug/l	10 ug/l
Bromomethane	<10 ug/l	10 ug/l
Chloroethane	<10 ug/l	10 ug/l
1,1-Dichloroethene	<5 ug/l	5 ug/l
Acetone	<20 ug/l	20 ug/l
Carbon Disulfide	<5 ug/l	5 ug/l
Methylene Chloride	<5 ug/l	5 ug/l
1,1-Dichloroethane	<5 ug/l	5 ug/l
Vinyl Acetate	<5 ug/l	5 ug/l
2-Butanone	<20 ug/l	20 ug/l
1,2-Dichloroethene (total)	<5 ug/l	5 ug/l
Chloroform	<5 ug/l	5 ug/l
1,1,1-Trichloroethane	<5 ug/l	5 ug/l
Carbon Tetrachloride	<5 ug/l	5 ug/l
Benzene	<5 ug/l	5 ug/l
1,2-Dichloroethane	<5 ug/l	5 ug/l
Trichloroethene	<5 ug/l	5 ug/l
1,2-Dichloropropane	<5 ug/l	5 ug/l
Bromodichloromethane	<5 ug/l	5 ug/l
cis-1,3-Dichloropropene	<5 ug/l	5 ug/l
4-Methyl-2-Pentanone	<10 ug/l	10 ug/l
Toluene	<5 ug/l	5 ug/l
trans-1,3-Dichloropropene	<5 ug/l	5 ug/l
1,1,2-Trichloroethane	<5 ug/l	5 ug/l
Tetrachloroethene	<5 ug/1	5 ug/l
2-Hexanone	<10 ug/1	10 ug/l
Dibromochloromethane	<5 ug/l	5 ug/l
Chlorobenzene	<5 ug/l	
Ethylbenzene	<5 ug/l	
Xylenes (total)	<5 ug/l	5 ug/l
Styrene	<5 ug/l	5 ug/l ·

-Continued-



Agalytical Report



Mountain States Analytical

The Quality Solution

CLIENT: J.M. Montgomery Engineers

4525 S Wasatch #200

Salt Lake City, UT 84124

Mr. Robert Glascok ATTN:

SAMPLE ID:

T-870-MW-7-U-92-HF

LAB NO: 31786

GROUP NO: 7776

DATE SAMPLED: 06/04/92

TIME SAMPLED: 1440

DATE RECFIVED: 06/04/92

DATE REPORTED: 09/16/92

DISPOSAL DATE: 10/17/92

ANALYSIS DATE: 06/13/92

ANALYSIS:

-

TCL VOLATILES

- Page 2 -

COMPOUNDS

Bromoform

1,1,2,2-Tetrachloroethane

FINAL RESULTS

QUANTITATION

LIMIT

<5 ug/l

5 ug/l

<5 ug/l

5 ug/l

Respectfully submitted,

John G Hayes, B.S.

Supervisor, GCMS Group

31781

7776



duy of MW-7?

The Quality Solution

CLIENT: J.M. Montgomery Engineers LAB NO: GROUP NO: 4525 S Wasatch #200 Salt Lake City, UT 84124 DATE SAMPLED: 09/07/92

TIME SAMPLED: DATE RECEIVED: 09/08/92 Mr. Robert Glascok ATTN:

DATE REPORTED: 09/16/92 T-870/-MW-27)-U-92-HF SAMPLE ID: DISPOSAL DATE: 10/17/92 ANALYSIS DATE: 09/15/92

TCL VOLATILES (SOW - 2/88) ANALYSIS:

COMPOUNDS	FINAL RESULTS	QUAN TITATION LIMIT
Compounds Chloromethane Vinyl Chloride Bromomethane Chloroethane 1,1-Dichloroethene Acetone Carbon Disulfide Methylene Chloride 1,1-Dichloroethane Vinyl Acetate 2-Butanone 1,2-Dichloroethene (total) Chloroform 1,1,1-Trichloroethane Carbon Tetrachloride Benzene 1,2-Dichloroethane Trichloroethene 1,2-Dichloroethane Trichloroethene 1,2-Dichloropropane Bromodichloromethane cis-1,3-Dichloropropene 4-Methyl-2-Pentanone Toluene	. —	-
trans-1,3-Dichloropropene 1,1,2-Trichloroethane	<5 ug/l <5 ug/l	5 ug/l 5 ug/l
Tetrachloroethene 2-Hexanone Dibromochloromethane Chlorobenzene Ethylbenzene	<5 ug/l <10 ug/l <5 ug/l <5 ug/l <5 ug/l	5 ug/l 10 ug/l 5 ug/l 5 ug/l 5 ug/l
Xylenes (total) Styrene	<5 ug/1 <5 ug/1	5 ug/l 5 ug/l

-Continued-



31781

7776



CLIENT: J.M. Montgomery Engineers

4525 S Wasatch #200

Salt Lake City, UT 84124

Mr. Robert Glascok ATTN:

ANALYSIS:

SAMPLE ID:

T-870-MW-27-U-92-HF

TCL VOLATILES

- Page 2 -

FINAL QUANTITATION COMPOUNDS RESULTS LIMIT Bromoform <5 ug/l 5 ug/l 1,1,2,2-Tetrachloroethane <5 ug/l 5 ug/l

Respectfully submitted,

LAB NO:

GROUP NO:

TIME SAMPLED:

DATE SAMPLED: 06/04/92

DATE RECEIVED: 06/04/92 DATE REPORTED: 09/16/92

DISPOSAL DATE: 10/17/92 ANALYSIS DATE: 06/13/92

John G Hayes, B.S.

Supervisor, GCMS Group

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 122

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY: RAK
AMPLE SOURCE: TWP-01 PAGE : 2 OF 2

SAMPLE SOURCE: TWP-01

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Sample	Analysis	· · · · · ·	
Parameter	Result	Unit	Detection Level
cis 1,2-Dichloroethene	N/A	mg/L	0.005
trans 1,2-Dichloroethene	N/A	mg/L	0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	N/A	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
cis 1,3-Dichloropropene	N/A	mg/L	0.005
trans 1,3-Dichloropropene .	N/A	mg/L	0.005
Ethylbenzene	0.085	mg/L	0.005
Hexachlorobutadiene	N/A	mg/L	0.005
Isoproylbenzene	N/A	mg/L	0.005
4-Isopropyltoluene	N/A	mg/L	0.005
Dichloromethane	N/A	mg/L	0.005
Napthalene	N/A	mg/L	0.005
Propylbenzene	N/A	mg/L	0.005
Styrene	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethene			
(Tetrachloroethylene)	0.795	mg/L	0.005
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005
Toluene	1.271	mg/L	0.005
1,2,3-Trichlorobenzene	N/A	mg/L	0.005
1,2,4-Trichlorobenzene	N/A	mg/L	0.005
1,1,1-Trichloroethane	N/A	mg/L	0.005
1,1,2-Trichloroethane	N/A	mg/L	0.005
Trichloroethene (TCE)	N/A	mg/L	0.005
Fluorotrichloromethane	N/A	mg/L	0.005
1,2,3-Trichloropropane	N/A	mg/L	0.005
1,2,4-Trimethylbenzene	N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
p-m-Xylene	0.141	mg/L	0.005
o-Xylene	0.032	mg/L	0.005

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 122

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLED BY : JMM Personnel SAMPLE DATE : 08/12/92

SAMPLE SOURCE: TWP-01 SUBMITTAL DATE: 08/12/92

ANALYST : NKT ANALYSIS DATE : 08/12/92

Organic Monitoring-Drinking Water Volatiles Full Suite

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 16

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Soil Gas CLIENT P.O. : None

SAMPLED BY: NKT/RAK SAMPLE DATE: 08/05/92 SAMPLE SOURCE: SGS-01 SUBMITTAL DATE: 08/05/92 ALYST: NKT ANALYSIS DATE: 08/05/92

Organic Monitoring-Drinking Water Volatiles Full Suite

Sample	Analysis		
Parameter	Result	Unit	Detection Level
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotehane Chloroform Chloromethane 2-Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromoethane Dibromomethane 1,2-Dichlorobenzene (meta) 1,4-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Dichloroethane	0.161 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 16

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY: RAK
SAMPLE SOURCE: SGS-01 PAGE : 2 OF 2

Sample	Analysis		
Parameter	Result	Unit	Detection Level
cis 1,2-Dichloroethene	N/A	mg/L	0.005
trans 1,2-Dichloroethene	N/A	mg/L	0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	N/A	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
	N/A	mg/L	0.005
	N/A	mg/L	0.005
	0.046	mg/L	0.005
Hexachlorobutadiene Isoproylbenzene	N/A	mg/L	0.005
	N/A	mg/L	0.005
	N/A	mg/L	0.005
Dichloromethane	N/A N/A N/A N/A	mg/L mg/L mg/L	0.005 0.005 0.005 0.005
1,1,2,2-Tetrachloroethane . 1,1,2,2-Tetrachloroethene (Tetrachloroethylene)	N/A < 0.005	mg/L	0.005
1,1,1,2-Tetrachloroethane Toluene	N/A	mg/L	0.005
	12.645	mg/L	0.005
	N/A	mg/L	0.005
	N/A	mg/L	0.005
1,1,1-Trichloroethane	N/A	mg/L	0.005
1,1,2-Trichloroethane	N/A	mg/L	0.005
Trichloroethene (TCE)	N/A	mg/L	0.005
Fluorotrichloromethane	N/A	mg/L	0.005
1,2,3-Trichloropropane	N/A	mg/L	0.005
1,2,4-Trimethylbenzene	N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
	< 0.005	mg/L	0.005
	0.295	mg/L	0.005



555 East Wahul Street, P.O. Box 7009 Pasadena, California 91109-7009 (818) 796-9141

Sampled 07-aug-1992 Received 08-aug-1992 Reported 14-aug-1992 Project VOA Sample # 920810002 Sample ID 565-1 Sample Type Water

Volatile Organics HSL

(ML/SW 8240

Laboratory Report

84214 Hill Air Force Base/JMM-SLC 4525 Wasatch Blvd Sait Lake City , UI ATIN: Dave fulton

Dacameter	Result	XRec Conc. D	Dilution	Det.Limit	Prepared	6	Analyzed	e X
						•		
			2	n			JAAI . BOR . JI	5
1,1-Dichloroethylene (1,10CE) ug/l	2	•	0	~			12-aug-1992	5
	₽	-	0	\$			12-aug-1992	d i
	웆		0	~			12-aug-1992	 9
	2		0	2			12-aug-1992	Ę
	: : : : :	•	0	2			12-aug-1992	<u>-</u>
1,3-Dichlorobenzene	2		0	~			12-aug-1992	đťi
	· •	-	0	~			12-aug-1992	dfi
2.Butenore (NEK)	2		0	100			12- aug- 1992	; jp
	2		0	10			12-aug-1992	Ë
	2		0	901			12-aug-1992	đ
	\$		0	01			12-aug-1992	e e
Acetone Ug/L	2		0	100			12-aug-1992	===
	2		0	5			12-aug-1992	Ë
	2		•	2			12-aug-1992	ğ.
	7.7		0	~	,		12-aug-1992	ž p
cis-1,2-Dichloroethere ug/l	2			~	•		12- aug- 1992	=
	2	•	•	2			12-aug-1992	ă.
cla-1,3-Dichloropropene	2		0				12-aug-1992	df.
	운		0	2			12-aug-1992	Ę
Chloroform (Trichloromethane) ug/l	2			.			12-aug-1992	ğ,
	2		0	9			12-809-1992	df.
Carbon disulfide ug/l	2		0	~			12-aug-1992	Ę.
		-	0	2			12-aug-1992	Ë
Dibrosochiorosathene ug/l	2		0.	•			12- aug- 1992	Ę
hane	윷	-	0	2			12-aug-1992	df.i
Ethyl benzene ug/l	S		0	~			12-aug-1992	Ę
Methyl Bromide ug/l	Q :	-	•	9			12-aug-1992	Ę.
Methyl Chloride	2	-	0	\$			12-aug-1992	Ë

Report #: 2253





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555 East Warrut Street, P.O. Box 7009 Pasadena, California 91109-7009 (818) 796-9141

Sampled <u>07-aug-1992</u> Received <u>08-aug-1992</u> Reported <u>14-aug-1992</u> Project VOA Sample # 920810002 Sample 1D 5GS-1 Sample Type Water

Volatile Organics HSL

(ML/SW 8240

Laboratory Report

Hill Air Force Base/JMM-SLC 4525 Wasatch Blvd

84214 Salt Lake City , UT ATTN: Dave fulton

8y Analyzed 8y 12-aug-1992 dfi 12-aug-1992 dfi	12-aug-1992 dfi	12-aug-1992 dfi	12-aug-1992 dfi 12-aug-1992 dfi	12-aug-1992 dfi 12-aug-1992 dff	12-aug-1992 dfi 12-aug-1992 dfi	12-aug-1992 dfi 12-aug-1992 dfi	12-aug-1992 dfi 12-aug-1992 dfi
Prepared							
Det.Limit 30 5	~ ;	~ ~ ·	~ ~	~ ~	5 °	100 	00 001
Dilution 10 10	0.00	2 2	<u>ء</u> ج	2 2	2 2	o o	5 6
XRec Conc.							
Result NO 61	- 61	3 2	99	2 2	2 2	2 2	9 9
Units UQ/L	1/85)/81 1/81	- 1 2 3]/ 3	1/85	1/6n 1/6n	1/8n
Parameter Hethytene Chloride m.o.Xvlenes	o-Xylene	1, 1, 2, 2-Tetrachloroethane Tetrachloroethylene (PCE)		1,1,1-Trichloroethane Trichloroethylane (TCE)			
\$		hloroethane ylene (PCE)	Styrene trans:1,2:Dichloroethane	pethane ane (TCE)	Trichlorofluoromethane trans-1,3-Dichloropropene	Tetrahydrofuran Tolugne	Vinyl Chloride (VC)
Parameter Methylene Chlor m.p-Xylenes	Xylene	1,1,2,2-Tetrachloroethane Tetrachloroethylene (PCE)	Styrene transr1,2-Dichl	1,1-Trichlorichlorock	Trichlorofluoromethane trans-1,3-Dichloroprope	Tetrahydrofuran Toluene	Vinyl Chloride (VC) Vinyl Acetate

Report #: 2253

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NG NG

CLIENT: James M. Montgomery

4525 S. Wasatch Blvd.

SLC, Utah 84124

PROJECT NO. : 92-1016

W?

DAF

SAMPLE NO. : 57

REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : SAMPLE MATRIX : Ground Water CLIENT P.O. :

SAMPLE MATRIX : Ground Water CLIENT P.O. : None SAMPLED BY : NKT/RAK SAMPLE DATE : 08/05/92 SAMPLE SOURCE : TP-01 SUBMITTAL DATE: 08/07/92

ANALYST : NKT ANALYSIS DATE : 08/07/92

Sample Analysis					
Parameter	Result	Unit	Detection Level		
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chloroethane Chloroform Chloromethane 2-Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromo-3-chloropropane	0.741 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005		
Dibromochloromethane 1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Dichloroethane 1,2-Dichloroethane	N/A N/A N/A N/A N/A N/A N/A	mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005		

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 57 SLC, Utah 84124 REPORT DATE : 10/09/92

REVIEWED BY : RAK

SAMPLE SOURCE: TP-01 PAGE : 2 OF 2

Sample Analysis					
Parameter	Result	Unit	Detection Level		
cis 1,2-Dichloroethene	N/A	mg/L	0.005		
trans 1,2-Dichloroethene	n/a	mg/L	0.005		
1,2-Dichloropropane	N/A	mg/L	0.005		
1,3-Dichloropropane	n/a	mg/L	0.005		
2,2-Dichloropropane	N/A	mg/L	0.005		
1,1-Dichloropropene	N/A	mg/L	0.005		
1,1-Dichloroethene	N/A	mg/L	0.005		
cis 1,3-Dichloropropene	n/a	mg/L	0.005		
trans 1,3-Dichloropropene .	N/A	mg/L	0.005		
Ethylbenzene	< 0.005	mg/L	0.005		
Hexachlorobutadiene	N/A	mg/L	0.005		
Isoproylbenzene	n/a	mg/L	0.005		
4-Isopropyltoluene	N/A	mg/L	0.005		
Dichloromethane	n/a	mg/L	0.005		
Napthalene	N/A	mg/L	0.005		
Propylbenzene	N/A	mg/L	0.005		
Styrene	N/A	mg/L	0.005		
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005		
1,1,2,2-Tetrachloroethene					
(Tetrachloroethylene)	0.425	mg/L	0.005		
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005		
Toluene	2.273	mg/L	0.005		
1,2,3-Trichlorobenzene	N/A	mg/L	0.005		
1,2,4-Trichlorobenzene	N/A	mg/L	0.005		
1,1,1-Trichloroethane	N/A	mg/L	0.005		
1,1,2-Trichloroethane	N/A	mg/L	0.005		
Trichloroethene (TCE)	N/A	mg/L	0.005		
Fluorotrichloromethane	N/A	mg/L	0.005		
1,2,3-Trichloropropane	N/A	mg/L	0.005		
1,2,4-Trimethylbenzene	N/A	mg/L	0.005		
1,3,5-Trimethylbenzene	N/A	mg/L	0.005		
Vinyl chloride	N/A	mg/L	0.005		
p-m-Xylene	0.540	mg/L	0.005		
o-Xylene	0.487	mg/L	0.005		

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CLIENT: James M. Montgomery PROJECT NO. : 92-1016

4525 S. Wasatch Blvd.

SAMPLE NO. : 39 REPORT DATE : 10/09/92 SLC, Utah 84124

(4)

REVIEWED BY : RAK SAMPLE SOURCE: TP-02 PAGE : 2 OF 2

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 39

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF

SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLED BY : NKT/RAK SAMPLE DATE : 08/05/92 SAMPLE SOURCE : TP-02 SUBMITTAL DATE: 08/05/92

ANALYST : NKT ANALYSIS DATE : 08/06/92

Sample Analysis					
Parameter	Result	Unit	Detection Level		
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotehane Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromoethane (EDB) 1,2-Dibromoethane Dibromomethane 1,2-Dichlorobenzene (meta) 1,4-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Dichloroethane	5.203 N/A		0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005		
1,2-Dichloroethane	N/A	mg/L	0.005		

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 90

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY: RAK
Attn: David A. Fulton PAGE: 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLE MAIRIX : GIODING WATCH

SAMPLED BY : NKT/RAK SAMPLE DATE : 08/10/92

SAMPLE SOURCE : TP-03 SUBMITTAL DATE: 08/10/92

ANALYST : NKT ANALYSIS DATE : 08/10/92

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 90

SIC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY: RAK
SAMPLE SOURCE: TP-03 PAGE: 2 OF 2

Sample Analysis Detection Unit Parameter Result Level cis 1,2-Dichloroethene N/A mg/L 0.005 0.005 trans 1,2-Dichloroethene .. N/A mg/L 0.005 1,2-Dichloropropane N/A mg/L 1,3-Dichloropropane N/A 0.005 mg/L 2,2-Dichloropropane N/A mg/L 0.005 1,1-Dichloropropene N/A mg/L 0.005 1,1-Dichloroethene N/A 0.005 mg/L cis 1,3-Dichloropropene ... mg/L N/A 0.005 trans 1,3-Dichloropropene . N/A mg/L 0.005 Ethylbenzene 0.322 0.005 mg/L Hexachlorobutadiene N/A 0.005 mg/LIsoproylbenzene N/A 0.005 mg/L4-Isopropyltoluene N/A 0.005 mg/L Dichloromethane N/A mq/L 0.005 Napthalene N/A mg/L 0.005 Propylbenzene N/A mg/L 0.005 Styrene N/A 0.005 mq/L 1,1,2,2-Tetrachloroethane . N/A mq/L0.005 1,1,2,2-Tetrachloroethene (Tetrachloroethylene) 2.447 0.005 mg/L 1,1,1,2-Tetrachloroethane . N/A 0.005 mg/L Toluene 0.005 3.112 mq/L mg/L 1,2,3-Trichlorobenzene N/A 0.005 1,2,4-Trichlorobenzene N/A mg/L 0.005 1,1,1-Trichloroethane N/A 0.005 mg/L 1,1,2-Trichloroethane N/A mg/L 0.005 Trichloroethene (TCE) N/A mg/L 0.005 Fluorotrichloromethane N/A mg/L 0.005 1,2,3-Trichloropropane N/A mg/L 0.005 1,2,4-Trimethylbenzene N/A mg/L 0.005 1,3,5-Trimethylbenzene N/A mg/L 0.005 Vinyl chloride N/A mg/L 0.005 p-m-Xylene 0.801 0.005 mg/L

0.854

mg/L

0.005

o-Xylene

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 26

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY: RAK
Attn: David A. Fulton PAGE: 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLE MATRIX : Ground Water CLIENT P.O. : None
SAMPLED BY : NKT/RAK SAMPLE DATE : 08/05/92
SAMPLE SOURCE : TP-07 SUBMITTAL DATE: 08/05/92
ANALYST : NKT ANALYSIS DATE : 08/06/92

Sample Analysis					
Parameter	Result	Unit	Detection Level		
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotehane Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromoethane Dibromomethane 1,2-Dichlorobenzene (meta) 1,4-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Pichloroethane 1,2-Lichloroethane 1,2-Lichloroethane	26.092 N/A	mg/L mg/L mg/L mg/L mg//L mg/L mg//L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005		

James M. Montgomery 4525 S. Wasatch Blvd. CLIENT: PROJECT NO. : 92-1016

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SAMPLE NO. : 26
REPORT DATE : 10/09/92
REVIEWED BY : RAK SLC, Utah 84124

SAMPLE SOURCE: TP-07 PAGE: 2 OF 2

Sample Analysis					
Parameter	Result	Unit	Detection Level		
cis 1,2-Dichloroethene	N/A	mg/L	0.005		
trans 1,2-Dichloroethene	N/A	mg/L	0.005		
1,2-Dichloropropane	N/A	mg/L	0.005		
1,3-Dichloropropane	N/A	mg/L	0.005		
2,2-Dichloropropane	N/A	mg/L	0.005		
1,1-Dichloropropene	N/A	mg/L	0.005		
1,1-Dichloroethene	N/A	mg/L	0.005		
cis 1,3-Dichloropropene	N/A	mg/L	0.005		
trans 1,3-Dichloropropene .	N/A	mg/L	0.005		
Ethylbenzene	0.753	mg/L	0.005		
Hexachlorobutadiene	N/A	mg/L	0.005		
Isoproylbenzene	N/A	mg/L	0.005		
4-Isopropyltoluene	N/A	mg/L	0.005		
Dichloromethane	N/A	mg/L	0.005		
Napthalene	N/A	mg/L	0.005		
Propylbenzene	N/A	mg/L	0.005		
Styrene	N/A	mg/L	0.005		
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005		
1,1,2,2-Tetrachloroethene					
(Tetrachloroethylene)	2.204	mg/L	0.005		
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005		
Toluene	21.919	mg/L	0.005		
1,2,3-Trichlorobenzene	N/A	mg/L	0.005		
1,2,4-Trichlorobenzene	N/A	mg/L	0.005		
1,1,1-Trichloroethane	N/A	mg/L	0.005		
1,1,2-Trichloroethane	N/A	mg/L	0.005		
Trichloroethene (TCE)	N/A	mg/L	0.005		
Fluorotrichloromethane	N/A	mg/L	0.005		
1,2,3-Trichloropropane	N/A	mg/L	0.005		
1,2,4-Trimethylbenzene	N/A	mg/L	0.005		
1,3,5-Trimethylbenzene	N/A	mg/L	0.005		
Vinyl chloride	N/A	mg/L	0.005		
p-m-Xylene	1.459	mg/L	0.005		
o-Xylene	2.447	mg/L	0.005		

CLIENT: James M. Montgomery PROJECT No.: 92-1016

4525 S. Wasatch Blvd. SAMPLE No. : 37

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF
SAMPLE MATRIX : Ground Water CLIENT P.O. : None
SAMPLED BY : NKT/RAK SAMPLE DATE : 08/06/92
SAMPLE SOURCE : TP-09 SUBMITTAL DATE: 08/06/92
ANALYST : NKT ANALYSIS DATE : 08/06/92

Sample Analysis					
Parameter	Result	Unit	Detection Level		
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chloroform Chloromethane 2-Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromo-3-chloropropane Dibromomethane	0.992 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005		
1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane	N/A N/A N/A	mg/L mg/L	0.005 0.005 0.005 0.005		
1,1-Dichloroethane	N/A N/A N/A	mg/L mg/L mg/L	0.005 0.005 0.005		

CLIENT: James M. Montgomery PROJECT NO. : 92-1016

4525 S. Wasatch Blvd.

SLC, Utah 84124

PROJECT NO.: 32-111 SAMPLE NO.: 37 REPORT DATE: 10/09/92 REVIEWED BY: RAK : 2 OF 2 SAMPLE SOURCE: TP-09 PAGE: 2 OF 2

Sample Analysis					
Parameter	Result	Unit	Detection Level		
cis 1,2-Dichloroethene	N/A	mg/L	0.005		
trans 1,2-Dichloroethene	n/a	mg/L	0.005		
1,2-Dichloropropane	N/A	mg/L	0.005		
1,3-Dichloropropane	N/A	mg/L	0.005		
2,2-Dichloropropane	N/A	mg/L	0.005		
1,1-Dichloropropene	N/A	mg/L	0.005		
1,1-Dichloroethene	N/A	mg/L	0.005		
cis 1,3-Dichloropropene	N/A	mg/L	0.005		
trans 1,3-Dichloropropene .	N/A	mg/L	0.005		
Ethylbenzene	0.173	mg/L	0.005		
Hexachlorobutadiene	N/A	mg/L	0.005		
Isoproylbenzene	N/A	mg/L	0.005		
4-Isopropyltoluene	N/A	mg/L	0.005		
Dichloromethane	N/A	mg/L	0.005		
Napthalene	N/A	mg/L	0.005		
Propylbenzene	N/A	mg/L	0.005		
Styrene	N/A	mg/L	0.005		
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005		
1,1,2,2-Tetrachloroethene		1 -			
(Tetrachloroethylene)	1.269	mg/L	0.005		
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005		
Toluene	2.128	mg/L	0.005		
1,2,3-Trichlorobenzene	N/A	mg/L	0.005		
1,2,4-Trichlorobenzene	N/A	mg/L	0.005		
1,1,1-Trichloroethane	N/A	mg/L	0.005		
1,1,2-Trichloroethane	N/A	mg/L	0.005		
Trichloroethene (TCE)	N/A	mg/L	0.005		
Fluorotrichloromethane	N/A	mg/L	0.005		
1,2,3-Trichloropropane	N/A	mg/L	0.005		
1,2,4-Trimethylbenzene	N/A	mg/L	0.005		
1,3,5-Trimethylbenzene	N/A	mg/L	0.005		
Vinyl chloride	N/A	mg/L	0.005		
p-m-Xylene	0.211	mg/L	0.005		
o-Xylene	0.090	mg/L	0.005		

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE No. : 38

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLED BY: NKT/RAK SAMPLE DATE: 08/06/92 SAMPLE SOURCE: TP-10 SUBMITTAL DATE: 08/06/92 ANALYST: NKT ANALYSIS DATE: 08/06/92

Sample Analysis					
Parameter	Result	Unit	Detection Level		
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotoluene Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromo-3-chloropropane Dibromomethane Dibromomethane 1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta)	1.928 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005		
1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Dichloroethane 1,2-Dichloroethane	N/A N/A N/A N/A	mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005		

James M. Montgomery 4525 S. Wasatch Blvd. SLC, Utah 84124 CLIENT: PROJECT NO. : 92-1016

SAMPLE NO. : 38
REPORT DATE : 10/09/92
REVIEWED BY : RAK

SAMPLE SOURCE: TP-10 PAGE : 2 OF 2

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 55

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT IC NO. : None AUTHORIZED BY : DAF
SAMPLE MATRIX : Ground Water CLIENT P.O. : None
SAMPLED BY : NKT/RAK SAMPLE DATE : 08/07/92

SAMPLE SOURCE: TP-12 SUBMITTAL DATE: 08/07/92
ANALYST: NKT ANALYSIS DATE: 08/07/92

Sample Analysis				
Parameter	Result	Unit	Detection Level	
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotoluene Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane Dibromomethane 1,2-Dichlorobenzene (ortho)	1.163 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005	
1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Dichloroethane 1,2-Dichloroethane	N/A N/A N/A N/A N/A	mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005	

CLIENT: James M. Montgomery 4525 S. Wasatch Blvd. SLC, Utah 84124 PROJECT NO. : 92-1016

SAMPLE NO. : 55 REPORT DATE : 10/09/92

REVIEWED BY : RAK SAMPLE SOURCE: TP-12 PAGE : 2 OF 2

Sample Analysis			
Parameter	Result	Unit	Detection Level
cis 1,2-Dichloroethene	N/A	mg/L	0.005
trans 1,2-Dichloroethene	N/A	mg/L	0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	N/A	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
cis 1,3-Dichloropropene	N/A	mg/L	0.005
trans 1,3-Dichloropropene .	N/A	mg/L	0.005
Ethylbenzene	0.062	mg/L	↑ 005
Hexachlorobutadiene	N/A	mg/L	0.005
Isoproylbenzene	N/A	mg/L	0.005
4-Isopropyltoluene	N/A	mg/L	0.005
Dichloromethane	N/A	mg/L	0.005
Napthalene	N/A	mg/L	0.005
Propylbenzene	N/A	mg/L	0.005
Styrene	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethene			
(Tetrachloroethylene)	0.636	mg/L	0.005
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005
Toluene	0.565	mg/L	0.005
1,2,3-Trichlorobenzene	N/A	mg/L	0.005
1,2,4-Trichlorobenzene	N/A	mg/L	0.005
1,1,1-Trichloroethane	N/A	mg/L	0.005
1,1,2-Trichloroethane	N/A	mg/L	0.005
Trichloroethene (TCE)	N/A	mg/L	0.005
Fluorotrichloromethane	N/A	mg/L	0.005
1,2,3-Trichloropropane	N/A	mg/L	0.005
1,2,4-Trimethylbenzene	N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
p-m-Xylene	0.215	mg/L	0.005
o-Xylene	0.050	mg/L	0.005

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 58

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF

SAMPLE MATRIX : Ground Water CLIENT P.O. : None SAMPLED BY : NKT/RAK SAMPLE DATE : 08/07/92 SAMPLE SOURCE : TP-13 SUBMITTAL DATE: 08/07/92

ANALYST : NKT ANALYSIS DATE : 08/07/92

Sample Analysis				
Parameter	Result	Unit	Detection Level	
Benzene	< 0.005	mg/L	0.005	
	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
Bromodichloromethane Bromoform Bromomethane n-Butylbenzene	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride	n/a	mg/L	0.005	
	n/a	mg/L	0.005	
	n/a	mg/L	0.005	
Chlorobenzene	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
2-Chlorotoluene (ortho)	N/A	mg/L	0.005	
4-Chlorotoluene (para)	N/A	mg/L	0.005	
1,2-Dibromoethane (EDB)	N/A	mg/L	0.005	
1,2-Dibromo-3-chloropropane Dibromochloromethane Dibromomethane	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
	N/A	mg/L	0.005	
1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane	n/a n/a n/a n/a	mg/L mg/L mg/L	0.005 0.005 0.005 0.005	
1,1-Dichloroethane	N/A	mg/L	0.005	
	N/A	mg/L	0.005	

CLIENT: James M. Montgomery PROJECT NO. : 92-1016

4525 S. Wasatch Blvd.

SAMPLE NO. : 58
REPORT DATE : 10/09/92
REVIEWED BY : RAK SLC, Utah 84124

SAMPLE SOURCE: TP-13 PAGE : 2 OF 2

		7	
Parameter	Result	Unit	Detection Level
cis 1,2-Dichloroethene	N/A	mg/L	0.005
trans 1,2-Dichloroethene	N/A	mg/L	0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	N/A	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
cis 1,3-Dichloropropene	N/A	mg/L	0.005
trans 1,3-Dichloropropene .	N/A	mg/L	0.005
Ethylbenzene	< 0.005	mg/L	0.005
Hexachlorobutadiene	N/A	mg/L	0.005
Isoproylbenzene	N/A	mg/L	0.005
4-Isopropyltoluene	N/A	mg/L	0.005
Dichloromethane	n/a	mg/L	0.005
Napthalene	N/A	mg/L	0.005
Propylbenzene	n/a	mg/L	0.005
Styrene	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethene		1	
(Tetrachloroethylene)	< 0.005	mg/L	0.005
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005
Toluene	0.069	mg/L	0.005
1,2,3-Trichlorobenzene	N/A	mg/L	0.005
1,2,4-Trichlorobenzene	N/A	mg/L	0.005
1,1,1-Trichloroethane	n/a	mg/L	0.005
1,1,2-Trichloroethane	N/A	mg/L	0.005
Trichloroethene (TCE)	N/A	mg/L	0.005
Fluorotrichloromethane	N/A	mg/L	0.005
1,2,3-Trichloropropane	N/A	mg/L	0.005
1,2,4-Trimethylbenzene	N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
p-m-Xylene	0.062	mg/L	0.005
o-Xylene	< 0.005	mg/L	0.005

CLIENT: James M. Montgomery PROJECT No.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 59

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLED BY : NKT/RAK SAMPLE DATE : 08/07/92 SAMPLE SOURCE : TP-14 SUBMITTAL DATE: 08/07/92 ANALYST : NKT ANALYSIS DATE : 08/07/92

Sample Analysis				
Parameter	Result	Unit	Detection Level	
Benzene	1.440 N/A N/A N/A N/A	mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005	
Bromomethane	N/A N/A N/A N/A N/A	mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005	
Chlorobenzene	N/A N/A N/A N/A N/A	mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005	
4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromo-3-chloropropane Dibromochloromethane Dibromomethane	N/A N/A N/A N/A N/A	mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005	
1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Dichloroethane	N/A N/A N/A N/A N/A	mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005	

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 59

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY: RAK
SAMPLE SOURCE: TP-14 PAGE : 2 OF 2

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 68

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY: RAK
Attn: David A. Fulton PAGE: 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLED BY: NKT/RAK SAMPLE DATE: 08/08/92
SAMPLE SOURCE: TP-17 SUBMITTAL DATE: 08/08/92
ANALYST: NKT ANALYSIS DATE: 08/08/92

Sample Analysis				
Parameter	Result	Unit	Detection Level	
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotehane Chloroform Chloromethane 2-Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromoethane Dibromomethane Dibromomethane 1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane	< 0.005 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005	

James M. Montgomery 4525 S. Wasatch Blvd. CLIENT: PROJECT NO. : 92-1016

SAMPLE NO. : 68 REPORT DATE : 10/09/92 SLC, Utah 84124

REVIEWED BY : RAK

SAMPLE SOURCE: TP-17 PAGE : 2 OF 2

Sample Analysis			
Parameter	Result	Unit	Detection Level
cis 1,2-Dichloroethene	N/A	mg/L	0.005
trans 1,2-Dichloroethene	N/A	mg/L	0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	N/A	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
cis 1,3-Dichloropropene	N/A	mg/L	0.005
trans 1,3-Dichloropropene .	N/A	mg/L	0.005
Ethylbenzene	0.014	mg/L	0.005
Hexachlorobutadiene	N/A	mg/L	0.005
Isoproylbenzene	N/A	mg/L	0.005
4-Isopropyltoluene	N/A	mg/L	0.005
Dichloromethane	N/A	mg/L	0.005
Napthalene	N/A	mg/L	0.005
Propylbenzene	N/A	mg/L	0.005
Styrene	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethene			
(Tetrachloroethylene)	< 0.005	mg/L	0.005
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005
Toluene	< 0.005	mg/L	0.005
1,2,3-Trichlorobenzene	N/A	mg/L	0.005
1,2,4-Trichlorobenzene	N/A	mg/L	0.005
1,1,1-Trichloroethane	N/A	mg/L	0.005
1,1,2-Trichloroethane	N/A	mg/L	0.005
Trichloroethene (TCE)	N/A	mg/L	0.005
Fluorotrichloromethane	N/A	mg/L	0.005
1,2,3-Trichloropropane	N/A	mg/L	0.005
1,2,4-Trimethylbenzene	N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
p-m-Xylene	0.057	mg/L	0.005
o-Xylene	< 0.005	mg/L	0.005

CLIENT: James M. Montgomery PROJECT NO. : 92-1016

4525 S. Wasatch Blvd.

SAMPLE NO. : 72
REPORT DATE : 10/09/92
REVIEWED BY : RAK SLC, Utah 84124

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLE DATE: 08/08/92 SUBMITTAL DATE: 08/08/92 ANALYSIS DATE: 08/08/92 NKT/RAK SAMPLED BY : SAMPLE SOURCE : TP-19 ANALYST : NKT

Sample Analysis			
Parameter	Result	Unit	Detection Level
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotoluene Chloromethane 2-Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromo-3-chloropropane Dibromomethane Dibromomethane 1,2-Dichlorobenzene (ortho)	0.646 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane	N/A N/A N/A	mg/L mg/L mg/L	0.005 0.005 0.005
1,1-Dichloroethane	N/A N/A	mg/L mg/L	0.005 0.005

CLIENT: James M. Montgomery

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4525 S. Wasatch Blvd.

SLC, Utah 84124

PROJECT NO.: 92-1016 SAMPLE NO.: 72 REPORT DATE: 10/09/92 REVIEWED BY: RAK PAGE: 2 OF 2 SAMPLE SOURCE: TP-19

Sample Analysis			
Parameter	Result	Unit	Detection Level
cis 1,2-Dichloroethene trans 1,2-Dichloroethene	N/A N/A	mg/L	0.005 0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	N/A	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
cis 1,3-Dichloropropene	N/A	mg/L	0.005
trans 1,3-Dichloropropene .	N/A	mg/L	0.005
Ethylbenzene	0.036	mg/L	0.005
Hexachlorobutadiene	N/A	mg/L	0.005
Isoproylbenzene	N/A	mg/L	0.005
4-Isopropyltoluene	N/A	mg/L	0.005
Dichloromethane	N/A	mg/L	0.005
Napthalene	N/A	mg/L	0.005
Propylbenzene	N/A	mg/L	0.005
Styrene	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethene	0 125	17	0.005
(Tetrachloroethylene)	0.125	mg/L	0.005
1,1,1,2-Tetrachloroethane . Toluene	N/A < 0.005	mg/L	0.005
1,2,3-Trichlorobenzene		mg/L	0.005
1,2,4-Trichlorobenzene	N/A	mg/L	0.005 0.005
1,1,1-Trichloroethane	N/A N/A	mg/L	0.005
1,1,2-Trichloroethane	N/A N/A	mg/L	0.005
Trichloroethene (TCE)	N/A N/A	mg/L mg/L	0.005
Fluorotrichloromethane	• .		0.005
1,2,3-Trichloropropane	N/A N/A	mg/L mg/L	0.005
1,2,4-Trimethylbenzene	N/A N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
p-m-Xylene	0.149	mg/L	0.005
o-Xylene	< 0.005	mg/L	0.005
		mg/ 11	0.003

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 73

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF
SAMPLE MATRIX : Ground Water CLIENT P.O. : None
SAMPLED BY : NKT/RAK SAMPLE DATE : 08/08/92
SAMPLE SOURCE : TP-20 SUBMITTAL DATE: 08/08/92
ANALYST : NKT ANALYSIS DATE : 08/08/92

Organic Monitoring __ng Water Volatiles Full Suite

Sample Analysis			
Parameter	Result	Unit	Detection Level
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotoluene Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromoethane Dibromomethane 1,2-Dichlorobenzene (ortho)	0.124 N/A		0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para) Dichlorodifluoromethane	N/A N/A N/A	mg/L mg/L mg/L	0.005 0.005 0.005
1,1-Dichloroethane	N/A N/A	mg/L mg/L	0.005 0.005

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 73

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

SAMPLE SOURCE: TP-20 PAGE : 2 OF 2

Sample Analysis			
Parameter	Result	Unit	Detection Level
cis 1,2-Dichloroethene	N/A	mg/L	0.005
trans 1,2-Dichloroethene	N/A	mq/L	0.005
1,2-Dichloropropane	N/A	mg/L	0.005
1,3-Dichloropropane	N/A	mg/L	0.005
2,2-Dichloropropane	N/A	mg/L	0.005
1,1-Dichloropropene	N/A	mg/L	0.005
1,1-Dichloroethene	N/A	mg/L	0.005
cis 1,3-Dichloropropene	N/A	mg/L	0.005
trans 1,3-Dichloropropene .	N/A	mg/L	0.005
Ethylbenzene	< 0.005	mg/L	0.005
Hexachlorobutadiene	N/A	mg/L	0.005
Isoproylbenzene	N/A	mg/L	0.005
4-Isopropyltoluene	N/A	mg/L	0.005
Dichloromethane	N/A	mg/L	0.005
Napthalene	N/A	mg/L	0.005
Propylbenzene	N/A	mg/L	0.005
Styrene	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005
1,1,2,2-Tetrachloroethene	·	ļ - ·	
(Tetrachloroethylene)	0.303	mg/L	0.005
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005
Toluene	2.699	mg/L	0.005
1,2,3-Trichlorobenzene	N/A	mg/L	0.005
1,2,4-Trichlorobenzene	N/A	mg/L	0.005
1,1,1-Trichloroethane	N/A	mg/L	0.005
1,1,2-Trichloroethane	N/A	mg/L	0.005
Trichloroethene (TCE)	N/A	mg/L	0.005
Fluorotrichloromethane	N/A	mg/L	0.005
1,2,3-Trichloropropane	N/A	mg/L	0.005
1,2,4-Trimethylbenzene	N/A	mg/L	0.005
1,3,5-Trimethylbenzene	N/A	mg/L	0.005
Vinyl chloride	N/A	mg/L	0.005
p-m-Xylene	< 0.005	mg/L	0.005
o-Xylene	0.504	mg/L	0.005
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CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 74

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLE MATRIX : GIOUNG Water CLIENT P.O. : NONE
SAMPLED BY : NKT/RAK SAMPLE DATE : 08/08/92
SAMPLE SOURCE : TP-21 SUBMITTAL DATE: 08/08/92
ANALYST : NKT ANALYSIS DATE : 08/08/92

Sample Analysis			
Parameter	Result	Unit	Detection Level
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chlorotethane Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromoethane (EDB) 1,2-Dibromo-3-chloropropane Dibromomethane Dibromomethane 1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta)	< 0.005 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
1,4-Dichlorobenzene (para) Dichlorodifluoromethane 1,1-Dichloroethane 1,2-Dichloroethane	N/A N/A N/A N/A	mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005

CLIENT: James M. Montgomery PROJECT NO. : 92-1016

4525 S. Wasatch Blvd.

SAMPLE NO. : 74
REPORT DATE : 10/09/92 SLC, Utah 84124

REVIEWED BY : RAK SAMPLE SOURCE: TP-21 PAGE : 2 OF 2

Sample Analysis				
Parameter	Result	Unit	Detection Level	
cis 1,2-Dichloroethene	N/A	mg/L	0.005	
trans 1,2-Dichloroethene	N/A	mg/L	0.005	
1,2-Dichloropropane	N/A	mg/L	0.005	
1,3-Dichloropropane	N/A	mg/L	0.005	
2,2-Dichloropropane	N/A	mg/L	0.005	
1,1-Dichloropropene	N/A	mg/L	0.005	
1,1-Dichloroethene	N/A	mg/L	0.005	
cis 1,3-Dichloropropene	N/A	mg/L	0.005	
trans 1,3-Dichloropropene .	N/A	mg/L	0.005	
Ethylbenzene	< 0.005	mg/L	0.005	
Hexachlorobutadiene	N/A	mg/L	0.005	
Isoproylbenzene	N/A	mg/L	0.005	
4-Isopropyltoluene	N/A	mg/L	0.005	
Dichloromethane	N/A	mg/L	0.005	
Napthalene	N/A	mg/L	0.005	
Propylbenzene	N/A	mg/L	0.005	
Styrene	N/A	mg/L	0.005	
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005	
1,1,2,2-Tetrachloroethene		1		
(Tetrachloroethylene)	< 0.005	mg/i	0.005	
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005	
Toluene	< 0.005	mg/L	0.005	
1,2,3-Trichlorobenzene	N/A	mg/L	0.005	
1,2,4-Trichlorobenzene	N/A	mg/L	0.005	
1,1,1-Trichloroethane	N/A	mg/L	0.005	
1,1,2-Trichloroethane	N/A	mg/L	0.005	
Trichloroethene (TCE)	N/A	mg/L	0.005	
Fluorotrichloromethane	N/A	mg/L	0.005	
1,2,3-Trichloropropane	N/A	mg/L	0.005	
1,2,4-Trimethylbenzene	N/A	mg/L	0.005	
1,3,5-Trimethylbenzene	N/A	mg/L	0.005	
Vinyl chloride	N/A	mg/L	0.005	
p-m-Xylene	0.057	mg/L	0.005	
o-Xylene	< 0.005	mg/L	0.005	

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 83

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLED BY: NKT/RAK SAMPLE DATE: 08/09/92
SAMPLE SOURCE: TP-22 SUBMITTAL DATE: 08/10/92
ANALYST: NKT ANALYSIS DATE: 08/10/92

Sample Analysis			
Parameter	Result	Unit	Detection Level
Benzene Bromobenzene Bromochloromethane Bromodichloromethane Bromoform Bromomethane n-Butylbenzene sec-Butylbenzene tert-Butylbenzene Carbon tetrachloride Chlorobenzene Chloroethane Chloroform Chloromethane 2-Chlorotoluene (ortho) 4-Chlorotoluene (para) 1,2-Dibromo-3-chloropropane Dibromomethane 1,2-Dichlorobenzene (ortho) 1,3-Dichlorobenzene (meta) 1,4-Dichlorobenzene (para)	0.056 N/A	mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
Dichlorodifluoromethane 1,1-Dichloroethane 1,2-Dichloroethane	N/A N/A N/A	mg/L mg/L mg/L	0.005 0.005 0.005

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

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4525 S. Wasatch Blvd. SAMPLE NO. : 83

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

SAMPLE SOURCE: TP-22 PAGE : 2 OF 2

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 131

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLED BY: NKT/RAK SAMPLE DATE: 08/13/92
SAMPLE SOURCE: TP-36 SUBMITTAL DATE: 08/13/92
ANALYST: NKT ANALYSIS DATE: 08/13/92

PROJECT NO. : 92-1016 CLIENT:

James M. Montgomery 4525 S. Wasatch Blvd. SLC, Utah 84124 SAMPLE NO. : 131

REPORT DATE: 10/09/92

REVIEWED BY : RAK SAMPLE SOURCE: TP-36 PAGE : 2 OF 2

CLIENT: James M. Montgomery PROJECT NO.: 92-1016

4525 S. Wasatch Blvd. SAMPLE NO. : 130

SLC, Utah 84124 REPORT DATE: 10/09/92

REVIEWED BY : RAK

Attn: David A. Fulton PAGE : 1 OF 2

CLIENT ID NO. : None AUTHORIZED BY : DAF SAMPLE MATRIX : Ground Water CLIENT P.O. : None

SAMPLE MATRIX : Ground Water CLIENT P.O. : None SAMPLED BY : NKT/RAK SAMPLE DATE : 08/13/92 SAMPLE SOURCE : TP-37 SUBMITTAL DATE: 08/13/92

ANALYST : NKT ANALYSIS DATE : 08/13/92

CLIENT: James M. Montgomery

PROJECT NO. : 92-1016 4525 S. Wasatch Blvd.

SAMPLE NO. : 130 REPORT DATE : 10/09/92 SLC, Utah 84124

REVIEWED BY : RAK SAMPLE SOURCE: TP-37 PAGE : 2 OF 2

Sample Analysis				
Parameter	Result	Unit	Detection Level	
cis 1,2-Dichloroethene	N/A	mg/L	0.005	
trans 1,2-Dichloroethene	N/A	mg/L	0.005	
1,2-Dichloropropane	N/A	mg/L	0.005	
1,3-Dichloropropane	N/A	mg/L	0.005	
2,2-Dichloropropane	N/A	mg/L	0.005	
1,1-Dichloropropene 1,1-Dichloroethene	N/A	mg/L	0.005	
cis 1,3-Dichloropropene	N/A	mg/L	0.005	
trans 1,3-Dichloropropene	N/A N/A	mg/L	0.005	
Ethylbenzene	< 0.005	mg/L	0.005	
Hexachlorobutadiene	N/A	mg/L	0.005	
Isoproylbenzene	N/A N/A	mg/L	0.005 0.005	
4-Isopropyltoluene	N/A N/A	mg/L	0.005	
Dichloromethane	N/A	mg/L	0.005	
Napthalene	N/A	mg/L	0.005	
Propylbenzene	N/A	mg/L	0.005	
Styrene	N/A	mg/L	0.005	
1,1,2,2-Tetrachloroethane .	N/A	mg/L	0.005	
1,1,2,2-Tetrachloroethene	<i>,</i>	_ mg/	0.005	
(Tetrachloroethylene)	2.525	mg/L	0.005	
1,1,1,2-Tetrachloroethane .	N/A	mg/L	0.005	
Toluene	0.930	mg/L	0.005	
1,2,3-Trichlorobenzene	N/A	mg/L	0.005	
1,2,4-Trichlorobenzene	N/A	mg/L	0.005	
1,1,1-Trichloroethane	N/A	mg/L	0.005	
1,1,2-Trichloroethane	N/A	mg/L	0.005	
Trichloroethene (TCE)	N/A	mg/L	0.005	
Fluorotrichloromethane	N/A	mg/L	0.005	
1,2,3-Trichloropropane	N/A	mg/L	0.005	
1,2,4-Trimethylbenzene	N/A	mg/L	0.005	
1,3,5-Trimethylbenzene	N/A	mg/L	0.005	
Vinyl chloride	N/A	mg/L	0.005	
p-m-Xylene	2.410	mq/L	0.005	
o-Xylene	1.769	mg/L	0.005	



Mountain States Analytical

The Quality Solution

CLIENT:

J.M. Montgomery Engineers

4525 So. Wasatch #200

Salt Lake City, UT 84124-

ATTN:

Mr. Robert Glascot

SAMPLE ID: MW-40

SAMPLE NO: SAMPLE SET NO:

0001527 000297S

11/24/92 DATE SAMPLED:

TIME SAMPLED: 300 DATE RECEIVED: 11/25/92

DATE REPORTED: 12/10/92 DISPOSAL DATE: 01/09/93

ANALYSIS: Volatiles - Water Matrix [EPA 601/602] (Capillary)

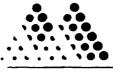
COMPOUND(s)		RESULT	LIMIT OF QUANTITATION
Chloromethane	<	2.0 ug/l	2.0 ug/l
Vinyl Chloride	<	2.0 ug/l	2.0 ug/l
Bromomethane	<	2.0 ug/l	2.0 ug/l
Chloroethane	<	2.0 ug/l	2.0 ug/l
Fluorotrichloromethane	<	2.0 ug/l	2.0 ug/l
1.1-Dichloroethene	<	1.0 ug/l	1.0 ug/l
Dichloromethane	<	1.0 ug/l	1.0 ug/l
trans-1,2-Dichloroethene	<	1.0 ug/l	1.0 ug/l
1,1-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Chloroform	<	1.0 ug/l	1.0 ug/l
1,1,1-Trichloroethane	<	1.0 ₋ g/l	1.0 ug/l
Carbon Tetrachloride	<	1.0 ug/l	1.0 ug/l
Benzene		6.5 ug/l	1.0 ug/l
1,2-Dichloroethane	<	1.0 ug/l	1.0 ug/l
Trichloroethene (TCE)	<		1.0 ug/l
1,2-Dichloropropane	<	1.0 ug/l	1.0 ug/l
Bromodichloromethane	<	1.0 ug/l	1.0 $ug/1$
cis-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
trans-1,3-Dichloropropene	<	1.0 ug/l	1.0 ug/l
Toluene		7.8 ug/l	1.0 ug/l
Tetrachloroethene (PCE)	<	1.0 ug/l	1.0 ug/l
Chlorodibromomethane	<	1.0 ug/l	1.0 ug/l
Chlorobenzene	<	1.0 ug/l	1.0 ug/l
Ethylbenzene		1.7 ug/l	1.0 ug/l
Bromoform	<	2.0 ug/l	2.0 ug/l
m,p-Xylene		12.2 ug/l	1.0 ug/l
o-Xylene/Styrene*		3.4 ug/l	1.0 ug/l

-Continued-

ENGINEERING-SCIENCE, INC.

Mui one har been usted av tabler an dup of 870-ws-2/1/2





Mountain States Analytical

The Quality Solution

James M. Montgomery Engineers 4525 South Wasatch Blvd., Suite 200

Salt Lake City, UT 84124 Telephone: (801) 272-1900 Facsimile: (801) 272-0403

Sample Number: Sample Set:

0001527 0002975

Date Reported: Date Received: 10 DEC 1992 25 NOV 1992

Disposal Date:

8 JAN 1993

Attention:

Robert Glascot

Project: Case Number: **HAFB USTs** VOCs/BTEXN

Purchase Order: 2208.0585

Customer Number: MW-40

Date Sampled: Matrix:

24 NOV 1992 Water/Waste Water

Containers:

Analysis	Catalog Number	/ Method	Result	Dry Result	Reporting Units
Volatile Aromatics/Halocarbons	05515	EPA 600 Series 601/ 602	See Attached		

1 Analysis for GC

Reviewed and approved by Kenneth Roberts, B.S. GC Group Leader

I Analysis for Sample Number 0001527





The Quality Solution

CLIENT: J.M. Montgomery Engineers LAB NO: 34828 GROUP NO: 8810 4525 S Wasatch #200 Salt Lake City, UT 84124 DATE SAMPLED: 10/01/92 TIME SAMPLED: : NTTA Mr. David Fulton DATE RECEIVED: 10/02/92 DATE REPORTED: 10/16/92 DISPOSAL DATE: 11/15/92 SAMPLE ID: Trip Blank ANALYSIS DATE: 10/12/92

ANALYSIS:

Priority Pollutants by GCMS (Volatiles)

EPA Method SW-846 8240

COMPOUNDS	FINAL RESULTS	QUANTITATION LIMIT
Compounds Chloromethane Vinyl Chlorade Bromomethane Chloroethane Trichlorofluoromethane Acrolein 1,1-Dichloroethene Methylene Chloride Acrylonitrile 1,1-Dichloroethane 1,2-Dichloroethene (total) Chloroform 1,1,1-Trichloroethane Carbon Tetrachloride Benzene 1,2-Dichloroethane Trichloroethene 1,2-Dichloroethane Trichloroethene 2-Chloroethylvinyl ether cis-1,3-Dichloropropene Toluene	<pre>RESULTS <10 ug/l <10 ug/l <10 ug/l <10 ug/l <5 ug/l<<5 ug/l</pre>	10 ug/l 10 ug/l 10 ug/l 10 ug/l 10 ug/l 5 ug/l 100 ug/l 5 ug/l
trans-1,3-Dichloropropene 1,1,2-Trichloroethane Tetrachloroethene	<5 ug/l <5 ug/l <5 ug/l <5 ug/l	5 ug/l 5 ug/l 5 ug/l 5 ug/l
	——————————————————————————————————————	
Bromoform 1,1,2,2-Tetrachloroethane	<5 ug/l <5 ug/l	5 ug/l 5 ug/l

Respectfully submitted,

John G. Hayes, B.S. Supervisor, GCMS Group

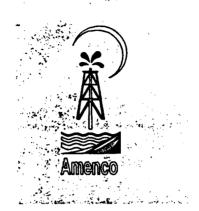




* Note the seemed to be of (Nix P. REMARKS RECEIVED BY: RECEIVED BY: (SIGNATURE) 1,22 200.1V DATE / TIME DATE / TIME REMARKS ANALYSIS USE I COLUMN ME BOTHE DATE / TIME CHAIN OF CUSTODY RECORD REUNQUISHED BY: (SIGNATURE) REUNQUISHED BY: 124 NO. OF CON-TAINERS c1 d S RECEIVED FOR LABORATORY BY: 1-870-11-MW-11-92-11P V 7.570 - 12-AM-4-92- HC 1-12-11-11-11-11 V 1520-10-1410-4-92-HE 1-872-5-MW-4-52-HF RECEIVED BY HAIS UST SIL 87% Tric Black 9/30 - 10/1 RECEIVED BY: (SIGNATURE) STATION LOCATION CP-7 DATE / TIME DATE / TIME PROJECT NAME CEVE **MONTGOMERY LABORATORIES** COMP 13.25 SAMPLERS: (Signature) 11/4: 115! 1905/1320 1 16/1/4 1200 1/ac 11/2/1/C/ ME 2208 343 PROJECT/JOB # /[*/i//.] REUNDUSHED BY: (SIGHATURE) RELINCUISHED BY: (SIGNATURE) PEUNOUISHED BY: DATE S Š Š

*

(4)



October 28, 1993

Engineering Science Todd Wiedemeier 700 Broadway, Suite 900 Denver, CO 80290

Dear Todd:

Enclosed is the sample identification and PID results for the Hill AFB project. John
 Wilson suggested that I send you a copy. I look forward to hearing from you soon.
 Call me if you have any questions.

Sincerely yours,

Lonnie G. Kennedy

Hill AFB EPA Soil Sampling Sample ID, Depth, and PID Reference

			Sample	
EPA Lab	Depth ft.	Depth ft.	Thickness	PID (ppm)
Sample ID	Top	Bottom	(Feet)	No Sample
NS	11.00	12.00	1.00	6
NS	12.00	13.00	1.00	18
NS	13.00	14.00	1.00	0
NS	14.00	15.00	1.00	4
NS_	15.00	16.00	1.00	0
NS	16.00	17.00	1.00	4
NS	17.00	18.00	1.00	9
NS	18.00	18.75	0.75	1
82-A 16	18.75	19.00	0.25	3
82-A 15	19.00	19.25	0.25	4
82-A 14	19.25	19.50	0.25	NS
82-A 13	19.50	19.75	0.25	NS
82-A 12	19.75	20.00	0.25	3
82-A 11	20.00	20.25	0.25	6
82-A 10	20.25	20.50	0.25	NS
82-A 9	20.50	20.75	0.25	9
82-A 8	20.75	21.00	0.25	3
82-A 7	21.00	21.25	0.25	3
82-A 6	21.25	21.50	0.25	3
82-A 5	21,50	21.75	0.25	3
82-A 4	21.75		0.25	3
82-A 3	22.00	22.25	0.25	2
82-A 2	22.25	22.50	0.25	2
82-A 1	22.50	22.75	0.25	2
82-A 25	22.75		0.25	>1000
82-A 24	23.00		0.40	132
82-A 23	23.40		0.40	56
82-A 22	23.80		0.40	56
82-A 21	24.20	24.60	0.40	35
82-A 20	24.60		0.40	6
82-A 19	25.00	25.40	0.40	2
82-A 18	25.40	25.80	0.40	2 2 2 2 2 2
82-A 17	25.80	26,20	0.40	2
82-A 16	26.20		0.40	2
82-A 15	26.60		0.40	2
82-A 41	27.00		0.30	2
82-A 40	27.30		0.30	<u></u>
82-A 39	27.60			2
82-A 38	27.90			
82-A 37	28.20			
82-A 36	28.50			8
82-A 35	28.80			5
82-A 34	29.10			
82-A 33	29.40			8
82-A 32	29.70			4
82-A 31	30.00			
82-A 30	30.30			
82-A 29	30.60			
82-A 28	30.90	31.20	0.30	5

Hill AFB
EPA Soil Sampling
Sample ID, Depth, and PID Reference

	145-1		Sample	
EPA Lab	Depth ft.	Depth ft.	Thickness	PID (ppm)
Sample ID	Тор	Bottom	(Feet)	No Sample
82-A 27	31.20	31.50	0.30	5
82-A 54	31.50	31.80	0.30	2
82-A 53	31.80	32.10	0.30	
82-A 52	32.10	32.40	0.30	5
82-A 51	32.40	32.70	0.30	8
82-A 50	32.70	33.00	0.30	6
82-A 49	33.00	33.30	0.30	8
82-A 48	33.30	33.60	0.30	6
82-A 47	33.60	33.90	0.30	4
82-A 46	33.90	34.20	0.30	9
82-A 45	34.20	34.50	0.30	10
82-A 44	34.50	34.80	0.30	8
82-A 43	34.80	35.10	0.30	3
82-A 42	35.10	35.40	0.30	3

Hill AFB EPA Soil Sampling Sample ID, Depth, and PID Reference

			Sample	
EPA Lab	Depth ft.	Depth ft.	Thickness	PID (ppm)
Sample ID		Bottom	(Feet)	No Sample
NS	0.00	1.00	1.00	2
NS	1.00	2.00	1.00	2
NS	2.00	3.00	1.00	2 2 1 2 2 2
NS	3.00	4.00	1.00	2
NS	4.00	5.00	1.00	1
NS	5.00	6.00	1.00	2
NS	6.00	7.00	1.00	2
NS	7.00	8.00	1.00	2
NS	8.00	9.00	1.00	
NS	9.00	10.00	1.00	2 2 2 2 2 3
NS	10.00	11.00	1.00	2
NS	11.00	12.00	1.00	2
NS	12.00	13.00	1.00	2
NS	13.00	14.00	1.00	3
NS	14.00	15.00	1.00	
NS	15.00	16.00	1.00	2
NS	16.00	17.00	1.00	0
NS_	17.00	18.00	1.00	0
NS	18.00	19.00	1.00	0
NS	19.00	20.00	1.00	
82B 12	20.00	20.30	0.30	2
82B 11	20.30	20.60	0.30	2
82B 10	20.60	20.90	0.30	2 2 3 2
82B 9	20.90	21.20	0.30	2
82B 8	21.20	21.50	0.30	
82B 7	21.50	21.80	0.30	1
82B 6	21.80	22.10	0.30	1
82B 5	22.10	22.40	0.30	1
82B 4	22.40	22.70	0.30	1
82B 2	22.70	23.00	0.30	1
82B 1	23.00	23.30	0.30	1
NS	23.30	23.60	0.30	NS NS
NS	23.60	23.90	0.30	NS
82B 24	23.90		0.20	2
82B 23	24.10	24.40	0.30	2
82B 22	24.40	24.70	0.30	2 · 2 2
82B 21	24.70		0.30	
82B 20	25.00			2
82B 19	25.30			2
82B_18	25.60			2
82B 17	25.90			2
82B 16	26.10			2
82B 15	26.40			2
82B 14	26.70			
82B 13	27.10			2
NS	27.40	27.80	0.40	NS

Hill AFB EPA Soil Sampling Sample ID, Depth, and PID Reference

			Sample	and the second
EPA Lab	Depth ft.	Depth ft.	Thickness	PID (ppm)
Sample ID	Тор	Bottom	(Feet)	No Sample
NS	0.00	1.00	1.00	0
NS	1.00	2.00	1.00	0
NS	2.00	3.00	1.00	0
NS	3.00	4.00	1.00	0
NS	4.00	5.00	1.00	6
NS	5.00	6.00	1.00	26
NS	6.00	7.00	1.00	31
NS	7.00	8.00	1.00	21
NS	8.00	9.00	1.00	11
NS	9.00	10.00	1.00	11
NS	10.00	11.00	1.00	14
NS	11.00	12.00	1.00	3
NS	12.00	13.00	1.00	1
82-C 2	13.00	13.60	0.60	NS
82-C 1	13.60	13.90	0.30	NS
82-C NS	13.90	14.10	0.20	NS
82-C NS	14.10		0.30	NS
82-C NS	14.40	14.80	0.40	NS
82-C NS	14.80	15.10	0.30	NS
82-C 12	15.10	15.40	0.30	1
82-C 11	15.40	15.70	0.30	1
82-C 10	15.70	16.00	0.30	1
82-C 9	16.00	16.30	0.30	1
82-C 8	16.30	16.60	0.30	
82-C 7	16.60	16.90	0.30	1
82-C 6	16.90	17.20	0.30	1
82-C 5	17.20	17.50	0.30	1
82-C 4	17.50		0.30	NS
82-C 3	17.80		0.30	NS
82-C NS	18.10		0.30	NS
82-C NS	18.40		0.30	NS
82-C NS	18.70		0.30	NS
82-C NS	19.00		0.30	NS
82-C NS	19.30		0.30	NS
82-C NS	19.60	19.90	0.30	NS
82-C 26	19.90	20.20	0.30	4
82-C 25	20.20			
82-C 24	20.50			
82-C 23	20.80			
82-C 22	21.10			
82-C 21	21.40			
82-C 20	21.55			
82-C 19	21.70			314
82-C 18	NS			NS
82-C 17	22.00			
82-C 16	22.10	·		
82-C 15	NS NS			
82-C 14	22.30			
82-C 13	22.60	22.90	0.30	4

Hill AFB EPA Soil Sampling Sample ID, Depth, and PID Reference

EPA Lab Sample ID	Depth ft. Top	Depth ft. Bottom	Sample Thickness (Feet)	PID (ppm) No Sample
82-C NS	22.90	23.20	0.30	NS
82-C NS	23.20	23.50	0.30	NS
82-C NS	23.50	23.80	0.30	NS
82-C NS	23.80	24.10	0.30	NS

Hill AFB EPA Soil Sampling Sample ID, Depth, and PID Reference

ſ			Sample	
EPA Lab	Depth ft.	Depth ft.	Thickness	PID (ppm)
Sample ID	Top	Bottom	(Feet)	No Sample
NS	0.00	1.00	1.00	0
NS	1.00	2.00	1.00	Ō
NS	2.00	3.00	1.00	0
NS	3.00	4.00	1.00	Ō
NS	4.00	5.00	1.00	Ö
NS	5.00	6.00	1.00	0
NS	6.00	7.00	1.00	0
NS	7.00	8.00	1.00	0
NS	8.00	9.00	1.00	0
NS	9.00	10.00	1.00	0
NS	10.00	11.00	1.00	0
NS	11.00	12.00	1.00	0
NS	12.00	13.00	1.00	0
NS	13.00	14.00	1.00	0
NS	14.00	15.00	1.00	0
NS	15.00	16.00	1.00	0
NS	16.00	17.00	1.00	0
NS	17.00	18.00	1.00	0
NS	18.00	19.00	1.00	0
NS	19.00	20.00	1.00	NS
82-D 11	20.00	20.30	0.30	0
82-D 10	20.30	20.60	0.30	0
82-D 9	20.60	20.90	0.30	1
82-D 8	20.90	21.20	0.30	1
82-D 7	21.20	21.50	0.30	1
82-D 6	21.50	21.80	0.30	1
82-D 5	21.80	22.10	0.30	1
82-D 4	22.10	22.40	0.30	199
82-D 3	22.40	22.80	0.40	17
82-D 2	22.80	23.80	1.00	3
82-D 1	23.80	24.00	0.20	
82-D 25	24.00	24.10	0.10	25
82-D 24	24.10	24.40	0.30	50
82-D 23	24.40	24.70	0.30	282
82-D 22	24.70	25.00	0.30	. 63
82-D 21	25.00	25.30	0.30	30
82-D 20	25.30	25.60	0.30	16
82-D 19	25.60			
82-D 18	25.90			
82-D 17	26.20	26.50	0.30	15
82-D 16	26.50	26.80	0.30	20
82-D 15	26.80	27.00	0.20	
82-D 14	27.00	27.30		
82-D 13	27.30			
82-D 12	27.60			
82-D NS	27.80			
82-D 40	28.00			
82-D 39	28.20			
82-D 38	28.50			12

Hill AFB
EPA Soil Sampling
Sample ID, Depth, and PID Reference

8 % 8 c c 2	8,44		Sample	- 4
EPA Lab	Depth ft.	Depth ft.	Thickness	PID (ppm)
Sample ID	Top	Bottom	(Feet)	No Sample
82-D 37	28.80	29.10	0.30	41
82-D 36	29.10	29.40	0.30	42
82-D 35	29.40	29.70	0.30	26
82-D 34	29.70	30.00	0.30	11
82-D 33	30.00	30.30	0.30	33
82-D 32	30.30	30.60	0.30	20
82-D 31	30.60	30.90	0.30	13
82-D 30	30.90	31.20	0.30	11
82-D 29	31.20	31.50	0.30	9
82-D 28	31.50	31.8Ū	0.30	4
82-D 27	31.80	32.10	0.30	1
82-D 26	32.10	32.40	0.30	3

Hill AFB EPA Soil Sampling Sample ID, Depth, and PID Reference

			Sample	
EPA Lab	Depth ft.	Depth ft.	Thickness	PID (ppm)
Sample ID	Top	Bottom	(Feet)	No Sample
82-E NS	0.00	0.30	0.30	
82-E 11	0.30	0.60	0.30	3.0
82-E 10	0.60	0.90	0.30	1.0
82-E 9	0.90	1.20	0.30	1.0
82-E 8	1.20	1.50	0.30	1.0
82-E 7	1.50	1.80	0.30	1.0
82-E 6	1.80	2.10	0.30	1.0
82-E 5	2.10 2.40	2.40	0.30	1.0
82-E 4	2.40	2.70	0.30	1.0
82-E 3	2.70	3.00	0.30	1.0
82-E 2	3.00	3.30	0.30	1.0
82-E 1	3.30	3.50	0.20	1.0
82-E 21	3.50	3.85	0.35	1.0
82-E 20	3.85	4.20	0.35	1.0
82-E 19	4.20	4.55	0.35	1.0
82-E 18	4.55	4.90	0.35	1.0
82-E 17	4.90	5.25	0.35	1.0
82-E 16	5.25	5.60	0.35	1.0
82-E 15	5.60	5.95	0.35	1.0
82-E 14	5.95	6.30	0.35	1.0
82-E 13	6.30	6.65	0.35	1.0
82-E 12	6.65	7.00	0.35	1.0
82-E 32	7.00	7.31	0.31	1.0
82-E 31	7.31	7.64	0.33	2.0
82-E 30	7.64	7.95 8.27	0.31	3.0
82-E 29	7.95	8.27	0.32	3.0
82-E 28	8.27	8.59	0.32	3.0 3.0
82-E 27	8.59	8.91	0.32	2.0 1.0
82-E 26	8.91	9.55	0.64	1.0
82-E 25	9.55	9.86	0.31	1.5
82-E 24	9.86	10.18	0.32	1.0
82-E 23	10.18	10.50	0.32	1.0

Hill AFB
EPA Soil Sampling
Sample ID, Depth, and PID Reference

			Sample	
EPA Lab	Depth ft.	Depts ft.	Thicknes	PID (ppm
Sample ID	Тор	Bottom	(Feet)	No Samp
82-I NS	0.00	1.00	1.00	NS
82-1 NS	1.00	2.00	1.00	0.0
82-1 NS	2.00	3.00	1.00	0.0
82-1 NS	3.00	4.00	1.00	1.0
82-1 NS	4.00	5.00	1.00	1.0
82-1 NS	5.00	6.00	1.00	1.0
82-I NS	6.00	7.00	1.00	1.0
82-1 NS	7.00	8.00	1.00	1.0
82-1 NS	8.00	9.00	1.00	2.0
82-I NS	9.00	10.00	1.00	3.0
82-1 NS	10.00	11.00	1.00	2.0
82-1 NS	11.00	12.00	1.00	3.0
82-I NS	12.00	13.00	1.00	3.0
82-I NS	13.00	13.80	0.80	2.0
82-I 14	13.80	14.00	0.20	3.0
82-1 13	14.00	14.40	0.40	3.0
82-1 12	14.40	14.80	0.40	2.0
82-l 11	14.80	15.20	0.40	0.0
82-1 10	15.20	15.56	0.36	4.0
82-1 9	15.56	15.92	0.36	4.0
82-1 8	15.92	16.28	0.36	6.0
82-1 7	16.28	16.64	0.36	13.0
82-1 6	16.64	17.00	0.36	81.0
82-1 5	17.00	17.36	0.36	257.0
82-1 4	17.36	17.72	0.36	181.0
82-1 3	17.72	18.08	0.36	137.0
82-1 2	18.08	18.44	0.36	150.0
82-I 1	18.44	18.80	0.36	143.0
82-1 27	18.80	19.12	0.32	397.0
82-1 26	19.12	19.45	0.33	301.0
82-1 25	19.45	19.77	0.32	136.0
82-1 24	19.77	20.09	0.32	176.0
82-1 23	20.09	20.42	0.33	78.0
82-1 22	20.42	20.74	0.32	87.0
82-I 21	20.74	21.06	0.32	79.0
82-1 20	21.06	21.38	0.32	95.0
82-I 19	21.38			103.0
82-1 18	21.71	22.03	0.32	298.0
82-1 17	22.03	22.35	0.32	357.0
82-1 16	22.35		0.33	293.0
82-1 15	22.68	23.00		270.0
82-1 39	23.00	23.20	0.20	255.0
82-1 38	23.20			145.0
82-1 37	23.40	23.76	0.36	330.0
82-1 36	23.76	24.12	0.36	239.0
82-1 35	24.12			74.0
82-1 34	24.48			68.0
82-1 33	24.84			
82-1 32	25.20			236.0

Hill AFB EPA Soil Sampling Sample ID, Depth, and PID Reference

EPA Lab Sample ID	Depth ft. Top	Depth ft. Bottom		PID (ppm No Samp
82-I 31	25.56	25.92	0.36	239.0
82-I 30	25.92	26.28	0.36	252.0
82-1 29	26.28	26.64	0.36	26.0
82-1 28	26.64	27.00	0.36	13.0



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Page 1 of 2
Part 1 of 1

Date	6-30.92	
Agency	Identification Number SC2=0429-BB	
Account	No. 03018	

James M. Montgomery Consulting Engineers 4525 Wasatch Blvd, Suite 200 Salt Lake City, UT 84124 Attention: Bob Glascott

Sampling Collection and Shipment

FAX (801) 272-0430 Telephone (801) 272-1900

	Sampling S	Site HA	FB			Date of	Collect	tion Ju	ne 18.	1992	
	Date Sampl	les Rec	eived a	t Labor	لد atory	une 19.	1992				
Λnalysis											
	Method of	Method of Analysis 8020MOD									
	Date(s) of	Date(s) of Analysis June 23, 1992 - June 24, 1992									
Analytical	Results										_
Field Semple Number	Laboratory Number	Sample Type	Benzene UG/G	Ethyl Benzene UG/G	Toluene UG/G	Xylene UG∕G	Naphthalene UG/G				
HF '1 1-11.5'	EL 2419	SOIL	ND.	0.12	.031	. 9 2	4.4				
* Limit of D	etection		.005	.005	.005	. 01	. 01				
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Analyst: Aythuy B. Clarke

Mary S. Clerke

Super A Mile

Laboratory Supervisor: Richard W. Wade



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					Date _		- 1// <u>E</u>	<u>: </u>			
							fication		592-042	29-AB	
4525 Wasa Salt Lake	Montgomery tch Blvd, S City, UT 8 : Bob Glasc	uite 2 34124	ting En 00	gineers			Te	FAX lephone		272-043 272-190	
Sampling (Collection a					Date of	f Collec	tion Jur	ne 18.	1992	
	Date Samp	les Rec	eived a	t Labor	atory _	lune 19	1992				
Analysis	Method of	Analys	is <u>DCL-</u>	TPHD							
	Date(s) of	f Analy	sis Jun	e 27. 1	992	<u> </u>					
Analytica	l Results										_
Field Sample Number	Laboratory Number	Sample Type	TPH-Jet Fuel mg/g								
HF/11-11.5°	EL 2419	SOIL	0.11	l	-			!			I
Limit of Det	ection		0.01	<u> </u>	<u> </u>		1				╀
						1					
ND Faramet	mment on last ter not detec ter not reque	ted.		See com Paramet							
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Page 1 of 2 Part 1 of 1

Date _	7-2892
Agency	Identification Number S92-0517-BC
Account	t No. <u>03018</u>

James M. Montgomery Consulting Engineers 4525 Wasatch Blvd, Suite 200 Salt Lake City, UT 84124 Attention: Bob Glascott

FAX (801) 272-0430 Telephone (801) 272-1900

Sampling (Collection a Sampling S		-			Date of	Collect	ion Ju	ne 29.	1992	
	Date Sampl	es Rec	eived a	t Labor	atory_	June 30.	1992				
Analysis	Method of	Analys	is <u>8020</u>	MOD							
	Date(s) of	Analy	sis July	y 22. 19	992						
Analytical	l Results										
Field Sample Number	Laboratory Number	Semple Type	Benzene 9/6/	Ethyl Benzene ug/g	Toluene vg/g	XY1ene rg/g	Naphthalene µ9/9				
2HF/17'-17.5	EL 2858	SOIL	.10	.18	.10	5.4	2.9				
7HF/17'-17.5	EL 2859	SOIL	10.	16.	23.	74.	6.6	<u> </u>		ļ	<u> </u>
Limit of Det	ection		.005	.005	.005	.01	.01				
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Analyst: Arthyr B. Clarke

· 1992

Reviewer: Lany Scarlan

Laboratory Supervisor: Richard W. Wade

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Page 1 of 2

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	Sampling C	Collection a		-			Date of	Collec	tion Ju	ine 29,	1992	
		Date Sampl	les Rec	eived a	t Labor	atory_	June 30,	1992				
	Analysis											
		Date(s) of	Analy	yluL sis	27, 1	992					 -	
	Analytical	Results										
? !		nigeriori il 11	-νεΩ -	TPH-Jet Fuel mg/g								
	2HF/17'-17.5 7HF/17'-17.5		SOIL	0.36		<u> </u>		-		 	ļ	+
	ND Paramet	ment on last er not detec	page.		See com	ment on	last pag					
					Re	viewer,	an y Supervi	-Br	nel	Y		

960 West LeVoy Drive / Salt Lake City, Utah 84123-2547 / (801) 266-7700 A Sorenson Company



Form ARF-AL

Page 1 of

Part 1 οf 1

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								-/ per <u>\$92-0</u>	427- AC	
				_	-	03018			<u> </u>	
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Sampling (Collection Sampling		pment FB		Date	of Coll	ection	June 17.	1992	
	Date Samp	les Rec	eived at L	aboratory	June	18. 1992	2			
Analysis	Method of	Analys	is DCL-TPH	D						
	Date(s) o	f Analy	sis <u>June</u> ?	1992		<u></u>				
Analytica:	l Results									
Field Sample Number	Laboratory Number	Sample Type	7PH-Jet Fuel mg/g							
HF/15.5'-16'		SOIL	0.02				_			\Box
HF/21'-21.5'		SOIL	ND*			- :				
* Limit of E	- tection		0.01			i				士
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	111 5 19	92		Reviewer	1	an	Bui	eh-		
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Account No. 03018

Form ARF-AL

Page 1 of 2 Part 1 of 1

Date _	6-25.92
Agency	Identification Number S92-0427-BC

James M. Montgomery Consulting Engineers 4525 Wasatch Blvd, Suite 200 Salt Lake City, UT 84124 Attention: Bob Glascott

FAX (801) 272-0430 Telephone (801) 272-1900

							T	'elephon	ie (801)	272-19	00
Sampling C	Collection of Sampling S	Site HA	FB					ction L	une 17.	1992	
Analysis	Date Sampl				atory 1	nue 18	_1992_				 -
	Method of	Analys	is <u>8020</u>	MOD							
	Date(s) of	E Analy	sis Jun	e_18,_19	992					·	
Analytical	Results										
Field Sample Number	Laboratory Number	Sample Type	Benzene UG/G	Ethyl Benzene UG/G	Toluene UG/G	Xylene UG/G	Naphthalene UG/G			5	
HF/15.5'-16'	EL 2415	SOIL	2.0	0.26	0.1,1	2.8	1.4	İ		1	1
HF/21'-21.5'	EL 2416	SOIL	. 009	ND.	ND.	ND.	. 0 5				
• Limit of D	etection		.005.	.005.	.005.	.01	.01				\mp

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Analyst: Arthur B. Clyrke

Reviewer:

Laboratory Supervisor: Richard W. Wade



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Page 1 of 2 Part 1 of 1

Date	7-7-	92
Agency	Identification	Number <u>\$92-0453-BB</u>
•	No. <u>03018</u>	

James M. Montgomery Consulting Engineers 4525 Wasatch Blvd, Suite 200 Salt Lake City, UT 84124 Attention: Bob Glascott

FAX (801) 272-0430 Telephone (801) 272-1900

Sampling C	Collection and Shipment Sampling Site <u>HAFR</u> Date of Collection <u>July 01, 1992</u>
	Sampling of the management of the sample of
	Date Samples Received at Laboratory July 02, 1992
Analysis	
	Method of Analysis 8020MOD
	Date(s) of Analysis July 06, 1992
Analytical	l Results

Field Sample Number	Laboratory Rusbor	Simple Type	Benzene UG/G	Ethyl Benzene UG/G	Toluene UG/G	VG/G	Naphthalene UG/G				
HF/59.5'-60'	EL 2578	SOIL	ND*	ND*	ND.	ND.	ND.	L			
· Limit of D			.005	.005	.005	.01	.01				
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JUL 10 1992

Analyst: Arthur B. Clarke

JAMES M. MONTGOMERY

Laboratory Supervisor: Richard W. Wade



Form ARF-AL

1 Page of 2 Part 1 of

Date 1/12/92	
Agency Identification	Number <u>S92-0453-AB</u>
Account No. 03018	

___ Date of Collection July 01, 1992

Sampling Site HAFR

James M. Montgomery Consulting Engineers 4525 Wasatch Blvd, Suite 200 Salt Lake City, UT 84124 Attention: Bob Glascott

Sampling Collection and Shipment

FAX (801) 272-0430 Telephone (801) 272-1900

Analysis											
·	Method of	Analys	is DCL-	TPHD							
	Date(s) o	f Analy	sis								
malytica	l Results				_						
Field Sample Number	Laboratory Number	Sample Type	TPH-Jet Puel mg/g								
/59.51-66	EL 2578	SOIL	ND*								
Limit of	Detection		0.01	 	 						
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JUL 1 4 1992

JAMES M. MONTGOMERY

Laboratory Supervisor:



Well Number	Sample Interval (ft bgs)	Benzene (ug/Kg)	Toluene (ug/Kg)	Ethyl Benzene (ug/Kg)	Xylene (ug/Kg)	TPH (mg/kg)
MW-1	16-17	150	129	57	318	<10.0
MW-1 /	18-19	564	145	341	2249	98.3
SB870A-02	15-16	43.2	_51.3	52.2	457.3	23.2
SB870A-02	17-18	13	60.2	57.7	509	37
SB870A-03	11-12	9400	115000	66700	634000	2790
SB870A-03	19-20	338	595	138	1143	<10.0
SB870A-03*	29-30	22200	187000	83100	744000	15100
MW-5	15.5-16	2000	110	260	2800	20
MW-6	21-21.5	9	<5	<5	<5	< 10.0
MW-8	11-11.5	<5	31	120	920	110
MW-9	17-17.5	100	100	180	5400	360
MW-1A**	17-17.5	10000	23000	16000	74000	1500
MW-1A**	59.5-60	<5	<5	_<5	< 10	<10

^{*} Duplicate of 19'-20'

ug/kg - Micrograms/kilogram mg/kg - Milligrams/kilogram ft bgs - feet below ground surface

b:todd

Client AFCEE - Hill AFFS
Proj. No. 5301.551
By Elect W. Date 7-26
Chkd. Acta Date 7-26
Revision

^{**} Well Abandoned



Well Number	Sample Interval (ft bgs)	Moisture %	USC Classification	Atterburg Limits	Permeability (cm/s)
MW-1	25.5-26	23.9	CL	Liquid Limit=28 Plastic Index=7	1.29 x 10 ⁻⁷
SB-3	15.5-16	NA	NA	NA	2.31 x 10 ⁻⁷
MW-5	31-31.5	29.1	CL	Liquid Limit=32 Plastic Index=10	
MW-6	30.5-31	23.9	ML	Non-plastic	2.03×10^{-6}

NA - Not analyzed

b:TODD1

Client AFCEE - (L.() AFB Proj. No. 530, 551 By Suntained Date 7-24 Chkd. Revision Date 7-24 Revision

Table 1. Quantitation Report for SR# SF-0-35.

Concentration = ppb

QC1123C 500 ppb	503	508	510	510	208	510	200	207	513	
TRIP BLANK	1	! !	1 1	1 1 1	! !	! !	! !	† 1	† 1	
EPA 82-1	2740	372	486	784	1370	1140	162	495	240	
Compound	Benzene	Toluene	Ethylbenzene	p-Xylene	m-Xylene	o-Xylene	1,3,5-Trimethylbenzene	1,2,4-Trimethylbenzene	1,2,3—Trimethylbenzene	

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Historiani Colored do mare

QC = Quality Control Standard

the as is the sose another. --- = Below Quantitation Limit (0.5 ppb)





(4)

(TABLE 2 (GROUND WATER SAMPLING ANALYSES

		Concent	ration, ppm		
Location	Benzene	Toluene	E-Benzene	Somb. Xyl.	PCE *
TP-01	0.741	2.273	·	1.027	0.425
TP-02	5.203	7.578	0.740	4.177	3.809
TP-03	2.701	3.112	0.322	1.655	2.447
TP-04					
TP-05					
TP-06					
TP-07	26.092	21.919	0.753	3.906	2.204
TP-08					
TP-09	0.992	2.128	0.173	0.301	1.269
TP-10	1.928	3.214		3.830	3.618
TP-11					
TP-12	1.163	0.565	0.062	0.265	0.636
TP-13		0.069		0.062	
TP-14	1.440	0.392	0.338	1.378	
TP-15					
TF-16					
TP-17			0.014	0.057	
TP-18					
TP-19	0.646		0.036	0.149	0.125
TP-20	0.124	2.699		0.504	0.303

= < 0.005

* Tetrachloroethylene

TERRA TECHNOLOGIES - SOUTHWEST, MIC.

TABLE 2 (CONTINUED GROUND WATER SAMPLING ANALYSES

(3)

		Concent	ration, ppm	(mg/l)	
Location	Benzene	Toluene	E-Benzene	Comb. Xyl.	PCE *
TP-21				0.057	
TP-22	0.056	0.090	0.022	0.104	
TP-23					
TP-24					
TP-25					
TP-26					
TP-27					
TP-28					
TP-29					
TP-30					•
TP-31					
TP-32					
TP-33					
TP-34					
TP-35	N/A	N/A	N/A	N/A	N/A
TP-36				0.052	
TP-37	0.789	0.930		4.179	2.525
TP-38					
TP-39					
TWP-01	0.520	1.271	0.085	0.173	0.795

= < 0.005

* Tetrachloroethylene

TABLE 2 (CONTINUED)

GROUND WATER SAMPLING ANALYSES

		Concent	ration, ppm	(mg/l)	
Location	Benzene	Toluene	E-Benzene	Comb. Xyl.	PCE *
SGS-01	0.161	12.645	0.046	0.295	
GWS-01	0.195	0.946	0.072	0.089	
GWS-02					<u></u>
MW-03	12.179	6.728		7.669	2.722
MW-07		-			

= < 0.005

* Tetrachloroethylene

•

TABLE 5
GROUNDWATER ANALYTICAL RESULTS

Analyte	MW870A-01	MW-570 (Duplicate)	CPT-42	CPT-43
BTEX (μg/L)		 -		
Benzene	305	222	<1.0	<1.0
Toluene	690	660	<1.0	<1.0
Ethylbenzene	132	102	<1.0	<1.0
Xylenes	2,303	2,396	<1.0	<1.0
TPH (mg/L)	11.9	7.5	<1.0	<1.0

μg/L Micrograms/liter mg/L Milligrams/liter -- Not analyzed

Water samples were analyzed according to EPA SW-846 Methods 8020/602 and 8015 Modified.

TABLE 6

GROUNDWATER ANALYTICAL RESULTS

Volatiles - Priority Pollutants	(LE1:)	MW-5 (µg/L)	of MW-5 (µg/L)	MW-10 µg/L)	MW-11 (μg/L)	MW-12 (µg/L)	10/1/92 (µg/L)	CPF-10 (µg/L)	CPT-14 (µg/L)
Chloromethane	17.	7	<100	<10	¢10	<10	<10	<10	<500,000
Vinyl Chloride	<009>	<100	<100	<10	<10	<10	<10	<10	<500,000
Bromomethane	<009>	<100	<100	<10	<10	<10	<10	<10	<500,000
Chloroethane	<500	<100	<100	<10	<10	<10	<10	<10	<500,000
Trichlorofluoromethane	250	<50	<50	\$, 5	\$	sē,	\$	<250,000
Acrolein	<6,000	<1,000	<1,000	<100	<100	<100	<100	<100	<1,000,000
1,1-Dichloroethene	2250	<50	<50	\$, 5	1 0	1 6	\$	<250,000
Methylene Chloride	2250	<50	<50	, 5	5	=	\$	ជ	<250,000
Acrylonitrile	<5,000	<1,000	<1,000	×100	<100	<100	<100	<100	<1,000,000
1,1-Dichloroethane	250	<50	~20	\$	~	\$	\$, S	<250,000
1,2-Dichloroethene (total)	~250	<50	<50	\$	~	\$, S	\$	<250,000
Chloroform	250	<50	<50	\$	\$ 5	\$	\$	\$	<250,000
1,1,1-Trichloroethane	250	<50	<50	\$	\$	\$, ,	¥9	<250,000
Carbon Tetrachloride	250	<50	<50	\$	\$	\$	Š.	\$	<250,000
Benzene	089	74	æ	\$	88	10	1 0	\$	<250,000
1,2-Dichloroethane	~ 250	<50	<50	\$	۸. ح	\$, S	, 5	<250,000
Trichloroethene	<250	0 9>	œ	\$	\$	~	, 5	\$	<250,000
1,2.Dichloropropane	<250	<50	<50	\$	~ 5	\$	\$	\$	<250,000
Bromodichloromethane	~ 250	<50	<50	\$, 55	\$, S	\$	<250,000
2-Chloroethylvinyl ether	<600	<100	<100	<10	<10	<10	<10	<10	<500,000
cis-1,3-Dichloropropene	250	<50	<50	\$	\$	\$	\$	\$	<250,000
* Toluene	*34J	<50	<50	17	ន	\$	\$	11	<250,000
trans-1,3-Dichloropropene	250	<50	<50	9	rč.	14	15	Ķ	250 000

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TABLE 6

GROUNDWATER ANALYTICAL RESULTS (CONTINUED)

Analyte Volatiles - Priority Pollutants	CPF-7 (µg/L)	MW-6 (µg/L)	MW-27 Blind Dup of MW-5 (μg/L)	MW-10 µg/L)	MW-11 (μg/L)	MW-12 (μ g/ L)	Trip Blank 10/1/92 (μg/L)	CPT-10 (µg/L)	CPT-14 (µg/L)
1,1,2.Trichloroethane	~250	<50	<50	76	\$	\$	\$	Ų	000 036
Tetrachloroethene	•<60J	ล	8	ıç,	\$ \$. . .	; .	; (000,000
Dibromochloromethane	~250	<50	<50	\$. .	; .) v(?	000,000
Chlorobenzene	<250	<20	<50	, 55	; . ç	; •{) *	9 4	000,000
* Ethylbenzene	1,400	991	951	. re	: 5	; g	; •	e :	000,062
Xylenes (Total)	5,700	006	98	110	: 25	a	3 4	e 5	1,400,000
Bromoform	<250	<50	<50	Ş	'	}	9 49	§ 4	13,000,000
1,1,2,2.Tetrachloroethane	•<50J	<50	8	Ŝ	\$; . .Ç) • 6	? *	000,000

μg/L J

Micrograms/liter Estimated value In an attempt to lower detection limits, a 1 ml aliquot was analyzed outside the holding time.

Water samples were analyzed according to EPA SW-846 Method 8240.

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TABLE 5

GROUNDWATER ANALYTICAL RESULTS

Analyte Voletilee - Organic Compounds	870-WS-1/32' (µg/L.)	870-WS-1/42' (µg/L.)	670-WS-1/42' 870-WS-1/92' 870-WS-2/40' (µg/L) (µg/L) µg/L)	870-WS-2/49° µg/L)	Blind Dup of 870-W8-2/49' (µg/L.)	870-WS-2/59' (µg/L.)	870-WS-2/69' (µg/L.)	CPT-40 (µg/L)	Trip Blank 11/23/93 (µg/L)
Chloromethane	<2.0	<20.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0
Vinyl Chloride	<2.0	<20.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0
Bromomethane	<2.0	<20.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0
Chloroethane	<2.0	<20.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0
Fluorotrichloromethane	<2.0	<20.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0
1,1-Dichlorvethene	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Dichloromethene	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	10.7
trans-1,2-Dichloroethene	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
1,1-Dichloroethane	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Chloroform	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
1,1,1-Trichloroethane	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Carbon Tetrachloride	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Benzene	17.4	30.6	27.0	8.4	6.5	24.0	43.5	<1.0	<1.0
1,2-Dichluroethane	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Trichloroethene (TCE)	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
1,2-Dichloropropane	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Bromodichloromethane	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
cis-1,3-Dichloropropene	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
trans-1,3-Dichloropropens	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Tolucae	1.8	113	69.3	13.8	7.8	68.0	711.7	<1.0	<1.0
Tetrachloroethene (PCE)	<1.0	<10.0	<1.0	<1.0	7	<1.0	<1.0	<1.0	<1.0
Chlorodibromomethane	<1.0	<10.0	<1.0	<1.0	√1. t	<1.0	<1.0	<1.0	<1.0
Chlorubenzene	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
* Ethylbenzene	<1.0	56.4	21.6	4.5	1.7	20.7	38.2	<1.0	<1.0
Bromoform	<2.0	<20.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0	<2.0
m.p.Xylene	4 .9	969	101	30.2	12.2	ক্ল	228	<1.0	<1.0
u-Xvlene/Styrene*	-	EUI.	36.4	9.6	9.4	93.7	63.6	<1.0	<1.0



GROUNDWATER ANALYTICAL RESULTS (CONTINUED)

Analyte Volatiles - Organic Compounds	870-WS-1/32' (µg/L.)	870-WS-1/42' (μg/L)	870-WS-1/42' 870-WS-1/92' 870-WS-2/49' (µg/L) (µg/L)	870.WS-2/49' µg/L)	MW-40 Blind Dup of 870-W8-249' (μg/L.)	870-WS-2/59° (µg/L.)	(hg/L) (hg/L)	CPT-40 (µg/L)	Trip Blank 11/23/93 (µg/L)
!									
1, 1, 2, 2-Tetrachloroethane	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	0.15	7
1.1.2-Trichloroethane	C 1	00[/	-	,	•			;	?
	?	V10.0	P: 17	0.1>	~1 .0	<1 .0	~1.0	<1.0	<1.0
1,2-Dichlorobenzene	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	5	•
1,3-Dichlorobenzene	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	0.12	, ,
1,4-Dichlorobenzene	<1.0	<10.0	<1.0	<1.0	<1.0	<1.0	<1.0	; ;	, ,

µg/L Micrograms/liter

Water samples were analyzed according to EPA Method 601/602.

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TABLE 5
GROUNDWATER ANALYTICAL RESULTS

Analyte Volatiles - Organic Compounds	CPT-7 (μ g/L)	SGS-1 (μ g/L)
1,1,2-Tri nloroethane (1,1,2-T)	<500	<5
1,1-Dichloroethylene (1,1DCE)	<500	<5
1,1-Dichloroethane	<500	<5
1,2-Dichlorobenzene	<500	<5
1,2-Dichloroethane	<500	<5
1,2-Dichloropropane	<500	<5
1,3-Dichlorobenzene	<500	<5
1,4-Dichlorobenzene (p-DCB)	<500	<5
2-Butanone (MEK)	<10,000	<100
2-Chloroethylvinylether	<1,000	<10
2-Hexanone	<10,000	<100
4-Methyl-2-Pentanone (MIBK)	<1,000	<10
Acetone	<1,000	<100
Acrolein	<1,000	<10
Acrylonitrile	<500	<10
Benzene	<500	7.3
cis-1,2-Dichloroethene	<500	<5
Chlorobenzene	<500	<5
cis-1,3-Dichloropropene	<500	<5
Bromoform	<500	<5
Chloroform (Trichloromethane)	<500	<5
Chloroethane	<1,000	<10
Carbon Disulfide	<500	<5
Carbon Tetrachloride	<500	<5
Dibromochloromethane	<500	<5
Dichlorobromomethane	<500	<5
Ethyl benzene	1,800	5.5
Methyl Bromide	<1,000	<10
Methyl Chloride	<1,000	<10
Methylene Chloride	<3,000	<30

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TABLE 5
GROUNDWATER ANALYTICAL RESULTS
(CONTINUED)

Analyte Volatiles - Organic Compounds	CPT-7 (μ g/ L)	SGS-1 (µ g/L)
m,p-Xylenes o-Xylene	4,600	8.8
o-Xylene	1,900	19
1,1,2,2-Tetrachloroethane	<500	<5
Tetrachloroethylene (PCE)	<500	18
Styrene	<500	<5
trans-1,2-Dichloroethene	<500	<5
1,1,1-Trichloroethane	<500	<5
Trichloroethylene (TCE)	<500	<5
Trichlorofluoromethane	<1,000	<10
trans-1,3-Dichloropropene	<500	<5
Tetrahydrofuran	<10,000	<100
Toluene	<500	<5
Vinyl Chloride (VC)	<1,000	<10
Vinyl Acetate	<10,000	<100

μg/L Micrograms/liter

All samples were analyzed according to EPA SW-846 Method 8240.

TABLE 5
GROUNDWATER ANALYTICAL RESULTS

Analyte Volatile Organic Compounds (TCL)	MW-6 (μg/L)	MW-7 (μg/L)	MW-27 Blind Dup of MW-7 (μg/L)
Chloromethane	<50	<10	<10
Vinyl Chloride	<50	<10	<10
Bromomethane	<50	<10	<10
Chloroethane	<50	<10	<10
1,1-Dichloroethene	<25	<5	<5
Acetone	<100	<20	<20
Carbon Disulfide	<25	<5	<5
Methylene Chloride	<25	<5	<5
1,1-Dichloroethane	<25	<5	<5
Vinyl Acetate	<25	<5	<5
2-Butanone	<100	<20	<20
1,2-Dichloroethene (total)	<25	<5	<5
Chloroform	<25	<5	<5
1,1,1-Trichloroethane	<25	<5	<5
Carbon Tetrachloride	<25	<5	<5
Benzene	<25	<5	<5
1,2-Dichloroethane	<25	<5	<5
Trichloroethene	<25	<5	<5
1,2-Dichloropropane	<25	<5	<5
Bromodichloromethane	<25	<5	<5
cis-1,3-Dichloropropene	<25	<5	<5
4-Methyl-2-Pentanone	<25	<10	<10
Toluene	<25	<5	<5
trans-1,3-Dichloropropene	<25	<5	<5
1,1,2-Trichloroethane	<25	<5	<5
Tetrachioroethene	<25	<5	<5
2-Hexanone	<50	<10	<10
Dibromochloromethane	<25	<5	<5
Chlorobenzene	<25	<5	<5
Ethybenzene	<25	<5	<5
Xylenes (total)	<25	<5	<5
Styrene	<25	<5	<5
Bromoform	<25	<5	<5
1,1,2,2-Tetrachloroethane	<25	<5	<5

μg/L Micrograms/liter

Water samples were analyzed according to EPA CLP.

TABLE 5
GROUNDWATER ANALYTICAL RESULTS

Analyte Semi-Volatiles (TCL)	MW-6 (μg/L)	MW-7 (µg/L)	MW-27 Blind Dup of MW-7 (μg/L)
N-Nitrosodimethylamine	<20	<20	<20
Phenol	<20	<20	<20
Bis (2-chloroethyl) ether	<20	<20	<20
2-Chlorophenol	<20	<20	<20
1,3-Dichlorobenzene	<20	<20	<20
1,4-Dichlorobenzene	<20	<20	<20
Benzyl Alcohol	<40	<40	<40
1,2-Dichlorobenzene	<20	<20	<20
2-Methylphenol	<20	<20	<20
Bis (2-chloroisopropyl) ether	<20	<20	<20
I-Methylphenol	<20	<20	<20
3- or 4-Methylphenol	<20	<20	<20
Hexachloroethane	<20	<20	<20
n-Nitrosodi-n-propylamine	<20	<20	<20
Nitrobenzene	<20	<20	<20
sophorone	<20	<20	<20
2,4-Dimethylphenol	<20	<20	<20
2-Nitrophenol	<20	<20	<20
Benzoic Acid	<100	<100	<100
Bis (2-chloroethoxy) methane	<20	<20	<20
2,4-Dichlorophenol	<20	<20	<20
1,2,4-Trichlorobenzene	<20	<20	<20
Naphthalene	<20	<20	<20
-Chloroaniline	<40	<40	<40
Hexachlorobutadiene	<20	<20	<20
4-Chloro-3-Methylphenol	<20	<20	<20
2-Methylnaphthalene	<20	<20	<20
Hexachlorocyclopentadiene	<20	<20	<20
2,4,6-Trichlorophenol	<20	<20	<20
2,4,5-Trichlorophenol	<20	<20	<20
2-Chloronaphthalene	<20	<20	<20
2-Nitroaniline	<100	<100	<100
2,6-Dinitrotoluene	<20	<20	<20
Acenaphthylene	<20	<20	<20
3-Nitroaniline	<100	<100	<100
2,4-Dinitrophenol	<100	<100	<100
Acenaphthene	<20	<20	<20
I-Nitrophenol	<100	<100	<100
2.4-Dinitrotoluene	<20	<20	<20
Dibenzofuran	<20	<20	<20
Diethylphthalate	<20	<20	<20
-Chlorophenyl phenyl ether	<20	<20	<20
Fluorene	<20	<20	<20

TABLE 5
GROUNDWATER ANALYTICAL RESULTS
(CONTINUED)

Analyte Semi-Volatiles (TCL)	MW-6 (μ g/L)	MW-7 (μg/L)	MW-27 blind dup. of MW-7 (µg/L)
4.35.	40		
4-Nitroaniline	<40	<40	<40
4,6-Dinitro-2-methylphenol	<100	<100	<100
n-Nitrosodiphenylamine	<20	<20	<20
4-Bromophenyl phenyl ether	<20	<20	<20
Hexachlorobenzene	<20	<20	<20
Pentachlorophenol	<100	<100	<100
Phenanthrene	<20	<20	<20
Anthracene	<20	<20	<20
Carbazole	<20	<20	<20
Di-n-butylphthalate	<20	<20	<20
Fluoranthene	<20	<20	<20
Pyrene	<20	<20	<20
Butylbenzylphthalate	<20	<20	<20
Bis (2-ethylhexyl) phthalate	<20	<20	<20
3,3'-Dichlorobenzidine	<40	<40	<40
Benzo (a) anthracene	<20	<20	<20
Chrysene	<20	<20	<20
Di-n-octyl phthalate	<20	<20	<20
Benzo (b) fluoranthene	<20	<20	<20
Benzo (k) fluoranthene	<20	<20	<20
Benzo (a) pyrene	<20	<20	<20
Indeno (1,2,3-c,d) pyrene	. <20	<20	<20
Dibenz (a,h) anthracene	<20	<20	<20
Benzo (g,h,i) perylene	<20	<20	<20

µg/L Micrograms/liter

Water samples were analyzed according to EPA CLP.

TABLE 5
GROUNDWATER ANALYTICAL RESULTS

Analyte Pesticides and PCBs (TCL)	MW-6 (μ g/L)	MW-7 (μg/L)	MW-27 Blind Dup of MW-7 (µg/L)
Alpha BHC	<0.10	<0.10	<0.10
Beta BHC	<0.10	<0.10	<0.10
Delta BHC	<0.10	<0.10	<0.10
Gamma BHC - Lindane	<0.10	<0.10	<0.10
Heptachlor	<0.10	<0.10	<0.10
Aldrin	<0.10	<0.10	<0.10
Heptachlor Epoxide	<0.10	<0.10	<0.10
Endosulfan I	<0.10	<0.10	<0.10
Dieldrin	<0.10	<0.10	<0.10
p,p'-DDE	<0.10	<0.10	<0.10
Endrin	<0.10	<0.10	<0.10
Endosulfan II	<0.10	<0.10	<0.10
p,p'-DDD	<0.10	<0.10	<0.10
Endosulfan Sulfate	<0.10	<0.10	<0.10
p,p'-DDT	<0.10	<0.10	<0.10
Endrin ketone	<0.10	<0.10	<0.10
alpha-Chlordane	<0.10	<0.10	<0.10
gamma-Chlordane	<0.10	<0.10	<0.10
Methoxychlor	<0.50	<0.50	<0.50
Toxaphene	<1.0	<1.0	<1.0
Aroclor-1016	<1.0	<1.0	<1.0
Aroclor-1221	<1.0	<1.0	<1.0
Aroclor-1232	<1.0	<1.0	<1.0
Aroclor-1242	<1.0	<1.0	<1.0
Aroclor-1248	<1.0	<1.0	<1.0
Aroclor-1254	<1.0	<1.0	<1.0
Aroclor-1260	<1.0	<1.0	<1.0

μg/L Micrograms/liter

Water samples were analyzed according to EPA SW-846 Method 8081

TABLE 5
GROUNDWATER ANALYTICAL RESULTS

nalyte - Metals (TCL)	MW-6 (mg/L)	MW-7 (mg/L)	MW-27 Blind Dup of MW-7 (mg/L)
ıminum	1.43	33.6	26.1
timony	<0.25	<0.25	<0.25
senic	<0.010	<0.010	<0.010
rium	0.71	0.20	0.19
yllium	<0.005	<0.005	<0.005
dmium	<0.005	<0.005	<0.005
cium	4.2	267	225
romium	<0.05	0.13	0.07
palt	<0.05	0.05	0.05
per	0.02	0.07	0.05
•	1.43	75.4	67.8
d	<0.05	<0.04	< 0.04
gnesium	84	55	45
nganese	1.62	1.36	1.13
reury	<0.0005	<0.005	<0.005
kel	<0.04	0.05	0.05
assium	3.95	0.509	0.513
enium	0.008	<0.005	< 0.005
/er	<0.01	<0.01	<0.01
ium	703	456	455
ıllium	<0.1	<0.003	<0.002
nadium	0.07	0.25	0.15
c	0.06	0.29	0.23
ınide	<0.005	<0.005	<0.005

^{&#}x27;L Milligrams/liter

v. fer samples were analyzed according to EPA CLP.

SOIL ANALYTICAL RESULTS

Mary Charles

			9.1	Soil Boring and Sample Depth	Sample Dept	` \	(/	•	
Analyte	MW-1 (16'-17')	MW-1 (18'-19')	SB870A-02 (15'-16')	SB870A-02 (17'-18')	SB870A-03 (11'-12')	SB670A-03 (19'-20')	SB870A.03 (29'-30') (Duplicate) of 19'-20')	Trip Blank (Water) 11/7/92 (µg/L)	rank 22 C
BTEX (µg/kg)					-				
Benzene	150	264	43.2	13.0	9,400	338	22,200		
Toluene	621	145	51.3	60.2	115,000	595	187.000	7	
Ethylbenzene	67.0	341	52.2	57.7	002'99	138	83,100	7	
Xylenes	318	2,249	457.3	203	634,000	1.143	744 000		
TPH (mg/kg)	<10.0	98.3	23.2	37.0	2,790	<10.0	15.100	7	
Total Organic Carbon (mg/kg)	:	;	:	:	;	1,100		; +	
Moisture (%)	21.9	19.4	18.9	24.2	7.3	20.3	14.0		
								-	

Micrograms/kilogram Milligrams/kilogram Micrograms/liter Not analyzed mg/kg µg/kg

Soil Samples were analyzed according to EPA SW-846 Methods 8020 and 8015 Modified.

BITEX TON H. Heel

10 mm - 2





TABLE 3

SOIL ANALYTICAL RESULTS (CONTINUED)

	4							,	
				Soil Bor	Soil Boring and Sample Depth	ple Depth			
	MW-6 M (15.5'-16') (21'	MW-6 (21'-21.5')	Trip Blank (Water)	MW-8 (11'-11.5')	Trip Blank (Water)	MW-9 (17'-17.5')	MW-1A (17'-17.6')	Trip Blank (Water)	MW-1A (59.5'-60')
Analyte			6/17/β2 (μg/L)		6/18/02 (Hg/L)		Abandoned	6/29/92	Abandoned
BTEX&N (µg/g)									
Benzene	2.0	0.009	<1.0	<0.005	<1.0	0.10	10	<1.0	<0.009
Toluene	0.11	<0.005	<1. 0	0.031	*	0.10	ន	<1.0	<0.005
/ Ethylbenzene	0.26	<0.005	<1.0	0.12	912	0.18	16	<1.0	<0.005
Xylenes	2.8	<0.005	ж. 13	0.92	5,5	5.4	74	6.2	<0.01
Naphthelene	1.4	0.05	<5.0	4.4	<5.0 <	2.9	9.9	~ \$>	<0.01
TPH (mg/g)	0.03	<0.01	-;	0.11	:	0.36	1.5	·:	<0.01

μg/g Micrograms/gram mg/g Milligrams/gram μg/L Micrograms/liter ... Not analyzed Soil Samples were analyzed according to EPA SW-846 Methods 8020 and 8015 Modified.

m5/Kg

TABLE 4
GEOTECHNICAL RESULTS

•	1		Sample ID an	d Sample Depth	
	Geotechnical Characteristic	MW-1 (25.5'-26')	SB-3 (15.5'-16')	MW-5 (31'-31.5')	MW-6 (30.5'-31')
	Moisture (%)	23.9	NA	29.1	23.9
	USC Classification	CL	NA	CL	ML
Ź	Atterburg Limits	Liquid Limit=28 Plastic Index=7	NA .	Liquid Limit=32 Plastic Index=10	Non-plastic
	Permeability (cm/s)	1.29 x 10 ⁻⁷	2.31 x 10 ⁻⁷	1.78 x 10-7	2.03 x 10 ⁻⁶

NA Not analyzed

Man

		Field D	Field Data Hill	Air Force base,	base, Utah	ah		
Sample	Date	Нď	Cond	Temp °C	Redox	Total Alk	cl mg/l	Ferrous Iron
71-29CPT-Geo Depth 1	8-2-93	7.1	1604	25	66	457	220	<u> </u>
.71-19CPT-Geo Depth 1	8-2-93	7.1	1196	25	-63	/ 219	~ LT	9.
71-29CPT-Geo Depth 2	8-2-93	7.4	1256	22.5	-137	452	801	<.05
71-38CPT-Geo Depth 2	8-3-93	7.3	1628	18	56	646	168	<.05
71-17CPT-Geo Depth 1	8-3-93	7.3	1127	24	135	384	78	<.05
71-17CPT-Geo Depth 2	8-3-93	7.3	1495	22	-10	451	192	.2
71-31CPT-Geo Depth 1	8-3-93	7.3	1099	25	162	394	76	τ.
71-31CPT-Geo Depth 2	8-3-93	7.3	1082	23	152	378	75	<.05
71-18CPT-Geo Depth 1	8-3-93	Not enough	gh sample	for field	d data		•	.2
71-18CPT-Geo Depth 2	8-3-93	7.4	1151	20	180	440	84	<.05
71-23CPT-Geo Depth 1	8-5-93	7.4	1451	19	274	632	86	1.
71-39CPT-Geo Depth 1	8-5-93	7.7	1525	21	179	592	174	.05
71-39CPT-Geo Depth 2	8-5-93	8.3	1321	24	207	451	100	<.05

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71-29611-600	Dotal	8.243		1604	25	95	457	550	۷.0
71-19 CPT - Geo 0	roth 1	7.2.93	7.1	1196	52	-63	612	. 17_	1.6
71- 39 CPT 6.0 (Depth 2	8.2.93	7. ץ	125%	22.5	-137	452	108	4.05
1-38 CPT-GeD	- Dofa1	8-3-93	2.3	1628	/8	56	646	168	4.05
71-1747 -60	Doja 7	8-3-13	7.3	1137	24	135	384	! 78	4.05
71-17CPT-610	Dro/A2	8-3-43	7.3	1495	: 22	-10	: पुर	192	.2
1-316pT- GeO		8-3-13	7.3	1099	25	162	394	94	• • •
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11-31 CP7-600	•	8-3-53	7.3	1082	23	152		75	∠.05
71-18 CPT - Ge	و الموق و	8-3-93	- Not e	wought s	ample for	f:cld	24/4	+	1 .2
71-18CP7- GC	- Dofna	8-343	7.4	1151	20	180	440	84	2.03
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1- 39 CPT -6:0	Defni	8-5-93	7.7	1525	21	179	592	174	.65
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,	Water Level Ft'	25.52	28.60	5.10	22.08	24.98	6.20	23.76	4.88	11.16		
	Ferrous Iron	.2	<.05	<.05	2.1	<.05	<.05	.4	<.05	<.05		
Phase 2	cl mg/l	<i>/</i> 17	43	163	160	158	09	190	08	141		
	11	>										
Utah,	Total Alk	543	518	576	745	450	550	959	349	485		
cr Base,	Redox	/ 99	125	170	-125	213	243	40	192	190		
.1 Air Forcr	Well Temp °C	14.8	15.4	16.5	15.5	16.9	22.6	15.9	22.8	18.0		
eld Data Hill Air	ConD	1209 /	1162	1677	1828	1421	1275	2520	1042	1400		
Field	нд	7.0 🗸	7.1	7.2	6.9	6.9	7.5	7.3	7.3	7.1		
	Date	8/18/93	8/18/93	8/19/93	8/20/93	8/20/93	8/21/93	8/21/93	8/22/93	8/22/93		
`	Sample	82 MW- 11	82 MW- 10	82 A	82 C	82 B	82 F	82 D	82 E	82 н		

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		Field Data	ld Dat	a Hill	Air For	Field Data Hill Air Forcr Base,	Utah, Pha	Phase 2		
Sample	Date	ਸ਼ੁਰ	ConD	Well Temp °C	Redox mill- volts	Total Alka- linity mg/l	C1 mg/l	Ferrous Iron mg/l	D.O.	Depth to Water Sevel
MW-11	8/18/93	7.0 ~	1209	14.8	99	543	41	.2	0.1	Ft' 25.52
MW-10	8/18/93	7.1	1162	15.4	125	518	43	<.05	9.0	28.60
82 A	8/19/93	7.2	1677	16.5	170	916	163	<.05	0.4	5.10
82 C	8/20/93	6.9	1828	15.5	-125	745	091	2.1	0.5	22.08
82 B	8/20/93	6.9	1421	16.9	213	450	158	<.05	1.0	24.98
82 14	8/21/93	7.5	1275	22.6	243	550	09	<.05	1.1	6.20
82 D	8/21/93	7.3	2520	15.9	40	959	190	4.	1.3	23.76
82 E	8/22/93	7.3	1042	22.8	192	349	08	<.05	5.6	4.88
82 н	8/22/93	7.1	1400	18.0	190	485	141	<.05	6.3	11.16

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Hill AFB Monitoring Well Samples

	191							
Locatio	Date	PH	D.O.	Temp.	Depth To	Fet2		
	T		mg/	6.	feet	<u>1918</u>		
82 A	"I dia 2	<u>י</u>	0.3	14 6	4.46	7	:	
DE M	و معلوم الس				%. 7.b _	<u></u>	•	
82 B	11/8/93	_7.5	1.2	12.9	25.37	0.11		• ••
82 C	11/9/93	· ·	0.4	111 0	22 12	- A & N	. .	
r.	•	•	_0.4	-17. -	22.17	- See 3	<u> </u>	name washing of the second of
820	11/9/93	7.2	0.8	14.1	23,72	1.7_		
52 E	11/8/93	<u> </u>	2.7		6,26		: 	•• · · ·
**************************************	.4/4/73							
82F	11/7/93	7.6	.1.1	16.8	7.30	0.04	 · . i	
<u> </u>		<u>'</u>	· · · · · · · · · · · · · · · · · · ·	150		4 10	ļ	
82.H.	11/3/47	<u></u>	5.4	15.7	11.46	<u> </u>	 	.
MW-10	11/9/93	7,4	1.5	15.0	28.05	0.22	<u>.</u>	
!!		! : _	·	:	:	1	<u> </u>	
MW-11	11/9/93	7.4	0.1	14.7_	25.74	0,05	!	
1	:	<u></u> -	-	<u> </u>	:	!		
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FUEL CARBON		4 %	4 2	٧×	¥	£	£	욷	8.13E+00	2.10E+03	2.47E+03	£	g	£	£	2.08E+03	1.805+04	£	××	¥	4 %
1,2,3-TMB		9.57E+01	4.67E+01	5.00E+01	£	£	£	£	ę	1.20E+02	8.88E+01	g	g	4.68E+02	£	6.93E+01	6.07E+02	ę	239E+00	4.82E+01	5.00E+01
1,2,4-TMB		9.49E+01	4.82E+01	5.00E+01	£	£	£	£	1.43E+00	3.24E+02	1,83E+02	£	£	4.71E+02	£	1.65E+02	8.28E+02	B	2.25E+00	4.95E+01	5.00B+01
1,3,5-TIMB		9.49E+01	4.57E+01	5.00E+01	£	£	£	£	1.06E+00	2.38E+02	1.29E+02	£	£	4.79B+02	£	7.18E+01	S.75E+02	£	2.47B+00	4.74E+01	5.00E+01
o-XYLENE		9.69E+01	4.98E+01	5.00E+01	£	£	£	£	2	2.62E+00	1.03E+02	£	Ę	4.75E+02	£	2.04E+02	1.28E+03	Ę	2.43E+00	S.09E+01	5.00E+01
B-XYLENE		9.78E+01	4.84E+01	5.00E+01	£	2	£	ę	£	4.72E+01	3.83E+02	£	£	4.79E+02	£	6.35E+02	2.47E+03	Ę	1.93B+00	4.89E+01	5.00E+01
PXYLENE		9.78E+01	4.79E+01	5.00E+01	ę	2	2	£	2	4.28E+01	1.49E+02	£	£	4.75E+02	Ę	2.30E+02	4.01E+02	£	2.69E+00	4.88E+01	5.00E+01
ETHYL BENZENE	,	9.95E+01	5.18E+01	5.00E+01	Ę	Ę	Ę	£	9	2.65E+01	1.47E+02	Ę	2	4.79E+02	£	1.39E+02	4.43E+02	QX.	3.12E+00	5.27E+01	5.00E+01
TOLUENE		1.018402	\$ 30P.01	\$ 00P+01	Ę	9	2	Ę	4 20 Page	3.135+00	1.04E+01	Ę	9	4.76E+02	Ę	9.03E+01	2.90E+02	Ę	2.09E+00	5.29E+01	5.00E+01
RENZENE		1 mam	10.871.5	10.800	5	2 5	2 5	9	9	4 97 11.00	0 587.01	2	Ę	4.73E+02	Ę	- 3.36F±02	١٤٠	Ę	2.30E+00	5.24E+01	5.00E+01
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Almt in total

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None Detected; * Lower Limit of Quantitation = 10 ppb

Units - nothel Analysis L. S - 1-3/L

d	SAMPLENAME	BENZENE	TOLUENE	ETHYLBENZENE	P-XYLENE	m-XYLENE	O-XYLENE	1.3.6-TMB	12.4.TM	ant.	Š
8										1,6,0	
0Z	100 PPB	1.01E+02	1.01E+02	1.01E+02	1.01F+02	1.015.00	. P		1		
81	OC, OBSERVED, PPB	4.83E+01	4.93E+01	4.05E+01	5015,01	104E.0:	1.001	1.015+02	1.01E+02	1.00E+02	ş
Σ	OC, TRUE VALUE, PPB	\$.00E+01	5.00E+01	100 H			4.84CH	4.775.01	6.14E+01	4.90E+01	4 2
88	₩24	S	ā		10+300.0	5.00=401	5.00E+01	5.00E+01	5.00E+01	5.00F+01	X
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	140	1.74E+02	4.64E+00	3.08E+01	1.41EAD	2 02E.02	200		5+060.0	6.41E+01	18E1
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	44.10	7.44E.m	A 205.04		200	2	2	9.42E-01	E O	910	2
;	III.MM	1.05/2.00	AREA	1.00c+UK	1.65E+02	1.09E+03	5.05E+02	1.746+02	2.97E+02	2.12E.02	7 626.7
0	GC LAB BLANK PPR	Ş			K-SOE+OI	2.21E+02	8,84E+01	3.00E+01	5.67E+01	2.87E+01	0 2KE
	500 PPB	AYEAS	4 70E .	£ .	2	2	5	ş	£	2	N/A
	OC DASFRACA DOG	A 100 A	304303.F	4.07E+02	4.67E+02	4.68E+02	4.74E+02	4.73E.00	4 75Fam	4 B1E.m	
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	SO, INDE VALCE, Pro	A BOC+01	5.00E+01	5.00E+01	5.00E+01	5 00E+01	\$ 00E.01			- NO.	\$
		1.00E+01	1.00E+01	1.02E+01	9.88E+00	DRIFTON	00000	0.000	A.005+01	5.00E+01	¥
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ND = None Detected; NVA = Not Analyzad; BLQ = Below Limit of Quantitation, 1 ppb

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FUEL CARBOI	XX XX XX XX XX XX XX XX XX XX XX XX XX
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MESTIYLENE PSEUDOCUMENE	ND \$1.3E+00 \$1.0E+01 \$1.37E+02 \$1.37E+02 ND ND ND ND ND ND ND ND ND ND
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o-XYLENB	ND 9-498-00 5-698-00 5-698-00 5-698-00 5-698-00 5-698-00 ND ND ND ND ND ND ND ND ND ND ND ND ND
B-XYLENB	ND 9.118-00 4.846401 5.008-01 2.738-03 ND ND ND ND ND ND ND ND ND ND
P-XYLENB	ND 4.828-61 5.008-62 ND ND ND ND ND ND ND ND ND ND ND ND ND
BTHYLBENZENB P-XYLENB	ND 9.498400 5.148401 4.618402 ND ND ND ND ND ND ND ND ND ND ND ND ND
TOLUENB	ND 9.208400 4.918401 81.0 ND ND ND ND ND ND ND ND ND ND
BENZENB	ND 4.658401 5.008401 5.008401 5.008401 ND ND ND ND ND ND ND ND ND ND ND ND ND
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ND-Mone Detected; BLQ-Below Limit of Ousnitistion, 1 ppb; *BLQ-4 ppb; NA - Not Analyznd

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Page 1 of 1

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B FUEL CARBON	V V V V V V V V V V V V V V V V V V V
1,23-7368	4.35E-01 5.00E-01 1.89E-00
124-TMB	4.62E+01 5.00E+01 1.88E+00
13,5-71/09	4.32B+01 5.00B+01 1.99B+00
o-XYLENE	4.67E+01 5.00E+01 1.99E+00
m-XYLENE	4.27E+01 5.00E+01 1.84E+00
PXYLENE	4.45E+01 5.00E+01 2.27E+00
ETHYLBENZENE	4.87E+01 5.00E+01 2.13E+00
TOLUENE	4.56B+01 5.00E+01 1.77E+00
BENZENE TOLUENE	4.52E+01 5.00E+01 1.79E+00
SAMPLENAME	QC, OBSERVED, PPB QC, TRUE VALUE, PPB 2 PPB

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ND = None Detected; *Lower Limit of Quantitation = 2 ppb; N/A = Not Analyzed

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March 2, 1994

Ogden Air Logistics Center Environmental Management Directorate OO-ALC/EMR, Building 5 7274 Wardleigh Road Hill Air Force Base, Utah 84056

ATTN:

Mr. Andrew Gemperline

Technical Project Manager

PROJECT:

December 1993/January 1994

Quarterly Ground-Water Sampling Letter

Report Contract No. F42650-92-D-0005, Delivery Order 5019

Project No.: 2208.0682

Dear Andrew:

The purpose of this letter report is to briefly summarize the recent quarterly ground-water sampling event. This work involved sampling 11 monitoring wells and collecting two blind duplicate samples; see Figure 1 for the location of wells located at Site 870 (MW-1, MW-2, MW-3, MW-4, MW-5, MW-6, MW-7, MW-8, MW-9, MW-13, and MW-14). The sampling was initially conducted over the period of December 16 to 21, 1993, however, due to unforeseen sampling and laboratory mistakes 7 of the 11 monitoring wells needed to be resampled for benzene, toluene, ethylbenzene, xylenes, and naphthalene (BTEXN). The seven wells (MW-1, MW-2, MW-3, MW-4, MW-5, MW-6, and MW-8) were then resampled over the period of January 27 and 28, 1994. Monitoring wells MW-10 and MW-11 were sampled in October 1993 as part of the Natural Attenuation Study. All ground-water sampling was conducted according to the methods outlined in the Draft Final Treatability Study Work Plan (Montgomery, 1993).

The analytical data from this and previous sampling events are summarized in Table 1, copies of all laboratory data reports are provided in Attachment A. All 11 wells sampled during the quarterly sampling were analyzed for; BTEXN, 1,2,4-Trimethylbenzene (TMB), 1,3,5-TMB, sulfate, nitrate, nitrite, iron, and dissolved methane. The samples collected for dissolved methane were analyzed by the United States Environmental Protection Agency Robert S. Kerr Environmental Research Lab.

The results of the quarterly ground-water sampling and previous sampling events for benzene are shown in Figure 2. The benzene data have been plotted because benzene is typically the fuel component that guides regulatory compliance. Over time, the figure may allow for trends to be identified related to the concentration of benzene.

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Ogden Air Logistics Center March 2, 1994 Page 2



We appreciate the opportunity to work on this project for the Air Force. Please do not hesitate to call us if you have questions or comments regarding this report, or any other aspect of the work at Site 870.

Very truly yours,

MONTGOMERY WATSON

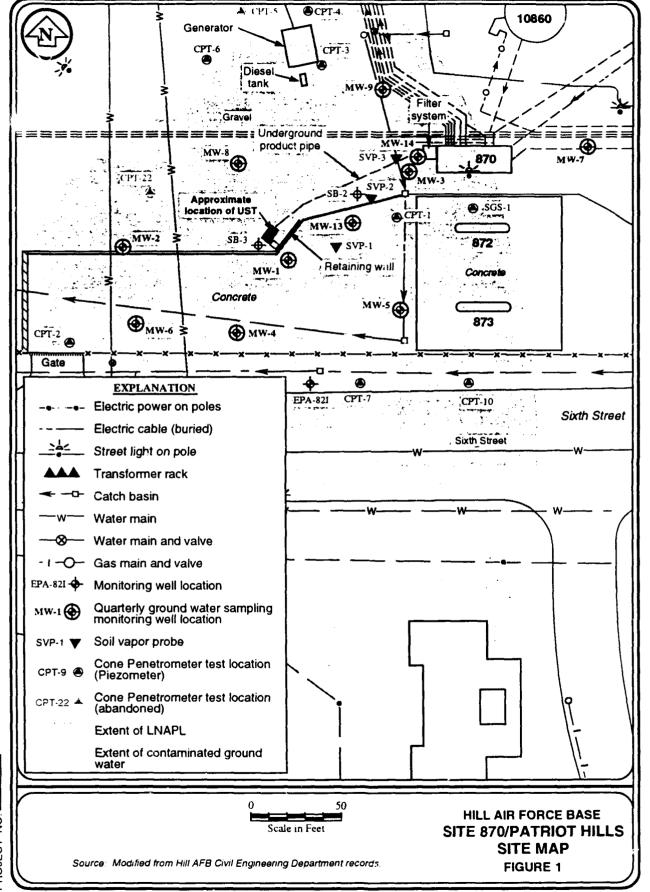
Robert Glascott
Project Geologist

David Fulton, P.G. Project Manager

/pa

Enclosures

cc: Bill Helms, PKOE



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PROJECT NO. 2208.0682

SITE 870/PATRIOT HILLS GROUND-WATER SAMPLING RESULTS FOR MONITORING WELLS MW-1 THROUGH MW-14

TABLE 1

	W	MW-1	MW-2	M	MW-3	MW-4	M	MW-S	W	MW-6
Analytes	Sampled 11/18/91	Sampled 12/93 - 1/94	Sampled 12/93 - 1/94	Sampled 10/92	Sampled 12/93 - 1/94	Sampled 12/93 - 1/94	Sampled 9/92	Sampled 12/93 - 1/94	Sampled 9/92	Sampled 12/93 - 1/94
Iron (mg/l)	¥ Z	10.8	50.5	¥Z	8.2	13.6	¥	6.41	¥	10.3
Nitrate (mg/l)	Ϋ́	<0.05	0.25	Y Z	<0.05	1.68	ž	<0.05	×	0.04
Nitrite (mg/l)	X A	<0.01	<0.01	¥ Z	0.025	0.637	₹ Z	<0.01	¥ X	0.031
Sulfate (mg/l)	Y Y	2	40	¥ Z	4	4	Y Y	7	Š	21
Methane (mg/l)	₹ Z	4	⊽	۲	459	12	₹ Z	2,040	∢ Z	4
1,2,4-Trimethylbenzene (µg/l)	A A	089	750	Y Z	1,000	1,500	¥ X	96	¥ X	1,500
1,3,5-Trimethylbenzene (µg/l)	Y X	330	350	۲ ۲	480	550	¥ X	450	ž	650
Benzene (µg/l)	305	475	51	12.18	2,320	930	74	416	<25	24.5
Toluene (µg/l)	069	88	56.3	6.73	1,300	1,830	<50	250	\$	10.1
Ethylbenzene (µg/l)	132	183	73.3	7	376	450	091	246	425	18.6
Xylenes (μg/l)	2,283	1,160	176	19.1	5,470	5,120	006	2,508	\$2	155.9
Naphthalene (µg/l)	¥ Z	76	88	Y V	<100	<100	X X	×100	ž	66

NA Not analyzed mg/l Miligrams per liter µg/l Micrograms per liter

Iron analyzed by EPA Method SW-846-6010 Nitrate/nitrite analyzed by EPA Method 353.3 Sulfate analyzed by EPA Method 375.4

1.2.4- and 1.3.5-Trimethylbenzene analyzed accoording to EPA Method 524.2

All monitoring wells were analyzed for BTEXN according to EPA Method SW846-8020

Methane was analyzed using the methods described in "Dissolved Oxygen & Methane in Water by a GC Headspace Equilibration Technique" by Kambell et. al. in International Journal of Environmental Analytical Chemistry, Volume 36, pp. 249-257.

SITE 870/PATRIOT HILLS GROUND-WATER SAMPLING RESULTS FOR MONITORING WELLS MW-1 THROUGH MW-14 (CONTINUED) TABLE 1

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	M	MW-7	MW-8	MW-9		MW-10		MW-11	11-	MW-12
Analytes	Sampled 9/92	Sampled 12/93 - 1/94	Sampled 12/93 - 1/94	Sampled 12/93 - 1/94	Sampled 10/92	Sampled 10/92	Sampled 8/93	Sampled 8/93	Sampled 9/93	Sampled 10/92
Iron (mg/l)	¥ Z	1.36	5.22	2.07	A A	¥ X	¥ X	0.2	ž	ž
Nitrate (mg/l)	X Y	11.78	0.28	0.4	٧	¥ Z	¥ Z	¥Z	Y	۷ Z
Nitrite (mg/l)	A A	0.021	<0.01	0.577	٧	₹ Z	¥ Z	¥ Z	۷ Z	۲ ۲
Sulfate (mg/l)	N A	56	Ξ	22	Y Y	N A	A A	86	∢ Z	Ž
Methane (mg/l)	¥ Z	⊽	9	9	۷ Z	¥ Z	ď Z	0.117	¥	Š Z
1.2,4-Trimethylbenzene (µg/l)	¥ Z	⊽	280	650	¥ Z	¥ Z	828	165	¥ Z	¥ Z
1,3,5-Trimethylbenzene (µg/l)	Y Y	⊽	140	150	٧ ٧	∢ Z	575	71.8	₹	۷ Z
Benzene (µg/l)	\$	⊽	18.6	72	1.16	۵	<10	336	56	۵
Toluene (µg/l)	D	⊽	10.8	27	0.57	17	290	90.3	33	۵
Ethylbenzene (µg/l)	\$	⊽	29.3	35	90:0	۵	443	139	21	53
Xylenes (μg/l)	۵	~	314.4	558	0.27	110	4,151	1,069	180	300
Naphthalene (µg/l)	Y Z	\$	294	865	۷ ۲	Y Y	ž	¥ Z	× Z	₹

Not analyzed

1 Milligrams per liter

Micrograms per liter A M Preservation

Iron analyzed by EPA Method SW-846-6010

Nitrate/nitrite analyzed by EPA Method 353.3

Sulfate analyzed by EPA Method 375.4

1.2.4- and 1.3.5-Trimethylbenzene analyzed accoording to EPA Method 524.2

All monitoring wells were analyzed for BTEXN according to EPA Method SW846-8020

Methane was analyzed using the methods described in "Dissolved Oxygen & Methane in Water by a GC Headspace Equilibration Technique" by Kambell et. al. in International Journal of Environmental Analytical Chemistry, Volume 36, pp. 249-257.

SITE 870/PATRIOT HILLS GROUND-WATER SAMPLING RESULTS FOR MONITORING WELLS MW-1 THROUGH MW-14 (CONTINUED) TABLE 1

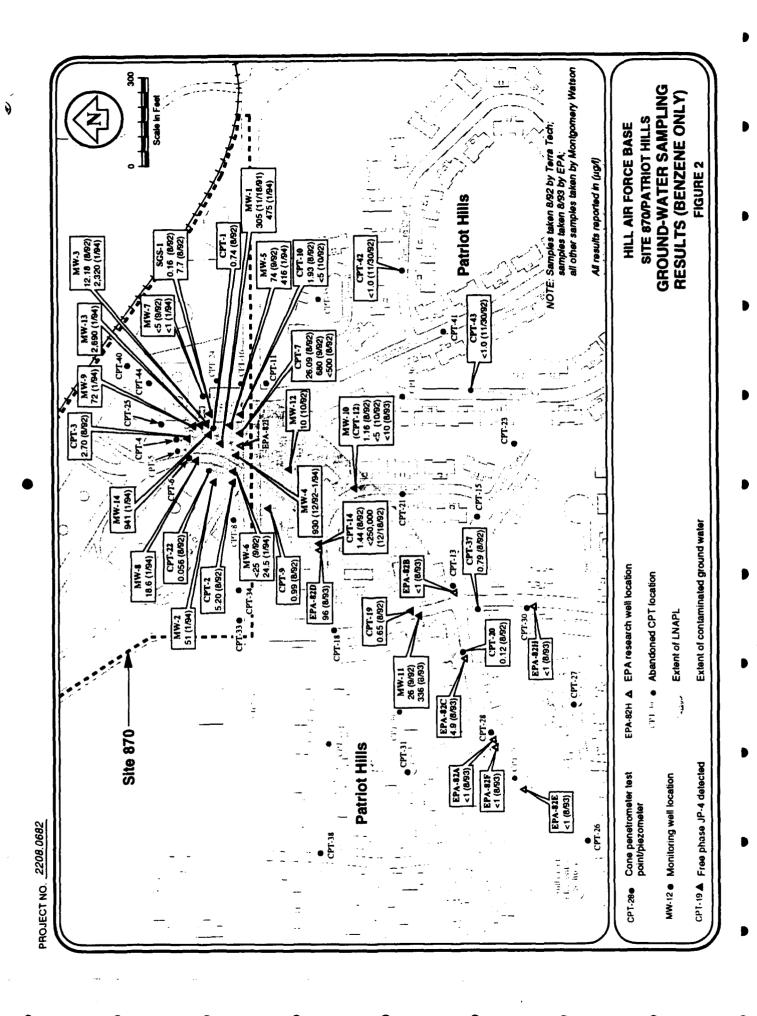
10.3 0.06 0.037 3 498 zene (µg/l) 1.113 1 2.690 1.570 2.690 4.280	Analytes	MW-13 Sampled 12/93 - 1/94	MW-13 MW-14 Sampled Sampled 12/93 - 1/94 12/93 - 1/94	
0.06 0.037 3 498 enzene (µg/l) 1,113 enzene (µg/l) 470 2,690 1,570 g/l) 589	Iron (mg/l)	10.3	5.96	
0.037 3 498 enzene (µg/l) 1.113 enzene (µg/l) 470 2.690 1.570 8/l) 589 4,280	Nitrate (mg/l)	90:0	1.72	
3 498 498 enzene (µg/l) 1,113 enzene (µg/l) 470 2,690 1,570 g/l) 589	Nitrite (mg/l)	0.037		
498 Senzene (µg/l) 1,113 Senzene (µg/l) 470 2,690 1,570 g/l) 589 4,280	Sulfate (mg/l)	£		
lbenzene (µg/l) 1.113 lbenzene (µg/l) 470 2.690 1.570 1.570 4.280	Methane (mg/l)	498	23	
1henzene (µg/1) 470 2.690 1,570 1,570 4,280	1,2,4-Trimethylbenzene (µg/l)	1,113		
2,690 1,570 1,570 899 4,280	1,3,5-Trimethylbenzene (µg/l)	470	650	
1,570 1,89 4,280	Benzene (µg/l)	2,690		
4.280	Toluene (µg/l)	1,570		
4,280	Ethylbenzene (µg/l)	589	505	
107	Xylenes (μg/l)	4,280		
101	Naphihalene (µg/l)	401	187	

NA Not analyzed mg/1 Milligrams per liter µg/1 Micrograms per liter

1.2.4- and 1.3.5.Trimethylbenzene analyzed accoording to EPA Method 524.2

All monitoring wells were analyzed for BTEXN according to EPA Method SW846-8020

Methane was analyzed using the methods described in "Dissolved Oxygen & Methane in Water by a GC Headspace Equilibration Technique" by Kanibell et. al. in International Journal of Environmental Analytical Chemistry, Volume 36, pp. 249-257. Nitrate/nitrite analyzed by EPA Method 353.3 Iron analyzed by EPA Method SW-846-6010 Sulfate analyzed by EPA Method 375.4



ATTACHMENT A LABORATORY ANALYTICAL DATA

RECEIVED

JE3 04 1994

MOSTER SERVINGEON

January 31, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: HAFB 870 Project No.: 2208.0682

MSAI Group: 3676

Dear Mr. Glascot:

Enclosed are the analytical results for your project referenced above. The following samples are included in the report.

Site 870 MW-3

Site 870 MW-20

Site 870 MW-1

Site 870 MW-8

Site 870 Trip Blk 1/27/94

All holding times were met for the tests performed on these samples.

If the report is acceptable, please approve the enclosed invoice and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

With Regards,

Leon A. Peterson

Project Manager

Analytical Report.

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Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: HAFB 870

Sample ID: Site 870 MW-3 Matrix: Waste Water MSAI Sample: 15462 MSAI Group: 3676 Date Reported: 01/31/94

Discard Date: 03/02/94
Date Submitted: 01/27/94
Date Sampled: 01/27/94

Collected by: RG

Purchase Order: Reanalysis Project No.: 2208.0682

Test	Analysis	Results as Received	Units		t of tation
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020				
	Benzene	2,320	ug/l	(1)	50
	Toluene	1,300	ug/l		50
	Ethylbenzene	376	ug/l		50
	m,p-Xylene	3,940	ug/l		50
	o-Xylene	1,530	ug/l		50
	Naphthalene	< 100	ug/l		100

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by

Leon A. Peterson Project Manager



Analytical Report:



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: HAFB 870

Sample ID: Site 870 MW-20 Matrix: Waste Water

MSAI Sample: 15463 MSAI Group: 3676 Date Reported: 01/31/94

Discard Date: 03/02/94
Date Submitted: 01/27/94
Date Sampled: 01/27/94
Collected by: RG

Purchase Order: Reanalysis Project No.: 2208.0682

Test	Analysis	Results as Received	Units	Limit of Quantitation
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020			
	Benzene	429	ug/l	20
	Toluene	<i>7</i> 5	ug/l	20
	Ethylbenzene	170	ug/l	20
	m,p-Xylene	793	ug/t	20
•	o-Xylene	276	ug/l	20
	Naphthalene	67	ug/l	40

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager



Analytical Report



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: HAFB 870

Sample ID: Site 870 MW-1 Matrix: Waste Water

MSAI Sample: 15464 MSAI Group: 3676 Date Reported: 01/31/94

Date Submitted: 03/02/94
Date Submitted: 01/27/94
Date Sampled: 01/27/94

Collected by: RG

Purchase Order: Reanalysis Project No.: 2208.0682

		Results		Limit of
Test	Analysis	as Received	Units	Quantitation
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020			
	Benzene	475	ug/l	20
	Toluene	88	ug/l	20
	Ethylbenzene	183	ug/l	20
	m,p-Xylene	856	ug/l	20
	o-Xylene	304	ug/l	20
	Naphthalene	97	ug/l	40

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager



Analytical Report:



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn:

Mr. Robert Glascot

Project: HAFB 870

Sample ID: Site 870 MW-8 Matrix: Waste Water

MSAI Sample: 15465 MSAI Group: 3676 Date Reported: 01/31/94

Discard Date: 03/02/94
Date Submitted: 01/27/94
Date Sampled: 01/27/94

Collected by: RG

Purchase Order: Reanalysis Project No.: 2208.0682

		Results		Limit of
Test	Analysis	as Received	Units	Quantitation
4264	BTEX and Naphthalene			
	Method: 600/SW-846 602/8020			
	Benzene	18.6	ug/l	5.0
	Toluene	10.8	ug/l	5.0
	Ethylbenzene	29.3	ug/l	5.0
)	m,p-Xylene	281	ug/l	5.0
	o-Xylene	33.4	ug/l	5.0
	Naphthalene	294	ug/l	10

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager

Project Manager



Analytical Report



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: HAFB 870

Sample ID: Site 870 Trip Blk 1/27/94

Matrix: Waste Water

MSAI Sample: 15466
MSAI Group: 3676
Date Reported: 01/31/94

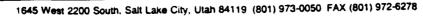
Discard Date: 03/02/94
Date Submitted: 01/27/94
Date Sampled: 01/27/94
Collected by: RG

Purchase Order: Reanalysis
Project No.: 2208.0682

Test	Analysis	Results as Received	Units	Limit of Quantitation
1690				
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020			
	Benzene	< 1.0	ug/l	1.0
	Toluene	< 1.0	ug/l	1.0
	Ethylbenzene	< 1.0	ug/l	1.0
	m,p-Xylene	< 1.0	ug/l	1.0
	o-Xylene	< 1.0	ug/l	1.0
	Naphthalene	< 2.0	ug/l	2.0

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager





CHAIN OF CUSTODY RECORD/LAB WORK REQUEST

LABORATORY ME SALES

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Chain of Cuatody Number Cooler Number

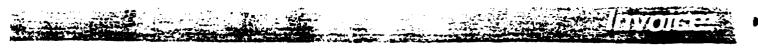
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	LABORATORY USE ONLY	SAMPLES WERE: 1 Shipped or hand delivered Notes: 2 Ambient or Chilled Notes:	3 Temperature	4 Received Broken/Leaking (Improperly Sealed) Y Notes:	5 Properly Preserved Y Notes:	6 Received Within Holding Times Y Notes	COC Tape Was: 1 Present on Outer Package Y N NA	2 Unbroken on Outer Package	3 Present on Sample Y NA NA	4 Unbroken on Sample Y N N NA Notes:	Discrepancies Between Samole Labels and COC	Record? N Y N Notes:	
									Á	Time			
	IED	BUKE Poet.	AOC	XXX	XX			4 0 1	7	Dete			
	ANAL YSES REQUESTED		CASU					INSTRICTIONS	Analyses 4	Received by			
	ANAL	wę.msu bcB	Diox					- Special	Note: Kust Analyzes 48 hr.				
	(190)	s aupiration of the following of the following for the following f		21 22 23 23 23 23 23 23 23 23 23 23 23 23						Relinquished by			
		Collected 7	emiT thaM		145				² Sampling Technique: Composite=C Grab=G	Time			
		Collected (Collected	Depth Interval (ft)	1/21/54	איניין איניין איניין איניין איניין איניין איניין איניין איניין איניין איניין איניין איניין איניין איניין איניין				DC - Drum Solids LD- Drum Llquids EP/TCLP Leachate	Dete	4 16/12		
	(1, 20. If (24.)	1 AT 5: LUE	Sample OI	MW-20	AND -8				l Water	Receight by	11-W.W.		
ي	MW Contact	Project LinkEb & 10 652 Project Number 22 08 0 652 Date Date Date Date Signature Columbia Col	No. Location nly) ID	\$4.8 A.8	1 Cip B 6.24			:	i da		11/2		_
MONTG	Phone (4	Project LIII Project Number Date Due	Lab ID No. (Lab Only)						Matrix: SO-Soil SE - Sediment	Refi	12		



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Invoice No. 202567
Invoice Date 01/31/9-

Page: 1 o. .

0.00



The Quality Solution

Project Number: 2208.0682
Purchase Order: Reanalysis
Samples Received: 01/27/94
Date Reported: 01/31/94

Turnaround Time:

Project Name:

4 days

HAFE 870

Reported To:

Mr. Robert Glascot

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Salt Lake City, UT 84124 Suite 200

HSAI Group Number: 3676

Analyses Performed See Analysis Reference Table Below

	Date	•	List	Rush		Extended
Sample I.D.	Sampled	Analyses	Price	Charges	Discount	Price
		~ ~~~~~~~~				
15462 Site 870 MW-3	01/27/94	4264	90.00		90.00	0.00
15463 Site 870 MW-20	01/27/94	4264	90.00		90.00	0.00
15464 Site 870 MW-1	01/27/94	4264	90.00		90.00	0.00
15465 Site 870 MV-8	01/27/94	4264	90.00		90.00	0 00
15466 Site 870 Trip 81k 1/27/94	01/27/94	4264	90.00		90.00	0.00

Analysis Reference Table

			Unit						
Analysi	s			# of	List	Rush	Discount	Net	Extended
No.	Analysis Name	Matrix	Hethod	Tests	Price	Charges	Amount	Price	Price
4264	BTEX and Naphthalene	W	600/SW-846 602/802	5	90.00		90.00	0.00	0.00
							Tat	tal Price 1	0.00

Pricing Summary

•	0.00
•	0.00
\$(450.00)
	\$(

TOTAL AMOUNT DUE \$ 0.00

Total Price \$



February 2, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: HAFB 870 Project No.: 2208.0682 MSAI Group: 3686

Dear Mr. Glascot:

Enclosed are the analytical results for your project referenced above. The following samples are included in the report.

Site 970 MW-5 Site 870 MW-6 Site 870 MW-4 Site 870 MW-2

Site 870 MW-16

Site 870 Trip Blk 1/28/94

TRACEIVED

TIS 0.4 1992

17 77 May 16

All holding times were met for the tests performed on these samples.

If the report is acceptable, please approve the enclosed invoice and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

With Regards,

Leon A. Peterson Project Manager

from Muss

Analytical Report

Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: HAFB 870

Sample ID: Site 870 MW-5 Matrix: Waste Water

MSAI Sample: 15487 MSAI Group: 3686 Date Reported: 02/02/94

Discard Date: 03/04/94
Date Submitted: 01/28/94
Date Sampled: 01/28/94

Collected by: RG

Purchase Order:

Project No.: 2208.0682

Test	Analysis	Results as Received	Units	Limit of Quantitation
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020 Benzene Toluene Ethylbenzene m,p-Xylene o-Xylene Naphthalene	416 250 246 1,870 638 < 100	ug/l ug/l ug/l ug/l ug/l ug/l	50 50 50 50 50 100

Respectfully Submitted, Reviewed and Approved by

Leon A. Peterson Project Manager



Analytical Report:

Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: HAFB 870

Sample ID: Site 870 MW-4 Matrix: Waste Water

MSAI Sample: 15488
MSAI Group: 3686
Date Reported: 02/02/94

Discard Date: 03/04/94
Date Submitted: 01/28/94
Date Sampled: 01/28/94

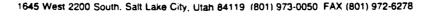
Collected by: RG
Purchase Order:

Project No.: 2208.0682

		Results		Limit of
Test	Analysis	as Received	Units	Quantitation
4264	BTEX and Naphthalene			
	Method: 600/SW-846 602/8020			
	Benzene	930	ug/l	50
	Toluene	1,830	u g/ l	50
	Ethylbenzene	450	ug/l	50
	m,p-Xylene	3,670	ug/l	50
	o-Xylene	1,450	ug/l	50
	Naphthalene	< 100	ug/l	100

Respectfully Submitted, Reviewed and Approved by

Leon A. Peterson
Project Manager





Analytical Report

Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT

Mr. Robert Glascot

Project: HAFB 870

Sample ID: Site 870 MW-6 Matrix: Waste Water

MSAI Sample: 15489 MSAI Group: 3686 Date Reported: 02/02/94

Discard Date: 03/04/94 Date Submitted: 01/28/94 Date Sampled: 01/28/94

Collected by: Purchase Order:

Project No.: 2208.0682

Test	Analysis	Results as Received	Units	Limit of Ouantitation
		as received		Agencaracion
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020			
	Benzene	24.5	ug/l	1.0
	Toluene	10.1	ug/l	1.0
	Ethylbenzene	18.6	ug/l	1.0
	m,p-Xylene	113	ug/l	1.0
	o-Xylene	42.9	ug/l	1.0
	Naphthalene	59.1	u g/ l	2.0

Respectfully Submitted, Reviewed and Approved by

Peterson Project Manager



Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: HAFB 870

Sample ID: Site 870 MW-2 Matrix: Waste Water

MSAI Sample: 15490 MSAI Group: 3686 Date Reported: 02/02/94

Discard Date: 03/04/94
Date Submitted: 01/28/94
Date Sampled: 01/28/94
Collected by: RG

Purchase Order:

Project No.: 2208.0682

		Results		Limit of
Test	Analysis	as Received	Units	Quantitation
4264	BTEX and Naphthalene			
	Method: 600/SW-846 602/8020			
	Benzene	51.0	ug/l	5.0
	Toluene	56.3	ug/l	5.0
	Ethylbenzene	73.3	ug/l	5.0
	m,p-Xylene	500	ug/t	5.0
	o-Xylene	276	ug/l	5.0
	Naphthalene	85	ug/l	10

Respectfully Submitted, Reviewed and Approved by

Leon A. Peterson Project Manager



Analytical Report.



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: HAFB 870

Sample ID: Site 870 MW-16 Matrix: Waste Water

MSAI Sample: 15491 MSAI Group: 3686 Date Reported: 02/02/94

Discard Date: 03/04/94
Date Submitted: 01/28/94
Date Sampled: 01/28/94

Collected by: RG

Purchase Order:

Project No.: 2208.0682

		Results		Limit of
Test	Analysis	as Received	Units	Quantitation
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020			
	Benzene	49.4	ug/l	1.0
	Toluene	9.8	ug/l	1.0
	Ethylbenzene	70.1	ug/l	1.0
	m,p-Xylene	660	ug/l	50
	o-Xylene	344	ug/l	50
	Naphthalene	95.5	ug/l	2.0

Respectfully Submitted.
Reviewed and Approved by

Leon A. Peterson Project Manager

1645 West 2200 South. Salt Lake City, Utah 84119 (801) 973-0050 FAX (801) 972-6278



Analytical Report

Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: HAFB 870

Sample ID: Site 870 Trip Blk 1/28/94

Matrix: Waste Water

MSAI Sample: 15492 MSAI Group: 3686 Date Reported: 02/02/94

Discard Date: 03/04/94
Date Submitted: 01/28/94
Date Sampled: 01/28/94

Collected by: RO Purchase Order:

Project No.: 2208.0682

		Results		Limit of
Test	Analysis	as Received	Units	Quantitation
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020			
	Benzene	< 1.0	ug/l	1.0
	Toluene	< 1.0	ug/i	1.0
	Ethylbenzene	< 1.0	ug/l	1.0
	m,p-Xylene	< 1.0	ug/l	1.0
	o-Xylene	< 1.0	ug/l	1.0
_	Naphthalene	< 2.0	ug/l	2.0

Respectfully Submitted, Reviewed and Approved by



CHAIN OF CUSTODY RECORD/LAB WORK REQUEST

Chain of Custody Number

Cooler Number

LABORATORY USE ONLY 1 Present on Outer Package 1 Shipped or hand delivered Notes: 4 Received Broken/Leaking 4 Unbroken on Semple (Improperly Sealed) Properly Preserved 2 Unbroken on Outer 3 Present on Sample 2 Ambient or Chilled Notes: SAMPLES WERE: Received Within Holding Times COC Tape Was: 3 Temperature 5 Package Notes Let Control ID Air Bill No. P. 0 Jenp = 1960 7 SPECIAL INSTRUCTIONS (i.e. metals list...); NYZIA 3 ANALYSES REQUESTED AOC BAYE beer コイラドの زداله į Received by signeth COM HAT Dioxin/Funan BO4Nee4 BNYE Refinquished by SOA ここころ 2 Sampling Technique: Composite=C Grab=G 1 ' xhiaM 12 | SIG 72/年1年 13 KH 1210 Time Collected Ē 620 15/87 27 Date Collected DC - Drum Solids LD- Drum Liquids EP/TCLP Leachate Depth Interval (ft) 1/28/44 Š 11. 1 J-119 01.77 des (4/ De co FAX (801) 272-0430 Sample O Received by M4-5 多 . ₩ WG · Ground Water LF · Product Project Number 220% 0482 Date Due Due AA · Air SW · Wipe LABORATORY MT. Str. MONTGOMERY WATSON, INC. 5432 Location Phone (801) 272 1900 Samplers Signature Relinquished by WS - Surface Water SE Sediment Lab ID No. (Lab Only) Klard SQ- Soil Matrix:

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Sample Labels and COC Record?

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Discrepancies Between



Invaice Na. Invoice Date

202598 02/02/94

Page: 1 of 1

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Mr. Robert Glascot

Suite 200

Montgomery Watson, Inc.

4525 South Wasatch Blvd.

Salt Lake City, UT 84124

The Quality Solution

Project Name:

HAFB 870

Project Number:

2208.0682

Purchase Order:

Samples Received: 01/28/94

02/02/94

Date Reported: Turnaround Time: 5 days

Reported To:

Mr. Robert Glascot

Analyses Performed

MSA1 Group Number: 3686	See Analysis Reference Table Below
	,,

	Date		List	Rush	Extended
Sample I.D.	Sampled	Analyses	Price	Charges Discount	Price
15487 Site 870 MW-5	01/28/94	4264	90.00	90.00	0.00
15488 Site 870 MW-4	01/28/94	4264	90.00	90.00	0.00
15489 Site 870 MW-6	01/28/94	4264	90.00	90.00	0.00
15490 Site 870 My-2	01/28/94	4264	90.00	90.00	0.00
15491 Site 870 MW-16	01/28/94	4264	90.00	90.00	0.00
15492 Site 870 Trip 81k 1/28/94	01/28/94	4264	90.00	90.00	0.00
				Total Price \$	0.00

Analysis Reference Table

						ปก	it		
Analysi	s			# of	List	∴sħ	Discount	Net	Extended
No.	Analysis Name	Matrix	Method	Tests	Price	Charges	Amount	Price	Price
4264	STEX and Naphthalene	W	600/SW-846 602/802	6	90.00		90.00	0.00	0.00
			•						
							Tot	tal Price	s 0.00

Pricing Summary

Extended List Price	\$	540.00
Total Rush Charges	\$	0.00
Total Discount	\$(. 540.00)

TOTAL AMOUNT DUE \$ 0.00

Mountain States Analytical

January 6, 1994

Mr. Robert Glascot Montgomery Watson Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, Utah 84124

re: MSAI groups 3474, 3465, 3452, 3439 Nitrite Results

Bob,

Pursuant to our conservation January 5, 1993 I have researched the Nitrite values for the above mentioned groups. If you would prefer the analytical groups be resubmitted with the following values please contact me. The nitrite results are as follows:

3474-14774	< 0.01 mg/l Nitrite
3474-14775	< 0.01 mg/l Nitrite
3474-14776	N/R on sample
3465-14748	< 0.01 mg/l Nitrite
3465-14749	0.637 mg/l Nitrite
3465-14750	< 0.01 mg/l Nitrite
3465-14751	N/R on sample
3452-14700	< 0.01 mg/l Nitrite
3452-14701	0.025 mg/l Nitrite
3452-14702	0.031 mg/l Nitrite
3452-14703	N/R on sample
3439-14663	0.021 mg/l Nitrite
3439-14664	0.037 mg/l Nitrite
3439-14665	0.187 mg/l Nitrite
3439-14666	0.577 mg/l Nitrite - M W - 9
3439-14667	N/R on sample

Bob if you need any further information from me please do not hesitate to contact me at (801) 973-0050.

Best regards.

Leon A. Peterson

January 18, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: 870 - Hill AFB Project No.: 2208-0652 MSAI Group: 3474

Dear Mr. Glascot:

Enclosed are the analytical results for your project referenced above. The following samples are included in the report.

870 MW-20

870 MW-1

Trip Blank

All holding times were met for the tests performed on these samples.

If the report is acceptable, please approve the enclosed invoice and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

With Regards,

Leon A. Peterson

son XI Lluson

Project Manager /

Analytical Report.



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: 870 - Hill AFB

Sample ID: 870 MW-1 Matrix: Waste Water MSAI Sample: 14775
MSAI Group: 3474
Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/21/93
Collected by: MA

Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	10.8	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	< 0.05	mg/l	0.05
• 1125	Sulfate, Turbidimetric Method: EPA 375.4	2	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2			
	Ethylbenzene	250	ug/i	(1) 12
	Toluene	130	ug/l	12
	o-Xylene	280	ug/l	12
	Naphthalene	< 12	ug/l	12
	1,2,4-Trimethylbenzene (Pseudocumer	1 680	ug/l	12
	1,3,5-Trimethylbenzene	330	ug/l	12
	Benzene	480	ug/l	12
	m,p-Xylene	850	ug/l	12

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by



Analytical Report:



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: 870 - Hill AFB

Sample ID: 870 MW-20 Matrix: Waste Water MSAI Sample: 14774
MSAI Group: 3474
Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/21/93
Collected by: MA
Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	11.4	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	< 0.05	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	3	mg/l	2
0976	Method: EPA 524.2 Ethylbenzene	< 12 60	ug/l ug/l	(1) 12 12
	Toluene o-Xylene Naphthalene 1,2,4-Trimethylbenzene (Pseudocume	120 88	ug/l ug/l ug/l	12 12 12
	1,3,5-Trimethylbenzene Benzene m,p-Xylene	100 220 < 12	ug/l ug/l ug/l	12 12 12

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager





January 18, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: Hill AFB - 870 Project No.: 2208-0652 MSAI Group: 3465

Dear Mr. Glascot:

Enclosed are the analytical results for your project referenced above. The following samples are included in the report.

870 MW-8

870 MW-4

870 MW-2

Trip Blank

All holding times were met for the tests performed on these samples.

If the report is acceptable, please approve the enclosed invoice and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

With Regards,

Leon A. Peterson

Leon Allus

Project Manager

Analytical Report.



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: Hill AFB - 870

Sample ID: 870 MW-2 Matrix: Waste Water MSAI Sample: 14750 MSAI Group: 3465 Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/20/93
Collected by: WA

Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	50.5	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	0.25	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	40	mg/t	2
0976	Drinking water volatiles Method: EPA 524.2 Ethylbenzene Toluene o-Xylene Naphthalene 1,2,4-Trimethylbenzene (Pseudocumen 1,3,5-Trimethylbenzene Benzene m,p-Xylene	170 330 550 160 750 350 120	ug/l ug/l ug/l ug/l ug/l ug/l ug/l	(1) 25 25 25 25 25 25 25 25 25 25

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by:



Analytical Report.



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: Hill AFB - 870

Sample ID: 870 MW-8
Matrix: Waste Water

MSAI Sample: 14748
MSAI Group: 3465
Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/20/93
Collected by: WA

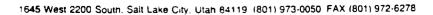
Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	5.22	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	0.28	mg/l	0.05
Q 125	Sulfate, Turbidimetric Method: EPA 375.4	11	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2			•
	Ethylbenzene	< 12	ug/i	(1) 12
	Toluene	< 12	ug/l	12
	o-Xylene	< 12	ug/l	12
	Naphthalene	300	ug/l	12
	1,2,4-Trimethylbenzene (Pseudocumen	280	ug/l	12
	1,3,5-Trimethylbenzene	140	ug/l	12
	Benzene	28	ug/l	12
	m,p-Kylene	190	ug/l	12

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by:





Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: Hill AFB - 870

Sample ID: 870 MW-4
Matrix: Waste Water

MSAI Sample: 14749
MSAI Group: 3465
Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/20/93

Collected by: WA

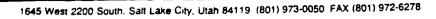
Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	13.6	mg/(0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	2.32	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	٠ 2	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2 Ethylbenzene Toluene o-Xylene Naphthalene 1,2,4-Trimethylbenzene (Pseudocum 1,3,5-Trimethylbenzene Benzene m,p-Xylene	550 2,300 1,500 < 120 en 1,500 550 1,500 4,300	ug/l ug/l ug/l ug/l ug/l ug/l	(1) 120 120 120 120 120 120 120 120

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by





January 18, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: UST 870 MSAI Group: 3452

Dear Mr. Glascot:

Enclosed are the analytical results for your project referenced above. The following samples are included in the report.

870 MW-5

870 MW-3

870 MW-6

Trip Blank

All holding times were met for the tests performed on these samples except:

Sample - (Sample Date) Test Description	Expiration Date	Date Analyzed	Days Past Holding Time
870 MW-5 - (12/17/93)			
Nitrogen, Nitrate/Nitrite	12/19/93	12/20/93	1
870 MW-3 - (12/17/93)			
Nitrogen, Nitrate/Nitrite	12/19/93	12/20/93	1
870 MW-6 - (12/17/93)			
Nitrogen, Nitrate/Nitrite	12/19/93	12/20/93	1

If the report is acceptable, please approve the enclosed invoice and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

January 18, 1994

Reference:

Project: UST 870 MSAI Group: 3452

Page 2

With Regards,

Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: UST 870

Sample ID: 870 MW-3 Matrix: Waste Water MSAI Sample: 14701 MSAI Group: 3452 Date Reported: 01/05/94

Discard Date: 02/04/94
Date Submitted: 12/20/93
Date Sampled: 12/17/93

Collected by: B Purchase Order: Project No.:

Test	Analysis	Results as Received	Limit of Quantitation		
7254	Iron by ICP Method: SW-846 6010	8.20	mg/l	0.10	
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	< 0.05	mg/l	0.05	
• 1125	Sulfate, Turbidimetric Method: EPA 375.4	< 2	mg/l	2	
0976	Drinking water volatiles Method: EPA 524.2				
	Ethylbenzene	450	ug/l	(1) 25	
	Toluene	1,550	ug/l	25	
	o-Xylene	1,500	ug/l	25	
	Naphthalene	140	ug/l	25	
	1,2,4-Trimethylbenzene (Pseudocumer	1,000	ug/l	25	
	1,3,5-Trimethylbenzene	480	ug/l	25	
	Benzene	4,300	ug/l	25	
	m,p-Xylene	4,300	ug/l	25	

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by





Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: UST 870

Sample ID: 870 MW-5
Matrix: Waste Water

MSAI Sample: 14700 MSAI Group: 3452 Date Reported: 01/05/94

Discard Date: 02/04/94
Date Submitted: 12/20/93
Date Sampled: 12/17/93

Collected by: E Purchase Order: Project No.:

Test	•	Results as Received	Units	Limit of Quantitation		
7254	Iron by ICP Method: SW-846 6010	6.41	mg/l	0.10		
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	< 0.05	mg/l	0.05		
1125	Sulfate, Turbidimetric Method: EPA 375.4	< 2	mg/l	2		
0976	Drinking water volatiles Method: EPA 524.2					
	Ethylberzene	330	ug/l	(1) 25		
	Toluene	430	ug/t	25		
	o-Xylene	900	ug/l	25		
	Naphthalene	110	ug/l	25		
	1,2,4-Trimethylbenzene (Pseudocumer	n 960	ug/(25		
	1,3,5-Trimethylbenzene	450	ug/l	25		
	Benzene	800	ug/i	25		
	m,p-Xylene	2,750	ug/l	25		

Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted Reviewed and Approved by







Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: UST 870

Sample ID: 870 MW-6
Matrix: Waste Water

MSAI Sample: 14702 MSAI Group: 3452 Date Reported: 01/05/94

Discard Date: 02/04/94
Date Submitted: 12/20/93
Date Sampled: 12/17/93

Collected by: E Purchase Order: Project No.:

Test	Analysis	Results as Received			
				Quantitation	
7254	Iron by ICP Method: SW-846 6010	10.3	mg/l	0.10	
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	0.07	mg/l	0.05	
• 1125	Sulfate, Turbidimetric Method: EPA 375.4	21	mg/l	2	
0976	Drinking water volatiles Method: EPA 524.2				
	Ethylbenzene	< 120	ug/l	(1) 120	
	Toluene	< 120	ug/l	120	
	o-Xylene	450	ug/l	120	
	Naphthalene	580	ug/l	120	
	1,2,4-Trimethylbenzene (Pseudocumen	1,500	ug/l	120	
	1,3,5-Trimethylbenzene	650	ug/l	120	
	Benzene	280	ug/l	120	
	m,p-Xylene	1,300	ug/l	120	

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly

Respectfully Submitted, Reviewed and Approved by





Suite 200

Salt Lake City, UT 84124

Attn:

Mr. Robert Glascot

Project: UST 870

Sample ID: Trip Blank Matrix: Waste Water MSAI Sample: 14703 MSAI Group: 3452 Date Reported: 01/05/94

Discard Date: 02/04/94
Date Submitted: 12/20/93
Date Sampled: 12/17/93

Collected by:
Purchase Order:
Project No.:

Test	Analysis	Results as Received	Units	Limit of Quantitation
0976	Drinking water volatiles Method: EPA 524.2 Ethylbenzene Toluene o-Xylene Naphthalene 1,2,4-Trimethylbenzene (Pseudocume 1,3,5-Trimethylbenzene Benzene m,p-Xylene	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	ug/l ug/l ug/l ug/l ug/l ug/l ug/l	0.5 0.5 0.5 0.5 0.5 0.5 0.5

Respectfully Submitted, Reviewed and Approved by



Analytical Report:

Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: Hill AFB - 870

Sample ID: Trip Blank Matrix: Waste Water MSAI Sample: 14751 MSAI Group: 3465 Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/20/93

Collected by: WA Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received			
				Quantitation	
0976	Drinking water volatiles Method: EPA 524.2				
	Ethylbenzene	< 0.5	ug/l	0.5	
	Toluene	< 0.5	ug/l	0.5	
	o-Xylene	< 0.5	ug/l	0.5	
	Naphthalene	< 0.5	ug/l	0.5	
•	1,2,4-Trimethylbenzene (Pseudocumer	n < 0.5	ug/l	0.5	
	1,3,5-Trimethylbenzene	< 0.5	ug/l	0.5	
	Benzene	< 0.5	ug/(0.5	
	m,p-Xylene	< 0.5	ug/l	0.5	

Respectfully Submitted, Reviewed and Approved by)



Analytical Report



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: 870 - Hill AFB

Sample ID: Trip Blank Matrix: Waste Water MSAI Sample: 14776
MSAI Group: 3474
Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/21/93

Collected by: Purchase Order:

Project No.: 2208-0652

Test Analysis	Results as Received	Units	Limit of Quantitation
0976 Drinking water volatiles			
Method: EPA 524.2 Ethylbenzene Toluene o-Xylene Naphthalene 1,2,4-Trimethylbenzene (Pseudocu 1,3,5-Trimethylbenzene Benzene	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	ug/l ug/l ug/l ug/l ug/l ug/l ug/l	0.5 0.5 0.5 0.5 0.5 0.5 0.5

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager

120,000





January 4, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: 870

Project No.: 2208-0652

MSAI Group: 3439

Dear Mr. Glascot:

Enclosed are the analytical results for your project referenced above. The following samples are included in the report.

870 MW-7

870 MW-13

870 MW-14

870 MW-9

870 Trip Blank

All holding times were met for the tests performed on these samples.

If the report is acceptable, please approve the enclosed invoice and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

With Regards,

Leon A. Peterson

off Eliosu for

Project Manager

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Analytical Report.



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: 870

Sample ID: 870 MW-7 Matrix: Waste Water MSAI Sample: 14663 MSAI Group: 3439 Date Reported: 01/04/94

Discard Date: 02/03/94
Date Submitted: 12/17/93
Date Sampled: 12/16/93

Collected by: BG

Purchase Order:

Project No.: 2208-0652

		Results		Limit of
Test	Analysis	as Received	Units	Quantitation
7254		1.36	mg/l	0.10
	Method: SW-846 6010			
0219	Nitrogen, Nitrate/Nitrite	11.8	mg/l	0.05
	Method: EPA 353.3			
1125	Sulfate, Turbidimetric	26	mg/l	2
	Method: EPA 375.4			
4264	BTEX and Naphthalene			
	Method: 600/SW-846 602/8020			
	Benzene	< 1.0	ug/l	1.0
	Toluene	< 1.0	ug/l	1.0
	Ethylbenzene	< 1.0	ug/l	1.0
	m,p-Xylene	< 1.0	ug/l	1.0
	o-Xylene	< 1.0	ug/(1.0
	Naphthalene	< 2.0	ug/l	2.0
0976	Drinking water volatiles Method: EPA 524.2			
	1,2,4-Trimethylbenzene (Pseudocume	n < 1	ug/l	(1) 1
	1,3,5-Trimethylbenzene	< 1	ug/l	1
	•			

(1) LOQ raised due to insufficient sample.

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager

1645 West 2200 South. Salt Lake City. Utah 84119 (801) 973-0050 FAX (801) 972-6278



Analytical Report.



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: 870

Sample ID: 870 MW-13 Matrix: Waste Water MSAI Sample: 14664
MSAI Group: 3439
Date Reported: 01/04/94

Discard Date: 02/03/94
Date Submitted: 12/17/93
Date Sampled: 12/16/93

Collected by: BG Purchase Order:

Project No.: 2208-0652

Test Analysis 7254 Iron by ICP Method: SW-846 6010	Results as Received	Limit of Quantitation		
	Iron by ICP	10.2	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	0.10	mg/l	0.05
• 1125	Sulfate, Turbidimetric Method: EPA 375.4	3	mg/l	2
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020			
	Benzene	2,690	ug/l	50
	Toluene	1,530	ug/l	50
	Ethylbenzene	589	ug/l	50
	m,p-Xylene	3,140	ug/l	50
	o-Xylene	1,140	ug/l	50
	Naphthalene	401	ug/l	100
0976	Drinking water volatiles Method: EPA 524.2			
	1,2,4-Trimethylbenzene (Pseudocumen	1,100	ug/t	(1) 20
	1,3,5-Trimethylbenzene	470	ug/l	20

Due to high non-target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by:



Analytical Report



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: 870

Sample ID: 870 MW-14 Matrix: Waste Water MSAI Sample: 14665
MSAI Group: 3439
Date Reported: 01/04/94

Discard Date: 02/03/94
Date Submitted: 12/17/93
Date Sampled: 12/16/93

Collected by: BG Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	5.96	 mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	1.91	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	27	mg/l	2
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020 Benzene Toluene Ethylbenzene	941 2,800 505	ug/l ug/l ug/l	50 50 50 50
	m,p-Xylene o-Xylene Naphthalene	4,050 1,460 187	ug/l ug/l ug/l	50 100
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocume 1,3,5-Trimethylbenzene	n 1,400 650	ug/l ug/l	(1) 20 20

(1) Due to high non-target compound level(s), dilution was required. The LOQ was raised accordinly.

Respectfully Submitted, Reviewed and Approved by:







Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: 870

Sample ID: 870 MW-9 Matrix: Waste Water MSAI Sample: 14666 MSAI Group: 3439 Date Reported: 01/04/94

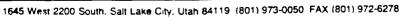
Discard Date: 02/03/94
Date Submitted: 12/17/93
Date Sampled: 12/16/93

Collected by: BO Purchase Order:

Project No.: 2208-0652

		Results	Limit of		
Test	Analysis	as Received	Units	Quantitation	
7254	Iron by ICP Method: SW-846 6010	2.07	mg∕l	0.10	
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	0.40	mg/l	0.05	
1125	Sulfate, Turbidimetric Method: EPA 375.4	22	mg/l	2	
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020				
	Benzene	72	ug/l	10	
	Toluene	27	ug/l	10	
	Ethylbenzene	35	ug/l	10	
	m,p-Xylene	406	ug/l	10	
	o-Xylene	152	ug/l	10	
	Naphthalene	598	ng/l	20	
3976	Drinking water volatiles Method: EPA 524.2				
	1,2,4-Trimethylbenzene (Pseudocume	n 650	ug/l	12	
	1,3,5-Trimethylbenzene	190	ug/l	12	

Respectfully Submitted, Reviewed and Approved by:





Analytical Report:



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: 870

Sample ID: 870 Trip Blank Matrix: Waste Water

MSAI Sample: 14667
MSAI Group: 3439
Date Reported: 01/04/94

Date Submitted: 02/03/94
Date Submitted: 12/17/93
Date Sampled: 12/15/93

Collected by: BO Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
4264	BTEX and Naphthalene Method: 600/SW-846 602/8020			
	Benzene	< 1.0	ug/l	1.0
	Toluene	< 1.0	ug/l	1.0
	Ethylbenzene	< 1.0	ug/l	1.0
	m,p-Xylene	< 1.0	ug/l	1.0
	o-Xylene	< 1.0	ug/l	1.0
	Naphthalene	< 2.0	ug/l	2.0
0976	Drinking water volatiles Method: EPA 524.2			
	1,2,4-Trimethylbenzene (Pseudocume	n < 1	ug/l	(1) 1
	1,3,5-Trimethylbenzene	< 1	ug/l	1

(1) LOQ raised due to insufficient sample.

Respectfully Submitted, Reviewed and Approved by:





Invoice No. Invoice Date

202400 01/04/94

ce Date 01/04/94 Page: 1 of

Mountain States Analytical

The Quality Solution

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Salt Lake City, UT 84124 Suite 200 Project Name: 870 · Project Number: 2208-0652

Purchase Order:

Samples Received: 12/17/93
Date Reported: 01/04/94
Turnaround Time: 18 days

Reported To:

Mr. Robert Glascot

Analyses Performed

MSA1 Group Number: 3439 See Analysis Reference Table Below

Sample I.D.	Date Sampled	Analyses					List Price	Rush Charges	Discount	Extended Price
14663 870 MW-7	12/16/93	0001F 0219	03921 0976	1125	4264	7254	534.00		80.10	453.9
14664 870 MW-13	12/16/93	0001F 0219	03921 0976	1125	4264	7254	534.00		80.10	453.9
14665 870 MW-14	12/16/93	0001F 0219	03921 0976	1125	4264	7254	534.00		80.10	453.90
14666 870 MW-9	12/16/93	0001F 0219	03921 0976	1125	4264	7254	534.00		80.10	453.9.
14667 870 Trip Blank	12/15/93	0001F 0976	4264				465.00		69.75	395.25

Total Price \$ 2,210.85

Analysis Reference Table

						TTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT	11 [
Analysi	s			# of	List	Rush	Discount	Net	Extended
No.	Analysis Name	Matrix	Method	Tests	Price	Charges	Amount	Price	Price
0001F	Special Instructions, GC/MS VOA		SPECIAL INST. MSAI	5	0.00		0.00	0.00	0.0
0219	Nitrogen, Nitrate/Nitrite	WA	EPA 353.3	4	15.00		2.25	12.75	51.0
03921	Flame/ICP Prep for Metals, Waters	WW	SW-846 3005	4	15.00		2.25	12.75	51.0
0976	Drinking water volatiles	WA	EPA 524.2	5	375.00		56.25	318.75	1,593.7
1125	Sulfate, Turbidimetric	W	EPA 375.4	4	25.00		3.75	21.25	85.0
4264	BTEX and Naphthalene	WW	600/SW-846 602/802	5	90.00		13.50	76.50	382.5
7254	Iron by ICP	WH.	SW-846 6010	4	14.00		2.10	11.90	47.6

Total Price \$ 2,210.8

Pricing Summary

Extended List Price \$ 2,601.C
Total Rush Charges \$ 0.0
Total Discount \$(370.1

TOTAL AMOUNT DUE \$ 2,210.8

CHAIN OF CUSTODY RECORD/LAB WORK REQUEST

LABORATORY ALL SAL ALLE KAL

Chain of Custody Number

Lot Control ID
Page
Air Bill No.

3

3

LABORATORY USE ONLY	SAMPLES WERE: 1 Shipped or hand delivered	2 Ambient or Chilled Notes Notes 3 Temperature	4 Received Broken/Leaking (Improperty Sealed)	S Properly Preserved Y Notes	6 Received Within Holding Times Y Notes	COC Tape Was: 1 Present on Outer Package Y N NA	2 Unbroken on Outer Package Y N NA	3 Present on Sample Y N NA 4 Unbroken on Sample	Time Y N NA	Discrepancies Between Sample Labels and COC
TED OF	.1 20 9 3.	AETA VOC BUA					(i.e. metals list.		ole 0	
ANALYSES REQUESTED		Dioxin/Fund TPH MOD Metals Cyanide TCLP- Med					SPECIAL INSTRUCTIONS (I.e. metals list):		Received by	
	EZI V X=	to sedmuM	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	NV NI	स्र				Relinquished by	
	perted	Time Collination 1	3 30	15.20 au 11.415 au	2000	. :		- Sampling Technique. Composite=C Grab=G	Time Rellin	27/5
	pelice	Depth Date Colle		31-21-20 PA-21-16-17-16-17-16-17-18-18-18-18-18-18-18-18-18-18-18-18-18-	Mals 2	1		DC - Drum Liquids LD- Drum Liquids EP/TCLP Leachate		12/16/10 154
Montage (1901) 272-1900 FAX (801) 272-0430 MW Contage McB France	218-0652-	Sample	MW-7 MW-13	100-14 100-9 100-19	nu 7 hael enes 2 maes 2		1	WG - Ground Water DC LF - Product LD AA - Air EP SW - Wipe	Received by	You Stull
thone (801) 272-1900 FAX (1871) W Contact	872. Iber 2703. Onallure 74	Location	 	222	L.711.17			Nater	shed by	
Phone (801) WW Contact	Project & 22. Project Number Date Due Samplers Signature	Lab ID No.	,					Matrix: SO-Sul SE: Sediment WS: Surface Water	Relinquished by	Mar

... ::::

January 6, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: 870 - Hill AFB Project No.: 2208-0652 MSAI Group: 3474

Dear Mr. Glascot:

Enclosed are the analytical results for your project referenced above. The following samples are included in the report.

870 MW-20

870 MW-1

Trip Blank

All holding times were met for the tests performed on these samples.

If the report is acceptable, please approve the enclosed invoice and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

With Regards,

Leon A. Peterson

won Alluno

Project Manager

Mountain States Analytical The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

り

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: 870 - Hill AFB

Sample ID: 870 MW-20 Matrix: Waste Water

MSAI Sample: 14774
MSAI Group: 3474
Date Reported: 01/06/94

Discard Date: 02/05/94 Date Submitted: 12/21/93 Date Sampled: 12/21/93

Collected by: MAP
Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	11.4	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	< 0.05	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	3	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocume 1,3,5-Trimethylbenzene	n < 10 100	ug/l ug/l	(1) 10 10

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager

Project manager



1645 West 2200 South. Salt Lake City, Utah 84119 (801) 973-0050 FAX (801) 972-6278



Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: 870 - Hill AFB

Sample ID: 870 MW-1 Matrix: Waste Water MSAI Sample: 14775
MSAI Group: 3474
Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/21/93
Collected by: MA

Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	10.8	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	< 0.05	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	2	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocum 1,3,5-Trimethylbenzene	en 680 330	ug/l ug/l	(1) 10 10

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by:





Suite 200

Salt Lake City, UT

Mr. Robert Glascot Project: 870 - Hill AFB

Sample ID: Trip Blank Matrix: Waste Water MSAI Sample: 14776 MSAI Group: 3474 Date Reported: 01/06/94

Discard Date: 02/05/94 Date Submitted: 12/21/93 Date Sampled: 12/21/93

Collected by: MA Purchase Order:

2208-0652 Project No.:

Test	Analysis	Results as Received	Units	Limit of Quantitation
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocumen 1,3,5-Trimethylbenzene	< 0.5 < 0.5	ug/l ug/l	0.5 0.5

Respectfully Submitted, Reviewed and Approved by

Peterson Leon A. Project Manager



HILL AIR FORCE BASE OPERABLE UNIT 1 CHAIN OF CUSTODY RECORD/LAB WORK REQUEST

LABORATORY HELL

Chain of Custody Number
Cooler Number
Lot Control ID
Page of

	LABORATORY USE ONLY	SAMPLES WERE:	1 Shipped or hand delivered Notes:	2 Ambient or Chilled Notes:	3 Temperature	4 Received Broken/Leaking	(Improperly Sealed)	Notes	5 Properly Preserved	Z .5000		Holding Times	Notes:	COC Tape Was:	1 Present on Outer Package	2 Unbroken on Outer Package	Z	a Present on Sample	4 Unbroken on Sample	NOIGE	Discrepancies Between	Record?	Notes	
																	~		e E					
	VESTED	po	z pa	7/2	eav ear	XXII	XX		4.5	# [/	7				(i.e. motals list.		obete					
	ANALYSES REQUESTED	aM .	. Mn, X . Mg. M . Fe, Mg	HCO ₃ ;e, Mg 2a, Fe, 1 1	K' M' VB' C CO' L					14-47	3	/			7		SPECIAL INSTRUCTIONS (I.e. metals list):		Received by					
	(1700	(MIS 4	(0058 (0058 V (0758 V (0758 V	CPLOU (SM (SM (SM	BNY	×	X												wheel by					
	-		I echnik	Guild		8089	Ged 13 5	114						\bigvee			2 Sampling Technique:		Relinguished by					
-			ected			220 0900	12-21 1140										2 Sampling Tec	Grab=G	1	1217				
	R A		audia.	7	Depth Interval (ft)	d h	b	93									· Drum Solids	EP/TCLP Leachate	100	1, 21,00				
5AX (801) 272-0430	Marie	3 0652	and the		Sample ID	W1120	/-mm/	7									1 Water	_	Barrelund hv		adrial State			
5 Y	4/4c	220%	nature /		Locatión	870	870	773									WG · Ground	Valer		#	174			-
Phone (801) 272-1900	MW Contact	Project Number	Date Due Semplers Signature		Lab ID No. (Lab Only)												Matrix	SC Sodiment SE Sediment WS - Surface Water	(a) mother					

202434 Invoice No. Invoice Date 01/06/94

Page



Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Salt Lake City, UT 84124 Suite 200

Project Name: 2208-0652 Project Number:

870. - HILL AFB

Purchase Order:

Samples Received: 12/21/93 01/06/94 Date Reported: Turnaround Time:

16 days

Reported To:

Mr. Robert Glascot

Analyses Performed

See Analysis Reference Table Below

MSAI Group Number: 3474		See Analysis Reference Table Below								
	Date		List	Rush	Extended					
Sample I.D.	Sampled	Analyses	Price	Charges Discount	Price					
14774 870 MW-20	12/21/93	0001F 0219 03921 0976 1125 7254	444.00	66.60	377.40					
14775 870 MW-1	12/21/93	0001F 0219 0392I 0976 1125 7254	444.00	66.60	377.40					
14776 Trip Blank	12/21/93	0001F 0976	375.00	56.25	318.75					

Total Price \$ 1,073.55

Analysis Reference Table

				Unit								
Analysi	s			# of	List	Rush	Discount	Net	Extended			
No.	Analysis Name	Matrix	Hethod	Tests	Price	Charges	Amount	Price	·e			
00015	Special Instructions, GC/MS VOA		SPECIAL INST. MSAI	3	0.00		0.00	0.00	0.0			
0219	Hitrogen, Hitrate/Nitrite	WA	EPA 353.3	2	15.00		2.25	12.75	25.5			
03921	Flame/ICP Prep for Metals, Waters	w	SW-846 3005	2	15.00		2.25	12.75	25.5			
0976	Drinking water volatiles	WA	EPA 524.2	3	375.00		55.25	318.75	956.2			
1125	Sulfate, Turbidimetric	W	EPA 375.4	2	25.00		3.75	21.25	42.5			
7254	Iron by ICP	W	SW-846 6010	2	14.00		3,10	11.90	23.8			

Total Price \$ 1,073.5

Pricing Summary

Extended List Price	\$	1,263.
Total Rush Charges	\$	0.
Total Discount	\$(189.

TOTAL AMOUNT DUE \$ 1,073.

January 6, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: Hill AFB - 870 Project No.: 2208-0652 MSAI Group: 3465

Dear Mr. Glascot:

Enclosed are the analytical results for your project referenced above. The following samples are included in the report.

870 MW-8

870 MW-4

870 MW-2

Trip Blank

All holding times were met for the tests performed on these samples.

If the report is acceptable, please approve the enclosed invoice and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

With Regards,

Leon A. Peterson

Project Manager

Analytical Report:



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: Hill AFB - 870

Sample ID: 870 MW-8 Matrix: Waste Water MSAI Sample: 14748
MSAI Group: 3465
Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/20/93

Collected by: Yurchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	5.22	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	0.28	mg∕l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	11	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocume 1,3,5-Trimethylbenzene	en 280 140	ug/l ug/l	(1) 10 10

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by:



Analytical Report.



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: Hill AFB - 870

Sample ID: 870 MW-4
Matrix: Waste Water

MSAI Sample: 14749
MSAI Group: 3465
Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/20/93

Collected by: WA Purchase Order:

Project No.: 2208-0652

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	13.6	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	2.32	mg/(0.05
• 1125	Sulfate, Turbidimetric Method: EPA 375.4	< 2	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocume 1,3,5-Trimethylbenzene	n 1,500 550	ug/l ug/l	(1) 100 100

 Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager

1645 West 2200 South, Salt Lake City, Utah 84119 (801) 973-0050 FAX (801) 972-6278



Analytical Report



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: Hill AFB - 870

Sample ID: 870 MW-2 Matrix: Waste Water MSAI Sample: 14750 MSAI Group: 3465 Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/20/93

Collected by: WA

Purchase Order:

Project No.: 2208-0652

Test	•	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	50.5	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	0.25	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	40	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocum 1,3,5-Trimethylbenzene	en 750 350	ug/l ug/l	(1) 20 20

(1) Due to high target compound level(s), dilution was required. The LOQ was raised accordingly.

Respectfully Submitted, Reviewed and Approvedyby:

Leon A. Peterson Project Manager



Anaiytical Report.



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: Hill AFB - 870

Sample ID: Trip Blank Matrix: Waste Water MSAI Sample: 14751 MSAI Group: 3465 Date Reported: 01/06/94

Discard Date: 02/05/94
Date Submitted: 12/21/93
Date Sampled: 12/20/93
Collected by: WA

Purchase Order:

Project No.: 2208-0652

		Results		
Test	Analysis	as Received	Units	Quantitation
0976	Drinking water volatiles Method: EPA 524.2			
	1,2,4-Trimethylbenzene (Pseudocumen	< 0.5	ug/i	0.5
	1,3,5-Trimethylbenzene	< 0.5	ug/l	0.5

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager



OPERABLE UNIT 1 HILL AIR FORCE BASE

MONTGOMERY WATSON, INC

LABORATORY

Chain of Custody Number 5 Cooler Number Lot Control ID Air Bill No. Page

1 Present on Outer Package Y NA o Sample NA LABORATORY USE ONLY 1 Shipped or hand delivered Notes: 4 Received Broken/Leaking ž ž 3 Temperature (Improperly Sealed) 2 Unbroken on Outer Package Present on Sample Y Properly Preserved 2 Ambient or Chilled Notes: Received Within Holding Times SANPLES WERE: COC Tape Was: Unbroken on S Y N z Notes S Ē SPECIAL INSTRUCTIONS (I.e. metals list...) **\$** Zav/EON ANALYSES REQUESTED As, Cr, Ca, Fe, Mg, Mn, K, Na Received by Cs. Fe, Mg. Mn. K. Ns CO-MCO3. TDS CI, FI, 504, Mitrate, Hex CHOWS (2M 1186) 3 BARE (SW 8270) Relinquished by (093EATS) AOC 2Sampling Technique: Composite=C Grab=G 4 (latof) anematroc) to seamute sempling Techniques 195 W W 'xhisM 0, K Time Collected 02 Ē 12.20 2-20 07-21 Ra Data Collected DC - Drum Solids LD- Drum Liquids EP/TCLP Leachate -20-93 Depth Interval (ff) 5 -93 870 12-20 Phone (801) 272-1900 JEAX (901) 272-1999 WG - Ground Water LF - Product AA - Air SW - Wipe Received by Sample ID \mathcal{L} Location 018 820 870 Matrix: SO- Soil SE - Sediment WS - Surface Water Relinquished by Samplers Signature Project Number Lab ID No. (Lab Only) MW Contact Project -Date Due 3101ECT NO. 2208.0712 Discrepancies Between Sample Labels and COC Record?

N

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Notes



Invoice No. 202433 Invoice Date 01/06/94

Page: 1 c



The Quality Solution

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasarch Blvd. Salt Lake City, UT 84124 Suite 200 Project Name: Hill AFB - 870 Project Number: 2208-0652

Purchase Order:

Samples Received: 12/21/93
Date Reported: 01/06/94
Turnaround Time: 16 days

Reported To:

Mr. Robert Glascot

Analyses Performed

MSAI Group Number: 3465		See Analysis Reference Table Below					
	Date		List	Rush	Extend		
Sample 1.D.	Sampled	Analyses	Price	Charges Dis	count Price		

14748 870 HW-8	12/20/93	0001F 0219 0392I 0976 1125 7254	444.00		66.60 377.		
14749 870 MW-4	12/20/93	0001F 0219 0392I 0976 1125 7254	444.00		66.60 377.		
14750 870 MW-2	12/20/93	0001F 0219 0392I 0976 1125 7254	444.00		66.60 377.		
14751 Trip Blank	12/20/93	0001F 0976	375.00		56.25 318.		

Total Price \$ 1,450.

Analysis Reference Table

				Unit					
inalysi	s			# of	List	Rush	Discount	Net	Extence
No.	Analysis Name	Matrix	Method	Tests	Price	Charges	Amount	Price	Price
			^						
0001F	Special Instructions, GC/MS VOA		SPECIAL INST. MSAI	4	0.00		0.00	0.00	C .
0219	Nitrogen, Nitrate/Nitrite	WA	EPA 353.3	3	15.00		2.25	12.75	38.
03921	Flame/ICP Prep for Metals, Waters	w	SW-846 3005	3	15.00		2.25	12.75	38.
0976	Drinking water volatiles	WA	EPA 524.2	4	375.00		56.25	318.75	1,275.
1125	Sulfate, Turbidimetric	w	EPA 375.4	3	25.00		3.75	21.25	63.
7254	Iron by ICP	w	SW-846 6010	3	14.00		2.10	11.90	35.
	·								

Total Price \$ 1,45C.

Pricing Summary

Extended List Price \$ 1,707.
Total Rush Charges \$ C.
Total Discount \$(25c.

TOTAL AMOUNT DUE \$ 1,450.



January 5, 1994

Mr. Robert Glascot Montgomery Watson, Inc. 4525 South Wasatch Blvd. Suite 200 Salt Lake City, UT 84124

Reference:

Project: UST 870 MSAI Group: 3452

Dear Mr. Glascot:

Enclosed are the analytical results for y project referenced above. The following samples are included in the report.

870 MW-5 Trip Blank 870 MW-3

870 MW-6

All holding times were met for the tests performed on these samples except:

Sample - (Sample Date) Test Description	Expiration Date	Date Analyzed	Days Past Holding Time
870 MW-5 - (12/17/93)			
Nitrogen, Nitrate/Nitrite	12/19/93	12/20/93	1
870 MW-3 - (12/17/93)			
			•
Nitrogen, Nitrate/Nitrite	12/19/93	12/20/93	1
070 161 (/12/17/02)			
870 MW-6 - (12/17/93)			_
Nitrogen, Nitrate/Nitrite	12/19/93	12/20/93	1

If the report is acceptable, please approve the enclosed invoice

January 5, 1994

Reference:

Project: UST 870 MSAI Group: 3452

Page 2

and forward it for payment.

Thank you for selecting Mountain States Analytical, Inc. to serve as your analytical laboratory on this project. If you have any questions concerning these results, please feel free to contact me at any time.

We look forward to working with you on future projects.

With Regards,

Leon A. Peterson

Project Manager

Analytical Report



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot

Project: UST 870

Sample ID: 870 MW-5 Matrix: Waste Water MSAI Sample: 14700
MSAI Group: 3452
Date Reported: 01/05/94

Discard Date: 02/04/94
Date Submitted: 12/20/93
Date Sampled: 12/17/93

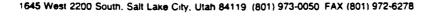
Collected by: B Purchase Order: Project No.:

Test	Analysis	Results as Received	Units	Limit of Quantitation	
7754	Tron has ICD			A 10	
7254	Iron by ICP Method: SW-846 6010	6.41	mg/l	0.10	•
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	ND	mg/l	0.05	
• 1125	Sulfate, Turbidimetric Method: EPA 375.4	ND	mg/l	2	•
0976	Drinking water volatiles Method: EPA 524.2				
	1,2,4-Trimethylbenzene (Pseudocume	n 960	ug/l	25	
	1,3,5-Trimethylbenzene	450	ug/l	25	Þ

ND - Not detected at the limit of detection

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson
Project Manager





Analytical Report:



Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT

Mr. Robert Glascot

Project: UST 870

Sample ID: 870 MW-3 Matrix: Waste Water MSAI Sample: 14701 MSAI Group: 3452 Date Reported: 01/05/94

Discard Date: 02/04/94 Date Submitted: 12/20/93 Date Sampled: 12/17/93

Collected by: Purchase Order: Project No.:

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	8.20	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	ND	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	ND	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocume 1,3,5-Trimethylbenzene	n 1,000 480	ug/l ug/l	25 25

ND - Not detected at the limit of detection

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson

Project Manager



Analytical Report:



The Quality Solution

Montgomery Watson, Inc. 4525 South Wasatch Blvd.

Suite 200

Salt Lake City, UT 84124

Attn: Mr. Robert Glascot Project: UST 870

Sample ID: 870 MW-6 Matrix: Waste Water MSAI Sample: 14702 MSAI Group: 3452 Date Reported: 01/05/94

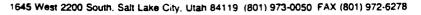
Discard Date: 02/04/94
Date Submitted: 12/20/93
Date Sampled: 12/17/93

Collected by: BO
Purchase Order:
Project No.:

Test	Analysis	Results as Received	Units	Limit of Quantitation
7254	Iron by ICP Method: SW-846 6010	10.3	mg/l	0.10
0219	Nitrogen, Nitrate/Nitrite Method: EPA 353.3	0.07	mg/l	0.05
1125	Sulfate, Turbidimetric Method: EPA 375.4	21	mg/l	2
0976	Drinking water volatiles Method: EPA 524.2 1,2,4-Trimethylbenzene (Pseudocument, 3,5-Trimethylbenzene)	n 1,500 650	ug/l ug/l	120 120

Respectfully Submitted, Reviewed and Approved by:

Leon A. Peterson Project Manager





Analytical Report



Montgomery Watson, Inc.

4525 South Wasarch Blvd.

Suite 200

Salt Lake City, UT 84124

Mr. Robert Glascot Attn:

Project: UST 870

Test Analysis

Sample ID: Trip Blank Matrix: Waste Water MSAI Sample:

14703

MSAI Group:

3452

Date Reported: 01/05/94

(

Discard Date:

02/04/94

Date Submitted: 12/20/93 Date Sampled:

12/17/93

Collected by:

BG

Purchase Order:

Project No.:

Results as Received Limit of

Quantitation

1976 Drinking water volatiles

Method: EPA 524.2

1,2,4-Trimethylbenzene (Pseudocumen 1,3,5-Trimethylbenzene

< 0.5 < 0.5

ug/l

Units

0.5

ug/l

0.5

Respectfully Submitted Reviewed and Approved by:

Leon A. Peterson

Project Manager

1645 West 2200 South, Salt Lake City, Utah 84119 (801) 973-0050 FAX (801) 972-6278



CHAIN OF CUSTODY RECORD/LAB WC.1K REQUEST

Chain of Custody Number

Cooler Number Lot Control ID

Page Air Bill No.

Sper	
dam	
Mar	
LABORATORY	

MONTGOMERY WATSON, INC.

1 Shipped of hand delivered Notes: LABORATORY USE ON! Y 1 Present on Outer Package 4 Received Broken/Leaking ž ž 3 Temperature (Improperly Sealed) Property Preserved 2 Ambient or Chilled 2 Unbroken on Outer Present on Sample SAMPLES WERE: 6 Received Within COC Tape Was: z Package Notes Notes SPECIAL INSTRUCTIONS (I.e. metals list...): **ANALYSES REQUESTED** AOC BNYE beef Dioxin/Furan PesVPCB 2.425 Sampling Technique: 0730 14 14 Composite=C Grab=G ^l xhisM Detaelled emiT Date Collected DC - Drum Solids LD- Drum Liquids EP/TCLP Leachate Depth Interval (ft) $\phi |\phi|$ Phone (801) 272-1900 FAX (80 (1272-9430 MW Contact Sample ID WG - Ground Water LF - Product AA - Air SW - Wipe 2520 Location Samplers Signature SO- Soil SE · Sediment WS · Surface Water Project Number Lab ID No. (Lab Only) **MW Contact** Date Due Project Matrix:

N N Y		Discrepancies Between	Record?	Z Soles	
Time					
Date					
Received by					
Relinquished by					
TIM•	1720				
Dete	12-17-93				
A Receipted by	Ent I de				
Relinquished by	The state of the s				



(4)



Invoice No. Invoice Date

202406 01/05

Page:



Mr. Robert Glascot

Suize 200

Montgomery Watson, Inc.

4525 South Wasatch Blvd.

Salt Lake City, UT 84124

Mountain States Analytical

The Quality Solution

Project Name:

UST 870

Project Number:

Purchase Order:

Samples Received: 12/20/93

Date Reported:

01/05/94

Turnaround Time: 16 days

Reported To:

Mr. Robert Glascot

Analyses Performed

MSAI Group Number: 3452		See Analysis Reference Table Below					A		Extended
	Date					List	Rush		
Sample 1.0.	Sampled	Analyses				Price	Charges	Discount	Price
14700 870 MW-5	12/17/93	0001F 0219	03921 0976	1125	7254	444.00		66.60	377.40
14701 870 MW-3	12/17/93		03921 0976		7254	444.00		66.60	377.40
	12/17/93		03921 0976		7254	444.00		66.60	377.40
14702 870 MW-6			93721 0710			375.00		56.25	318.75
14703 Trip Blank	12/17/93	0001F 0976							

Total Price \$ 1,450.95

Analysis Reference Table

					Unit					
Analysi	s			# af	List	Rush	Discount Amount	Net Price	Extended Price	
No.	Analysis Name	Matrix	Method	Tests	Price	Charges	Amount			
40040	a in terrorian come von		SPECIAL INST. HSAT	4	0.00		0.00	0.00	0.00	
0001F	Special Instructions, GC/MS VOA		SPECIAL INST. NON!				2.25	12.75	38.25	
0219	Nitrogen, Nitrate/Nitrite	WA	EPA 353.3	3	15.00		2.43		•	
. •	- ·		SW-846 3005	3	15.00		2.25	12.75	38.25	
03921	Flame/ICP Prep for Metals, Waters	·	28-840 3003	_			56.25	318.75	1,275.00	
0976	Orinking water volatiles	WA	EPA 524.2	4	375.00		20.22			
	_		504 77F /	3	25.00		3.75	21.25	63.7°	
1125	Sulfate, Turbidimetric	W	EPA 375.4	,				11,90	35.70	
7254	Iron by ICP	w	SW-846 6010	3	14.00		2.10	11.90	22.1.	
1234	11 on by ter									

Total Price \$ 1,450.95

Pricing Summary

\$ 1,707.0 Extended List Price 0.0 Total Rush Charges \$(256.0 Total Discount

TOTAL AMOUNT DUE \$ 1,450.9



Ref: 94-BN3/rc

January 6, 1994

Dr. John Wilson

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

Post Office Box 1198

Ada, OK 74820

THRU: S.A. Vandegrift

Dear John:

Attached are results for methane on samples as per Service Request # RE-0-39. Samples were received on 12/22/93 and 12/28/93 and analyzed on 12/27/93 and 1/3/94. Samples were prepared as described in the paper "Dissolved Oxygen and Methane in Water by a GC Headspace Equilibration Technique", by Kampbell et al., in International Journal of Environmental Analytical Chemistry, Volume 36, pp. 249-257. Analysis and calculations were performed as per RSKSOP-147.

If you have any questions, please feel free to see me.

Sincerely,

Bup Newell

Bryan Newell

xc: R.L. Cosby J.L. Seeley

SF-0-39

	•
ANALYZED 12/27/93	14NE
SAMPLE	METHANE
LAB BLANK	0.0003
MW-2	0.0003
MW-3	0.459
MW-4	0.012
MW-5	2.040
MW-6	0.002
MW-7	ND
MW-8	0.006
MW-9	0.006
MW-13	0.498
MW-13 FIELD DUP	0.483
MW-14	0.023
MW-14 LAB DUP	0.023
ANALYZED 1/3/94	
MW-1	0.041
MW-1 FIELD DUP	0.042
MW-20	0.044
STANDARDS	
10 PPM CH4	9.86
100 PPM CH4	99.79
1000 PPM CH4	1000.05
1 % CH4	0.94
4 % CH4	3.79
LIMITS OF QUANTITA	TION
LOWER	0.001
UPPER	3.679

UNITS FOR SAMPLES ARE mg/L UNITS FOR STANDARDS CORRESPOND TO UNITS IN THE SAMPLE COLUMN.

CHAIN OF CUSTODY RECORD/LAB WORK REQUEST

LABORATORY U.S. EPEN

Chein of Custody Number

Cooler Number Lot Control ID ō

A)r BIH No. Page

Present on Outer Peckage LABORATORY USE ONLY Shipped or hand delivered Received Broken/Leaking Clacrepancies Between Sample Labels and COC Record? 1 Unbroken on Sample (Improperly Seeled) Present on Sample Property Preserved 2 Unbroken on Outer 2 Ambient or Chilled SAMPLES WERE: Received Within Holding Times COC Tape Wee: z z 3 Temperature Notes: Notes Notes: Notes: SPECIAL INSTRUCTIONS (I.e. metale liet..): 200 JAHLISM ANALYSES REQUEBTED NOC CYanide Received by GOM HAT **Post/PCB** 3AME Relinquished by DOA ²Sempling Technique: Composibe=C Grab=G (IEDDI) enemiernes to B 3 12-20/5/7/60 Ž 3 12-20 1433 W 2-20/455 W 15/5/100 'Xhah 1257 1700 E E 12-21-97 1309 11-11 11.17 17-7 12-16 4-21 17-70 Data Collected DC - Drum Solids LD- Drum Uquids EP/TCLP Leachate 12-20-5 Depth Interval (ft) di. P į 0 1446-3 MW -8 AUL - 4 11M1-2 ans 6 Mul-5 The Kindle MWmm-K Burn Kruth SON (001) 273-043 Received by Sample 1D MW -MW. NG - Ground Water K-034 LF · Product AA · Air SW · Wipe MONTGOMERY WATSON, INC. 028 Location 2 S Z 7 Phone (801) 272-1900 E > S × Samplere Signature Refinquished by NS - Surface Water Project Number SE · Sediment Lab IO No. (Lab Only) WW Centact Project ... Date Due SQ- Sol Medic

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19-72-61

Notes:

HILL AIR FORCE BASE
OPERABLE UNIT 1
CHAIN OF CUSTODY RECORD/LAB WORK REQUEST

MONTGOMERY WATSON, INC.

LABORATORY

20.9 Jetot ŧ Chaln of Custody N Cooler Number Lot Centrol ID Ppge Air BIN No.

- 7	ୀ ଦ	30 P. 180	acot				(1810				AWAL)	analyses requested	EQUE	STED			LABORATORY USE OM.
Project Number Date Due Samplers Signature	2208.	200	hamha	batsolloc	Collected		ing Technique?	2M 65c0) 2M 85c0)	(AUS + OTS WZ) (OTS WZ) (BUT WZ) AMEN	SOI, NIVAA.	, 14g. 14n, الله	. Fe, Mg, Mn. . Ce, Fe, Mg, Mn,	-3MH				SAMPLES WERE: 1 Shipped or hand delivered Notes: 2 Ambien or Chilled
Lab ID No. (Lab Only)	Location	Semple	Depth Interval (ft)) elect	•miT	Matrix	ignas sanid	222		a. R	CA, Fa	K He					Notes:
	870	INW - 1	6	1221	03//	3	19						X				4 Received BrokeryLeaking
	870	14W-2	20 02	1221	0900	7	6 2					_	X		-		(Improperly Seeled)
						-											Notes
			1	~													5 Properly Preserved
						\vdash	_										Z
		0			1	H			41	1	1/	16					
				1		 	K					1			-		Holding Times
						1	_		14		7	+			i		Notes:
						\vdash	1		F			_					
					P	1	_			1							COC Tape Wee:
																	1 Present on Outer Packed
						-	-		-	_		7			\dashv		2
							_								-		2 Unbroken on Outer Package
100000	SW.		OC. Design Collide	•	Semaline Lechalone	404			SP	ECIAL	MSTA	UCTIO	NS P.		SPECIAL INSTRUCTIONS (B.O. Mobile Hot.):	•	N N
SG - Sedment		WG - Glound Water LF - Product AA - Ar sw - Water	LD- Drum Liquide EP/TCLP Leachale	•	Composite-C Grab-O	Ç											2 Present on Sample Y NA NA
· 11.50.74																	

Y N NA		Circrepencies Between	Record?	Abries:	
Time					
Received by					
Relinquished by					
Time	1700	(50c	/530		
Date	11-1193	12/81/21	66-36-61		
Received by	Keo X	Sters Vendly it	x Rues. Nuch		
Refineulabed by	A PART		\S		
	Received by Date Time Relinquished by Received by Date Time	Received by Date Time Relinquished by Received by Date Time	Recaived by Date Time Relinquished by Received by Date Time	Received by Cate Time Relinquished by Received by Date Time	Recaived by Clate Time Relinquished by Received by Date Time

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Ref: 93-LS9 August 25, 1993

for. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74821-1198

THRU: S.A. Vandegrift SH

Dear Don:

Please find attached results of the aqueous samples from Hill AFB, in Utah, to be analyzed by purge-and-trap GC-PID/FID for Benzene, Toluene, Ethylbenzene, the Xylene isomers, the Trimethylbenzenes and Fuel Carbon. We received your 11 samples, in duplicate, on August 24, 1993 in 40 mL VOA vials. A 1/10 dilution was performed on sample "82-MW-11" due to the presence of free-floating product on the sample. On August 24, 1993, automated purge-and-trap sampling was performed using an OI autosampler and an OI 4460 sample concentrator in line with a HP 5890 gas chromatograph. A 5 place external standard curve (1-10-100-500-1000 ppb) was used to uantitate the samples.

This work was performed under Service Request #SF-0-5. RSKSOP-133, "Simultaneous Analysis of Aromatics and Total Fuel Carbon by Dual Column-Dual Detector for Ground Water Samples" was used for these analyses.

If you have any questions about these analyses, please contact me at your convenience.

Sincerely,

Lisa R. Secrest

xc: R.L. Cosby J.L. Seeley

•	and or the	BASH I CAL	STANI BENZENE	e-XVI ENE	B-XYLENE	o-XYLENE	1,3,5-TMB	1,2,4-TMB	1,23-TMB	FUEL CARBON
SAMPLENAME	BENZENE	MOTOGRA								
		;		10.000	10,780,01	107doy 0	9.49E+01	9.49E+01	9.57E+01	YN N
100 PPB	1.02E+02	1.01E+02	9.93E+01	9.785401	4 84 0.01	10,990	4.57P+01	4.82E+01	4.67E+01	*
QC, OBSERVED, PPB	S.17E+01	\$.30E+01	5.18E+01	4.795401	S COLD A	COLFIDE	5.00P+01	S.00E+01	S.00E+01	4
QC, TRUE VALUE, PPB	5.00E+01	5.00E+01	S.CODE+OI	3.00c.ed	5	S	Ž	2	£	4 2
OC LAB BLANK, PPB	Ş	2	2 9	2 5	<u> </u>	Ş	2	2	2	2
O-2 SEWER	2	ş	2	2 9	2	Ę	£	2	£	욷
O.3 STORIM	웆	2	2 :	2 5	2 5	£	£	2	2	2
82 A	2	윤	2	2 5	2 5	Ę	1.06E+00	1.43E+00	Ş	8.138+00
82 B	2	4.29E+00			4 778-01	2.62F400	2.38P+02	3.24E+02	1.20E+62	2.10E+03
82 C	4.92E+00	3.136+00	2.65E+01	4.285+01	2 620.00	Orato i	1 20P+02	1.83E+02	8.88E+01	2.47EAS
82 D	9.58E+01	1.04E+01	1.47E+02	1.496+04	S. S. S. C. M.	X	Ę	2	Ę	욷
- C	욷	2	2	29	2 5	2	Ş	2	윷	욷
82 F	2	Î		2 5	200.4	W. 97. A	4.70P.402	4.71E+02	4.68E+02	웆
500 PPB	4.73E+02	4.76E+02	4.79E+02	4.735+04	3	Ę	Ę	2	ş	웆
82-H	2	욷		7 S	200.5	CALRAD.	7.188-01	1.65E+02	6.93E+01	2.08E+03
82-MW-11	3.36E+02	9 03E+01	1.398+02	704306.7	6.5.557.65	1 300,02	CO-032 9	# 28P+02	6.07E+02	1,000,04
•£2.MW-10	2	2.90E+02	4.43E+02	4.01E+02			5	S	2	2
CC LAB BLANK PPB	2	웆	2	2		2730.00	778.00	2.2584.00	2.39E+00	×
2 5 PPB	2.30E+00	2.09E+00	3.12E+00	2.692+00	1.93E+U0	0.000 a	4 748.01	104R201	4.82E+01	*
OC OBSERVED, PPB	5.24E+01	5.29E+01	5.27E+01	10+388.4	4.592401	2000.0	COP.AL	10+Box 5	5.00E+01	¥
OC, TRUE VALUE, PPB	5.00E+01	S.00E+01	\$.00E+01	5.00E+01	3.000	SWEET				

 Lower Limit of Quantitation = 10 ppb ND = Name Dr



Ref: 93-LS10 August 30, 1993

Dr. Don Kampbell

R.S. Kerr Environmental Research Lab

U.S. Environmental Protection Agency

P.O. Box 1198

Ada, OK 74821-1198

THRU: S.A. Vandegrift

Dear Don:

This letter is written in response to Dr. J. Wilson's inquiry concerning the reported value of benzene for the Hill AFB aqueous sample "82-MW-10" (Ref: #93-LS9). Due to the presence of free-floating product on the aqueous sample, a 1/10 dilution was performed prior to analysis on August 24, 1993. The report letter incorrectly identified the diluted sample as "82-MW-11." As a result of Dr. Wilson's inquiry, a 1/2 dilution was made on the duplicate of sample "82-MW-10" and was analyzed on August 30, 1993. The sample was stored at 4°C until diluted. Results of the analysis are attached. Due to the dilution, the lower limit of quantitation is 2 ppb for all compounds. A place external standard curve (1-10-100-500-1000 ppb) was used to quantitate the sample.

This work was performed under Service Request #SF-0-5. RSKSOP-133, "Simultaneous Analysis of Aromatics and Total Fuel Carbon by Dual Column-Dual Detector for Ground Water Samples" was used for these analyses.

If you have any questions about these analyses, please contact me at your convenience.

Sincerely,

Lisa R. Secrest

J.L. Seeley J. Wilson

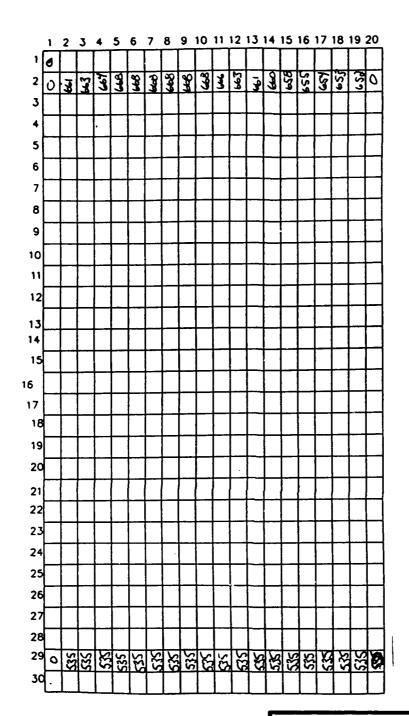
	NA NA NA 1.778-04
123-1948	4.35E+01 5.00E+01 1.89E+00 6.83E+02
1.24-TMB	4.62E+01 5.00E+01 1.89E+00 9.74E+02
13,5-TMB	4.32E+01 5.00E+01 1.99E+00 7.13E+02
•XYLENE	4.67E+01 5.00E+01 1.99E+00 1.49E+03
B-XYLENB	4.278+0% 5.00E+01 1.64E+00 2.88E+03
-XYLENB	4.45E+01 5.00E+01 2.27E+00 4.71E+02
ETITLBENZENE	4.87E+01 5.00E+01 2.13E+00 5.43E+02
TOLLIENE	. 4.56E+01 5.00E+01 1.77E+00 3.40E+02
BENZENE	4.528-01 5.008-01 1.798-00 ND
SAMPLENAME	QC, OBSERVED, PPB QC, TRUB VALUE, PPB 2 PPB •62-MW. (0 Duplicate

ND = None Detected; *Lower Limit of Quantitation = 2 ppb; N/A = Not Analyzed

(4)

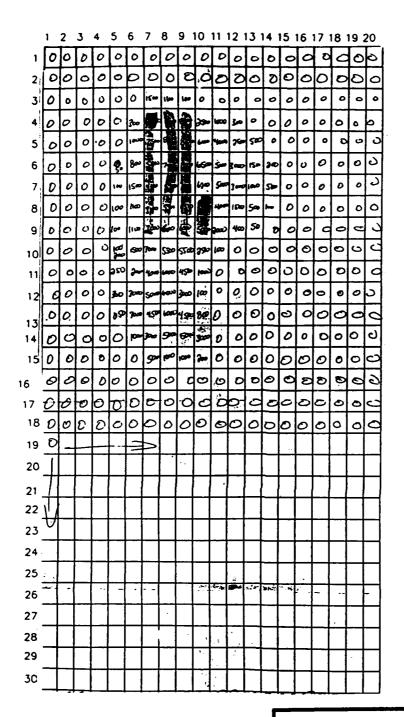
APPENDIX D

GRIDDED MODEL INPUT AND CALIBRATION RESULTS



Each cell is 85x110 ft Add 4,000 ft for ground water elevation above mean-sea-level (msl) Boundary Ground Water Levels For Hill AFB Model

ENGINEERING-SCIENCE, INC.



Each cell is 85x110 ft Concentrations are shown as $\mu g/L$, input as mg/L

Total BTEX Concentrations
For Hill AFB Model

ENGINEERING-SCIENCE, INC.

		Oxy	gen o	conc	entra	tions	use	d for	initia	al set	up o	f Hill	mod	el, F	all 19	993						
		(mg/	L)																			
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19		(x-axis)
(y-axis)	1	5	5	5	5	5	5	4.7	4.9	5	5	5	5	5	5	5	5	5	5	5	5	
 .	2	5	5	5	5	5	4.8	3	3	4.5	5	5	5	5	5	5	5	5	5	5	5	
	က	5	5	5	5	5	4.1	1	1	3	4.5	5	5	5	5	5	5	5	5	5	5	
	4	5	5	5	5	4.8	3.1	3	1	2	3	4	4.7	5	5	5	5	5	5	5	5	
	5	5	5	5	5	4.5	3	0.1	1.1	1.5	2	2.9	3.6	4.7	5	5	5	5	5	5	5	 -
	6	5	5	5		4.2	2.5	0.5	0.1	0.3	1	2	3	4	4.7	5	5	5	5	5	5	<u> </u>
	7	5	5	5		4	2	0.5	0	0.5	1.2	2	3	3.9	4.5	5	5	5	5	5	5	
	8	5	5	5	4.5	3.2	1.7	0.5	0		1.5		2.9	3.6	4.2	4.9	5	5	5	5	5	
	9	5	5		4.2	2.5	1.4	0.5	0		1.7	2.2	2.9	3.4	4	4.6	5	5	5	5	5	
	10	5	5		3.8	2	1.2	0.5	0		1.6	2.3	2.9	3.5	4	4.5	4.9	5	5	5	5	
	11	5	4.9	4.5	3.1	1.9	1.1	0.4	0	_1	1.6	2.4	3	3.5	4	4.5	4.9	5	5	5	5	
	12	5	4.7	4.2		1.7	1	0.1	0	L. I	1.9	2.6	3.3	3.8	4.2	4.7	4.9	5	5	5	5	
	13	5	4.7	4.2	2.5	1.5	0.7	0	0.5	1.2	2.1	3	3.8	4.4	4.7	4.9	5	5	5	5	5	
	14	5	4.7	4	2.5	1.5	0.5	0	0.7	1.7	2.6	3.6	4.5	4.8	5	5	5	5	5	5	5	
	15	5	4.7	4	2.3	1.3	0.5	1	1.2	2.3	3	4.5	4.9	5	5	5	5	5	5	5	5	
	16	5		3.5	2.2	1.5	1.1	1.2	2	2.6	4	4.9	5	5	5	5	5	5	5	5	5	
	17	5		3.5	2.1	1.8	1.8	2	2.6	3.6		5	5	5	5	5	5	5	5	5	5	
	18	5	4.7	4	2.5	2.2	2.2	2.7	3.5	4.5	5		5	5	5	5	5	5	5	5	5	
	19	5		4.2	3.1	3	3	3.5	4.5	4.9	5		5	5	5	5	5	5	5	5	5	
	20	5			4.2	4	4	4.5	4.9	5	5	5	5	5	5	5	5	5	5	5	5	
	21	5	5		4.7		4.7	4.9	5		5		5	5	5	5	5	5	5	5	5	
	22	5	5		5	5	5	5	5		5		5	5	5	5	5	5	5	5	5	
	23	5	5	5	5	5	5	5	5		5	5	5	5	5	5	5	5	5	5	5	ļ
	24	5	5	5	5	5	5	5	5		5	5	5	5	5	5	5	5	5	5	5	
	25	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	
·	26	5	5	5	5	5	5	5	5	5	5		5	5	5	5	5	5	5	5	5	
	27	5	5	5		5	5	5	5		5		5	5	5	5	5	5	5	5	5	
	28	5	5	5	5	5	5	5	5	5	5		5	5	5	5	5	5	5	5	5	
	29	5	5	5	5	5	5	5	5		5		5	5	5	5	5	5	5	5	5	
	30	5	5	5	5	5	5	5	5	5	5	5	5	5	_ 5	5	5	5	5	5	5	
																					<u></u>	
						L				<u> </u>	L			L							L	

Each cell is 85x110 ft Concentrations are in mg/L Dissolved Oxygen Grid For Hill AFB Model

ENGINEERING-SCIENCE, INC.

																		<u> </u>		7		_
																						
·— ·	\neg	Nitra	te (a	s N)	Val	ues	used	in in	itial s	setur	of F	iii M	odel	Fall	of 1	993.						
		(mg/															_					
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	(x-axis)
(y-axis)	1	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	
·	2	5	5	5	5	5	4.5	4.5	5	5	5	5	5	5	5	5	5	5	5	5	5	
	3	5	5	5	5	4.5	2	2	4.5	5	5	5	5	5	5	5	5	5	5	5	5	<u> </u>
	4	5	5	5	5	3.5	0.8	1	3.5	4.8	5	5	5	5	5	5	5	5	5	5	5	
	5	5	5	5	5	3.5	1	0.2	1	4.5	5	5	5	5	5	5	5	5	5	5	5	
	6	5	5	5	5	4	1.5	0	1	3.5	5	5	5	5	5	5	5	5	5	5	5	
	7	5	5	5	5		1.5	0	1.2	3.8	5	5	5	5	5	5	5	5	5	5	5	
	8	5	5	5	4	3	1	0	1.5	4.5	5	5	5	5	5	5	5	5	5	5	5	
	9	5	5		3.5	2	0.8	0	1.5	4	5	5	5	5	5	5	5		5	5	5	í
	10	4.9		3.5			0.6		0.8		4	4.5	4.7	4.7			4.9		5	5	5	,
	11			3.2	2.1	1.1	0.4		0.4		1.5	2	3	3	3	3	4	4.7	5	5	5	1
	12	3.6	3.3	2.9		0.9	0.4	0	0	0.4	0.6	8.0	1.3	2	2.2			4	5	5	5	
	13	3.5	3.2	3	2.9	1.5	0.6		0	0.2	0.4	0.6	1.1	1.7	2.2	2.7	3.2		5	5	5	ľ
	14	3.5	3.4	3.2	4.2	3.5		0.6		0.1	0.5		1.3	1.9	2.5	3.2	4.5	5	5	5	5	I
	15	3.7	3.7	3.9	4.9	4.9	3.5			0.2	0.7	1.2		2.5	3.3	4.5	5		5	5	5	
	16	3.9	4.5	4.7	5	5	4	1.5			1.4	2	3	3.6	4.5	5	5		5	5	5	1
	17	5	5	5	5	4	1.5	0.5		1.5	2.5	3.2	4	4.6	5	5	5		5	5	5	
	18	5	5	5	4	1	0.8	1	2.5	3	3.6	5	5	5	5	5	5		5	5	5	
	19	5	5	5	5		4.5		4.5	4.7	4.9	5	5	5	5	5	5		5	5	5	
	20	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5			5	5	5	
	21	5	5	5	5		5		5	5	5	5	5	5	5	5	5		5	5	5	
	22	5	5	5	5	5	5		5		5	5	5	5	5	5	5		5	5	5	
	23	5	5	5	5	5	5		5	5	5	5	5	5	5	5	5	5	5	5	5	
	24	5	5	5	5	5	5		5	5	5	5	5	5	5	5	5	5	5	5	5	
	25	5	5	5	5	5			5		5	5	5	5	5	5	5		5	5	5	
	26	5	5	5	5	5			5		5	5	5	5	5	5	5		5	5	5	
	27	5	5	5	5	5	5		5		5	5	5	5	5	5	5		5	5	5	
	28	5	5	5	5	5	5		5	5	5	5	5	5	5	5	5	5	5	5	5	
	29	5	5	5		5					5		5	5	5				5	5	5	
	30	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	

Each cell is 85x110 ft

Concentrations are in mg/L

Nitrate (as N) Grid For Hill AFB Model

ENGINEERING-SCIENCE, INC.

	Т																					
	N	litra	te va	alues	(as	nitra	te io	n) us	ed in	initi	al se	tup o	f Hill	mod	lel, F	all 1	993	•				
		mg/			r ` l																	
	⇈	_ <u>Ť</u>]	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	(x-axis)
(y-axis)	1	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14		14	<u>(</u>
	2	14	14	14	14	14	13	13	14	14	14	14	14	14	14	14	14	14	14		14	
	3	14	14	14	14	13	5.8	5.8	13	14	14	14	14	14	14	14	14	14	14	14	14	
	4	14	14	14	14	10	2.3	2.9	10	14	14	14	14	14	14	14	14	14	14	14	14	
	5	14	14	14	14	10	2.9	0.6	2.9	13	14	14	14	14	14	14	14	14	14	14	14	
	6	14	14	14	14	12	4.3	0	2.9	10	14	14	14	14	14	14	14	14	14	14	14	
	7	14	14	14	14	10	4.3	0	3.5	11	14	14	14	14	14	14	14	14	14	14	14	
	8	14	14	14	12		2.9	0	4.3	13	14	14	14	14	14	14	14	14	14	14	14	
		14	14	12	10		2.3	0	4.3	12	14	14	14	14	14	14	14	14	14	14	14	
1	0	14	12	10	8.6	4.6	1.7	0	2.3	5.8	12	13	14	14	14	14	14	14	14	14	14	
_		11	10	9.2	6	3.2	1.2	0	1.2	2.3	4.3			8.6	8.6	8.6	12	14	14	14	14	
		10	9.5				1.2	0	0	1.2	1.7	2.3	3.7	5.8	6.3	7.2	8.3	12	14	14	14	
		10	9.2			4.3	1.7	0.6	0	0.6	1.2	1.7	3.2	4.9	6.3	7.8	9.2	13	14	14	14	
		10	9.8		12	10		1.7	0.3	0.3			3.7	5.5		9.2	13	14	14	14	14	
	_	11	11	11	14	14	10	2.9	0.6	0.6	2	3.5			9.5	13	14	14	14	14	14	
		11	13	14	14	14	12	4.3	0.6		4	5.8		10	13	14	14	14	14	14	14	
		14	14	14	14	12	4.3	1.4	2				12	13	14	14	14	14	14	14	14	
		14	14	14	12			2.9	7.2				14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	13	13	13				14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
3	0	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	
		\dashv																[
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Each cell is 85x110 ft Concentrations are in mg/L Nitrate (as NO₃) Grid For Hill AFB Model

ENGINEERING-SCIENCE, INC.

ſ——																						
	\neg	Com	bine	d co	ncen	tratio	ns o	foxy	rgen	and	nitra	e us	ed fo	r se	up o	f Hill	mod	el, F	all 1	993.		
		(mg/																				
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	(x-axis)
(y-axis)	1	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	
	2	19	19	19	19	19	18	16	17	19	19	19	19	19	19	19	19	19	19			
	3	19	19	19	19	18	9.9	6.8	14	17	19	19	19	19	19	19	19	19	19			
	4	19	19	19	19	15	5.4	5.9	11	16	17	18	19	19	19	19	19	19	19	1		
	5	19	19	19	19	15	5.9	0.7	4	14	16	17	18	19	19	19	19	19	19		19	
	6	19	19	19	19	16	6.8	0.5	3	10	15	16	17	18	19	19	19	19	19	1		
	7	19	19	19	19	14	6.3	0.5	3.5	11	16	16	17	18	19	19	19	19				
	8	19	19	19	16	12	4.6	0.5	4.3	14	16	17	17	18		19	19	19	19	1		
	9	19	19	16	14	1	3.7	0.5	4.3	13	16	17	17	18		19	19	19	19			
	10	19	17	15			2.9	0.5	2.3	6.8	13	15	16	17	18	18	19	19	19	1		
L	11	16	15	14		5.1	2.3	0.4	1.2	3.3	5.9	8.2	12	12		13	16	19	19		19	
	12	15	14	13		4.3	2.2	0.1	0	2.2	3.6	4.9	7	9.6	11	12	13	17	19			
<u></u>	13	15	14	13		5.8	2.4	0.6		1.8	3.3	4.7	7	9.3	11	13	14	18	19			
	14	15	14	13			3.4	1.7	1	2	4	5.9	8.2	10	12	14	18	19	19			
	15	16	15	15	16	15	11	3.4	1.8	2.9	5	8	10	12	14	18	19	19	19			
	16	16	18	17	17	16	13	5.5	2.6	4.3		11	14	15	18	19	19	19	19			
	17	19	19	18	16	13		3.4	4.6	7.9	12	14	17	18		19	19	19				
	18	19	19	18	14		4.5	5.6	11	13	15	19	19	19		19	19	19				
	19	19	19	19	17	17	16	16	17	18		19	19	19		19	19	19				
ļ	20	19	19	19	19	18		19	19	19		19		19		19	19	19				
<u> </u>	21	19	19	19	19	19		_	1	19		:		19		19	19	19		1 -		
	22	19	19	19	19	19					19			19		19	19	19	19			
	23	19	19	19	19	19			19	19	19	19		19	19	19	19	19	19	1		
	24	19	19	19	19	19	L.			19	19	19		19		19	19	19	19			
	25	19	19	19	19	19				19	19	19		19	19		19	19				
	26	19	19	19	19	19				19	19	19		19	19	19	19	19				
	27	19	19	19		19	L			19	19			19	19	19	19	19	19			
	28	19	19	19	19	19			1	19	19			19	19	19	19	19	19			
	29	19	19	19	19	19	<u> </u>		19	19	19	19	19	19	19	19	19	19	19			
L	30	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	19	

Each cell is 85x110 ft Concentrations are in mg/L Combined Oxygen and Nitrate (as NO₃) Concentrations For Hill AFB Model

ENGINEERING-SCIENCE, INC.

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		(x-axis)																																
	7	20	5	5	5	2	ý	5	သ	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	S	သ	2	5	5	5		
		19	2	2	2	2	5	5	5	S	2	5	2	5	5	5	2	5	5	2	5	5	5	5	5	5	2	2	2	5	5	5		
	7	18	2	2	2	2	2	2	2	2	5	2	5	2	5	5	5	5	5	2	2	5	5	5	5	5	5	2	S	5	5	2		
	\dashv	17	2	5	2	2	2	5	သ	2	2	5	2	2	2	2	2	5	2	2	2	2	5	2	2	5	2	သ	2	2	2	2		
	\neg	16	2	5	2	2	5	5	5	2	5	4.9	4.9	4.9	2	2	5	5	2	5	2	5	5	5	2	5	2	2	2	2	2	5		
33	\dashv	15	2	5	5	5	2	5	5	4.9	4.6	4.5	-	4.7	6.4	2	2	2	2	2	2	5	5	5	5	5	2	2	2	5	2	5		
1993		4	2	5	5	5	2	4.7	4.5	4.2	4	4		4.2	4.7	2	2	5	5	5	2	5	2	2	5	5	5	2	2	2	5	5		П
Hill model, Fall	-	13	2	5	5	2	4.7	4	3.9	3.6	3.4	3.5	3.5	3.8	4.4	8.4	2	5	2	5	2	5	2	2	5	5	2	2	2	5	2	2	П	
ode	-	2	2	2	2	7.	3.6	3	3	6	6	2.9	6	3.3	3.8	4.5	4.9	5	2	2	2	5	2	2	2	5	2	2	5	2	2	2		
±ill π	+	=======================================	5	2	2	4	6.	7	2	2 2	2	3	4	9	3	3.6	5.	6.	2	2	2	2	2	5	2	5	2	2	2	2	2	2		
of t	\dashv	0	2	5	3.	က	2 2	-	7	.5	1.7 2	.6	1.6 2	1.9 2.	2.1	ဖ	3 4	4	ω.	2	2	2	5	2	2	5	2	2	5	2	2	2	Н	
etup	-	6	2	5	3 4	2	.5	6	.5	1	1	-	-	1	7	1.7 2	က	9	3.6 4	5	6	2	5	2	2	5	2	2	2	2	2	2		
tials	-	- 80	6	3 4	1	-	11	1.	0 0	0	0	0	0	0	5.	0.7	.2 2.	2 2	9	.5 4	5.	<u>ن</u>	2	2	S	5	2	2	5	5	2	5		
or in	\dashv		7	3	-	3	1	5	5	5	0.5	0.5	4	0.1	0	0	5.	7	2.2	7 3	4	5	6.	2	2	5	2	2	2	5	2	2	H	H
ed f	1	9	5.4	80	-	1	3 0.1	5 0.	_	7 0		2.0	0	0	7	0.5	0.5	1	ω .	2 2	<u>ي</u>	4	7 4	2	2	5	2	5	5	5	2	2		
รท รเ	\vdash	2		5.4.	5.4	3.	2	2 2	4	2 1.	5 1.	2 1.	1.1	_	5 0.7	1.5	<u>د.</u>	5.1.1	8	2	3	4	7	2	2	2	2	2	2	2	2	2	\vdash	
atio		4	<u> </u>	2	5	4	5.4	9.4	_	5.	2	80	_	9 1.7	5 1.5	<u> </u>	7	7	_	5 2	_	2	7.4	2	2	5	5	2	5	5	2	2	H	
Oxygen concentrations used for initial setup of		3		2	5	2	5	5.4	5	5.4	7	က	5.3.1	2.2	2	4 2.5	4 2.3	5 2.2	5 2.1	4 2.5	2 3.1	7 4.2	4	2	2	5	5	5	5	5	2	2		Н
Š			<u> </u>	L	L			5			5.4	5 4.6	9.4	4	4	Ĺ	,	લ	6		4	9 4.7	5.4	3	20	2	L	5	5	2	2	2		<u> </u>
/gen	ĮĮ.	2		2	3	L		L	L			L	4	4.7	4.7	4.7	4	4.7	4.7	4.7	4	4	L		5		L			5	5	5	_	
ố	(mg/L)		3	2	2	2	2		2	2	2		5	3	3	3	S	3	2	2	5	2	2				L	L	L		L		_	L
			1	2	3	4	3	9	7	æ	6	우	1	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		
			(y-axis																															

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				(x-axis)									Ē																					
				20	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	2	2	5	5	5	S	သ	5	5	150	3	2
				19	5	5	5	5	2	5	5	2	5	2	5	2	5	5	2	5	2	2	2	5	2	2	2	2	5	2	5	5	2	2
				18	5	2	5	5	2	5	5	5	5	5	2	S	2	5	2	5	2	2	2	2	2	2	2	5	2	S	2	2	5	5
		1		17	5	5	5	5	5	5	5	2	2	5	4.7	4	4.5	2	5	2	2	2	သ	5	2	2	2	5	5	5	2	5	3	5
		Ī		16	5	2	5	5	2	5	5	2	2	60:	4	2.9	3.2	4.5	2	5	5	S	2	2	5	2	2	2	2	5	S	2	5	2
		1993.		15	5	S	5	2	2	5	5	2	2	1 0	6	2.5	2.7	3.2	4.5	2	5	2	2	2	2	2	2	2	2	2	5	5	3	2
		of 15		4	2	2	2	2	S	5	5	2	2	4.7	3	2.2	2.2	2.5	3.3	4.5	2	2	2	2	5	2	2	2	2	2	2	2	5	2
		Fall		13	5	2	2	5	2	2	2	5	S	4.7	6	7	1.7	1.9	2.5	3.6	4.6	2	2	2	5	2	2	2	5	5	2	2	5	5
П		Model	十	12	2	2	2	2	5	5	5	S	2	4.7	3	1.3	1.1	1.3	1.9	3	L	5	2	2	2	2	2	2	2	2	2	2	သ	2
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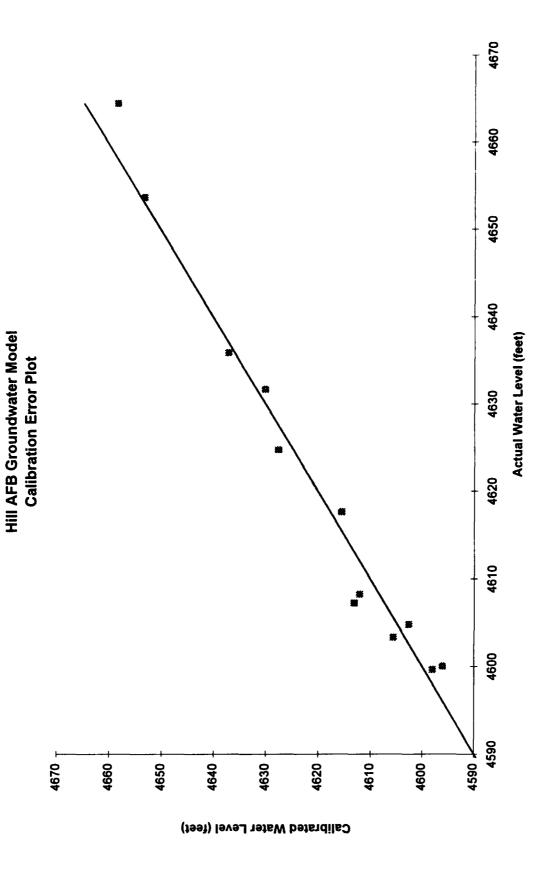
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Ground Water Model Calibration Error

	Actual	Calibrated	derivation from mean								
Location	Water Level	Water Level	h _m -h _s	abs(h _m -h _s)	$(h_m-h_s)^2$						
EPA82I	4664.53	4658.0	-6.53	6.53	42.6409						
EPA82D	4631.70	4630.0	-1.7	1.7	2.89						
EPA82B	4608.28	4612.0	3.72	3.72	13.8384						
EPA82C	4603.37	4605.5	2.13	2.13	4.5369						
EPA82F	4600.06	4596.0	-4.06	4.06	16.4836						
EPA82E	4595.21	4587.5	-7.71	7.71	59.4441						
EPA92H	4599.66	4598.0	-1.66	1.66	2.7556						
CPT-41	4635.89	4637.0	1.11	1.11	1.2321						
CPT-23	4 617. 65	4615.5	-2.15	2.15	4.6225						
CPT-21	4624.80	4627.5	2.7	2.7	7.29						
CPT-15	4607.29	4613.0	5.71	5.71	32.6041						
CPT-31	4604.83	4602.5	-2.33	2.33	5.4289						
MW12	4653.73	4653.0	-0.73	0.73	0.5329						
Total:	60047	60035.5	-11.5	42.24	194.3						
	<u> </u>										
			ME	-0.884615							
			MAE=	3.2492308							
			RMS=	3.8660256							

hm=calibrated water level hs=actual water level ME=1/n* Σ (h_m-h_s) MAE=1/n* Σ |(h_m-h_s)| RMS=(1/n* Σ (h_m-h_s)²)^{0.5}

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ESTIMATION OF LONGITUDINAL DISPERSIVITY

Assumptions:

A. Plume migration is sufficiently aligned along the

longitudinal axis of the grid that a longitudinal moment may be

calculated.

B. Longitudinal dispersivity is 1/10 of the distance from the

source of contamination to the center of contamination.

From the attached figure, an estimate for the center of mass will be taken by calculating the longitudinal moment around cell 9,2 which is near the source of contamination:

		Distance From	Mass x Dist.
Row	<u>Mass</u>	cell (2.9)	From Cell 9,2
Row 3	4500 ug/L	110	495000
Row 4	25660 ug/L	220	5645200
Row 5	29950 ug/L	330	9883500
Row 6	29150 ug/L	440	12826000
Row 7	26450 ug/L	550	14547500
Row 8	22850 ug/L	660	15081000
Row 9	18700 ug/L	770	14399000
Row 10	16600 ug/L	880	14608000
Row 11	17000 ug/L	990	16830000
Row 12	17625 ug/L	1100	19387500
Row 13	15100 ug/L	1210	18271000
Row 14	2950 ug/L	1320	3894000
Total	226535 ug/L		145867700

The estimated longitudinal centroid of the plume is:

145867700/226535 ug/L = 643.9 ft (from the center of cell 2,9)

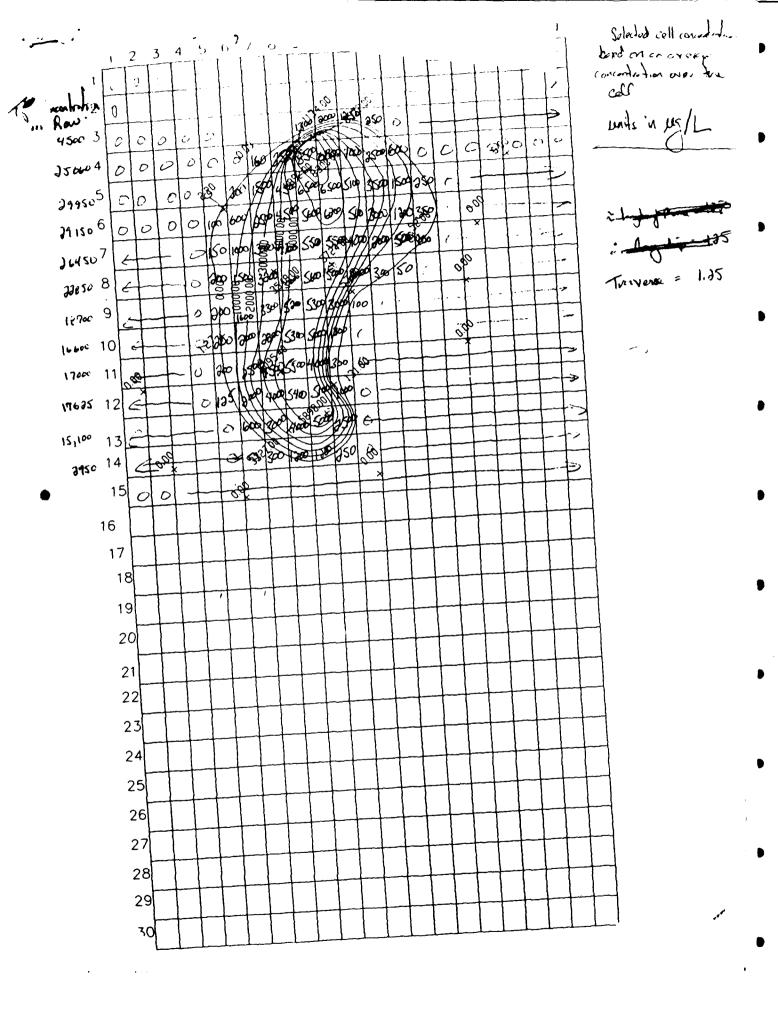
The estimated source of contamination is at cell 3,9. Therefore, the estimated distance between the source of contamination and the longitudinal center of mass is:

$$643.9 \text{ ft (centroid)} - 110 \text{ ft (distance from 2,9 to 3,9)} = 533.9 \text{ ft}$$

From assumption B, the estimated longitudinal dispersivity is 1/10 of the distance between the source of contamination and the longitudinal center of mass and is:

Estimated Long. Dispersivity = $533.9 \times 0.1 = 53.39 \text{ or } 53.4 \text{ ft.}$

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